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- Item 1** Specifications Section 09671 Epoxy Flooring
Part 2 - Products, paragraph **2.3 Components**
Under item 1 **delete** sub-item .9 and **replace** with “Basis-of-Design Product: Sika Canada Inc., Sikafloor Duochem-9205.”

Under item 4 **delete** sub-item .12 and **replace** with “Basis-of-Design Product: Sika Canada Inc., Sikafloor 510 LPL”
- Item 2** Specifications Section 08520 Aluminum Windows and Doors
Part 2 – Products, paragraph **2.4 Fabrication**
Add item 8 – “Insulated Panels –Spandrel Glass, mineral wools semi-rigid insulation in galvanized steel back pan to be held in place with stick pins clips and continuously sealed to frame. Panel finish: Duranar XL, three coat, coil-coated finish containing Kynar 500 polyvinylidene fluoride resin. Colour: to Consultant’s selection”
- Item 3** Specifications Section 07112 Air / Vapour Barrier
Part 2 – Products, paragraph **2.1 Membranes**
Delete item 4 – Air Barrier in its entirety.
- Item 4** Specification Section 07212 – Rigid Insulation
Part 2 – Products, paragraph **2.1 Insulation**
Add item
“ **2. Cavity Wall Insulation - Masonry:** Expanded polystyrene insulation to CAN/CGSB-51.20-M87, Type 4 butt or ship lapped edges. For use in cavity wall construction above and below grade.

.1 Thickness 100 mm or as indicated.
.2 Acceptable Material: “Cavitymate” Type 3 as manufactured by Dow Chemical Canada Inc.
.3 Acceptable Material: “Celfort 300” as manufactured by Celfortec Inc. or approved equal.”
And item

“**3. Cavity Wall Insulation – Metal Panel:** water-repellent and semi-rigid thermal insulation to CAN/ULC-S702-97, formed of bonded basalt fibres. For use in cavity wall construction or portions thereof with metal panel or siding cladding.

.1 Acceptable Material: 100mm “CavityRock MD” as manufactured by Rockwool Inc.
.2 Acceptable Material: 100mm “MB PLUS” as manufactured by Fibrex Insulations Inc.”
- Item 5** Specification Section 08800 Glazing
Part 2-Products paragraph 2.1 Materials
Add item
“ 10. Spandrel Glass (SG) - 6 mm clear tempered float glass conforming to CAN/CGSB-12.3; Opaci-coat 300 by ICD High Performance Coating on 2nd surface.

- a. Spandrel Glass-1 (SG-1) colour by Architect from standard colour range.
- b. Spandrel Glass-2 (SG-2) colour by Architect from standard colour range.”

Delete item 4 – Wired Glass in its entirety.

- Item 6** Specification Section 00200 Instruction to Bidders
Under item 4. Subcontractor **add** subitem
“2. **The List of Subcontractors in the Tender Form can be issued 1 hour after tender closing.**”
and subitem
“3. The List of Subcontractors to be submitted by email to the following
- Grguric Architects office@2gai.com and to
 - the Diocese asmith@thecatholiccemeteries.ca”
- Item 7** Refer to attached A8.00. The frames for doors **107, 109, 111, and 112** have been revised to a hollow metal (HM) frame. The frame for door **102A** has been revised to screen **SC3**. The material for **SC3** in the screen schedule has been **revised to aluminium (ALUM)**.
- Item 8** Specification Section 09330 Floor Porcelain Tile
Part 2-Products, paragraph 2.1 Tiles
Under item 1. **Delete** subitem .1 and replace with “
Acceptable material: Vitra – Cement Mix Series, distributed by Centura Tiles. Size 600 mm x 600 mm, plus trim and 600 mm x 100 mm bullnosed base. Allow 2 colors from manufacturer’s full line.
Acceptable equal: Daltille/American Olean and Crossville.”
- Item 9** **Clarification** – Refer to revised A2.00 for the extent of the epoxy floor and sealed concrete floor in the Circulation Area (Rm 110) and Retort Room (Rm 121).

Electrical

Refer to attached Electrical Addendum No. E3 and E4 Issued by NRG Consultants Inc dated October 20, 2023 and October 23, 2023

Questions and Answers

Question 1

L-1 drawing indicates strip along asphalt roadway has a 1.5m sodded width, however, scales at 3m. Clarify.

Answer 1

We previously noted a minimum 1.5m sod strip but I have updated the plan to note 3m along the roadway

Question 2

Same for L-2 loop area, where scale is 2m, but notes indicate 1.5m width. Clarify.

Answer 2

We previously noted a minimum 1.5m sod strip but I have updated the plan to note 2m along the building, parking lot and turn around

Question 3

Could you provide specifications for Sodding, Seeding & Planting. Mainly for installation procedures & Warranty requirements.

Answer 3

We typically do not include specifications for a project that only involves only planting as all of the details, notes, and noted specifications (Canada Landscape Standards) provide all the information required. We have noted a 1 year warranty in our landscape notes but this will need to be confirmed by the client as we do not have a contract for the construction phase of the project and do not want to speak on their behalf if they require a longer warranty period.

Question 4

If native topsoil can be used, are there any amendments for the Seeding & Sodding areas?

Answer 4

Planting notes and details are provided on the drawing and the Landscape Notes refer to the applicable sections (seed and sod) of the Canadian Landscape Standards.

Question 5

L-2 drawing indicates that septic field is seeded, however, septic fields must be sodded. Clarify.

Answer 5

This area has been proposed to be seeded with Turf/sod mix. This area will not be naturalized as this seed will be mowed.

Question 6

Please provide further information and detail regarding the feeder from the existing administration basement utility room 002 to 200A disconnect switch in crematorium building. We need the following clarified and more information to be provided to accurately quote:

- Who is responsible for the tie-in of this feeder to the existing equipment in administration basement utility room 002? If by electrical contractor, we need to know what we are tying into. Is it during afterhours? Do we need to supply and install an overcurrent device in the existing equipment? If so, we require photos and information of the existing equipment
- No detail or information is provided on how the feeder will enter the existing administration building and what routing is required inside the building to the basement utility room 002. Please provide this information as electrical contractor cannot quote this based on assumptions.
- Please confirm the distance provided of 2,100 feet on the site plan on drawing E02 is for the underground duct bank section only from building to building. Confirm this

distance does not include any additional conduit and wire required from underground to electrical equipment in the buildings

Answer 6
Refer to electrical addendum E3

Question 7

Please confirm all EMT conduit fittings inside of building must be watertight as per specification

Answer 7
Refer to electrical addendum E3

Question 8

Please confirm supply and install of all hand dryers is not part of the electrical scope of work

Answer 8
Refer to electrical addendum E3

Question 9

Please clarify that electrical contractor to include for all communication rough-in which includes conduit stub up to ceiling space only. Confirm no conduit is required in the ceiling space and J-hooks are not required. If so, provide what is required and to what location

Answer 9
Refer to electrical addendum E3

Question 10

Please clarify that electrical contractor to include for all security rough-in which includes conduit stub up to ceiling space only. Confirm no conduit is required in the ceiling space and J-hooks are not required. If so, provide what is required and to what location

Answer 10
Refer to electrical addendum E3

Question 11

Electrical specification speaks to wiremold to be installed in exposed areas. Electrical drawings do not show any wiremold or what locations require wiremold. Please revise electrical drawings to show the wiremold in every location that it is required. This includes all vertical and horizontal runs, please also provide a detail showing how the design is intended with transitions to conduit.

Answer 11
Refer to electrical addendum E3

Question 12

Would you please be able to provide us with the latest SWM report complete with the Hydrostorm HS10 sizing report? It is requested by the manufactures of the structures.

Answer 12

Please refer to the attached SWM report prepared by S. Llewellyn and Associates Ltd dated July 2022.

Question 13

Could you provide a Site Service specification for material & installation procedures?

Answer 13

Our specifications are on our drawings. We do not provide separate written specs.

Question 14

Door frame schedule indicates 6 wood frames. Could you provide a jamb section including width of jamb, casing type, trim profile, & species of wood required. Stained?

Answer 14

All doors are to have hollow metal (HM) frames. Refer to Item #7.

Question 15

Can you provide a jamb schedule for metal frames indicating all profiles?

Answer 15

All doors with a hollow metal frame will have the same jamb profile. The over all dimensions of the profile are shown in the jamb details found on A5.00

Question 16

Door 102A indicates having a frame SC2, was this to be a ST2?

Answer 16

The frame of Door 102A is to be SC3 which is screen type ST2. Refer to item #7.

Question 17

Door Screen SC3 has 2 doors, but they are not listed or have any door dimensions, rating, paint requirements etc. Clarify

Answer 17

The doors in SC3 are to be Door 102A.

Question 18

In reference to Add#3 item#1 the base layer of ISO has been requested as a base layer of 4.5" thick plus another layer at 2" thick.

4.5" ISO is special order only and not readily available. Standard ISO sizing ends at 4" thick.

Can we substitute with a base layer of 4" and second layer at 2.5" achieving the same overall thickness.

Answer 18

Any combination of insulation thicknesses is acceptable as long as the number of layers does not exceed 2 layers and the thickness of the insulation is 165mm (6.5").

Question 19

It would appear the RTU supplier (Carrier is basis of design) is not quoting this project.

Their reason....."Engineer spec-d a product that is no longer available with Carrier"

Answer 19

The equipment schedule has two alternates, Trane and Lennox.

Question 20

Is there a cut/fill plan available for this project?

Answer 20

A cut/fill plan was not prepared for this site.

Question 21

Electrical contractor needs further detail including a detail drawing showing how the duct bank and all conduits are transitioning from underground to inside of administration building. We also require information on the existing building exterior for penetrations to enter building. A detail drawings is required to show routing inside the admin building from penetration location to existing panel PP-1

Answer 21

Refer to electrical addendum E3

Question 22

Electrical contractor requires pictures and information of the existing panel PP-1 and existing manufacture information to quote the correct 200A-3P breakers

Answer 22

Refer to electrical addendum E3

Question 23

Electrical contractor needs clarification if all work in the admin building, including power shutdown, is to be done during regular business hours

Answer 23

Refer to electrical addendum E3

Question 24

Duct bank note #8 on drawing E02 says to fix spacers to avoid floating during Concreting. However, in the section, it is Clean sand filling. Please confirm whether we go for sand filling or concreting ?

Answer 24

Refer to electrical addendum E3

Question 25

In speaking with a rep at Sika the following came up:

1. Sika 261 is typically a tinted epoxy and generally they like the quartz broadcast to be put into a clear epoxy. He is recommending 9205 instead of the 261 prime coat and body coat.
2. Regarding the 2002 and then the 510 LPL coats, he recommended doing 2 coats of 510 instead. Please advise.

Answer 25

The proposed changes suggested by Sika are acceptable. Refer to Item #1

Question 26

Can we use directional drilling with HDPE conduits in highlighted area, instead of directional boring with steel casing? This approach could potentially offer significant cost savings.

Directional drilling is only HDPE conduits, while directional boring is steel casing has conduits.

Could you please provide us with more information.

Answer 26

Refer to electrical addendum E3

Question 27

The 200A feeder shown to feed the new crematorium from the Administration Basement Utility room is not sized properly. This run will require an additional parallel run which will increase our duct bank size as shown and we will need to add an additional spare conduit.

Answer 27

Refer to electrical addendum E3

Question 28

We are also concerned with the difficulty of pulling the feeders from the second manhole to the new Crematorium as this is a great distance. We propose installing an additional 1-2 manholes along the roadway leading to the building from the second manhole. This will decrease the distance of the greatest pull.

Answer 28

Refer to electrical addendum E3

Question 29

Will splices of the building feeder done inside the manholes be accepted? If so, are there any specific requirements for these splices.

Answer 29

Refer to electrical addendum E3

Question 30

Will aluminum cabling be accepted for all feeders above 100A?

Answer 30

Refer to electrical addendum E3

Question 31

What colour is the curtainwall framing finish?

Answer 31

Medium Bronzed Anodized

Question 32

Has there been a spandrel colour chosen?

Answer 32

Colour to be provided after tender award.

Question 33

Where the spandrel and back pans are? Do the back pans need to be skinned with the framing finish?

Answer 33

Back pans can be galvanized steel where they are not visible on the interior. Where the back pans are visible, they should be coloured to match the frame colour.

Question 34

On a couple of the elevation drawings, there are posts that require aluminum cladding. Is this under my contract, or will that be taken care of by someone else?

Answer 34

Cladding of the structural posts is to be done by the same supplier as the ACM panels

Question 35

The ACM specs call for 2 different colours, one of them being Wood Grain..

Do you have any clue where this wood grain to be?

The panels on the Feature Tower Wall are oversized if we run the wood grain horizontally,

Not sure if vertical is the Architect's intent.

Answer 35

Refer to question #7 on addendum #3

Question 36

Can we submit the Proposed Subcontractors (Section 9 on the Tender Form) one hour post tender via email along with the unit rates?

Answer 36

Submission of the List of Subcontractors 1 hour after the tender closes by email is acceptable. Refer to item #6

Question 37

Reference 9.1.4 of the Supplementary Conditions:

1. Please define what can be considered a reasonable precaution necessary to protect the place of work. Would site fencing around areas of work and security cameras be considered reasonable.
2. Is it the intent that the General Contractor carry the cost of a security guard even if it is deemed unnecessary.

Answer 37

- 1) **Site fencing and security cameras would be considered reasonable precautions for the protection of the work site and owner's adjacent property.**
- 2) **A security guard will not be necessary.**

Question 38

In lieu of torch grade, can we use self-adhering Blueskin throughout masonry cavity walls.

Answer 38

Using self-adhering Blueskin on the masonry cavity walls is acceptable.

Question 39

Please provide a spec for the rigid insulation in above ground masonry walls.

Answer 39

Refer to item #4.

Question 40

DWG M6. Acoustic Treatment Of Ducts – “Supply and install all acoustic insulation as indicated on the drawings by cross hatching or by notation”. The acoustic insulation shall be 25mm thick fibre glass insulation. DWG M5, Detail 4 – HVAC-1 & HVAC-2 Plenum Details – The detail indicates the plenum with cross hatching, but the insulation is 1” thick Armaflex installed on the exterior of the ductwork. Please confirm which one will be required for this tender.

Answer 40

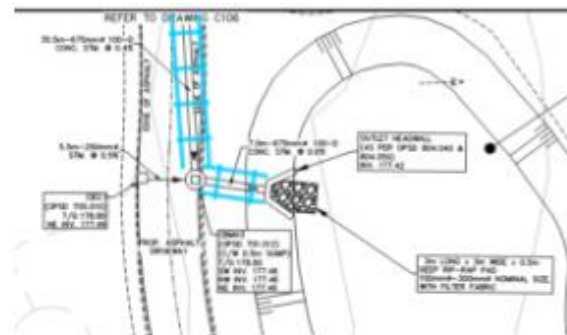
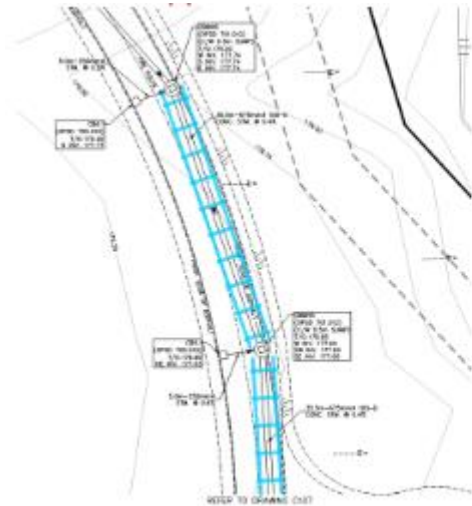
1. **Crosshatched areas of both supply and return air plenums shall have ½” thick cement board installed on the bottom inside surface of the duct.**
2. **Crosshatched areas of both supply and return air plenums shall have AP Armaflex 1” thick insulation, 25/50 smoke and flame spread tested to CAN/ULC- S102 applied to all interior surfaces of the duct.**

Question 41

Is it the intent that 575 & 675 Storm Sewers are to have rigid insulation?

Answer 41

Insulation to be as per Engineering Drawing Notes and Detail Dwg. C109 and to be applied to storm sewer sections noted below.



Question 42

On C108 it says "Dewatering Pump (Sized by Others)". Who is responsible for the pump and please provide spec.

Answer 42

Dewatering is the responsibility of the Contractor who will be responsible for supplying the pump size necessary to complete the work.

Question 43

Section 10620 indicates accordion door partitions, but they have an incorrect length. Clarify

Answer 43

The door for the viewing room (Room 109) is to be the full width of the room from the face of the door pocket to the shared wall with the circulation area (Room 110).

The 2 doors in the circulation area (Room 110) are to go from the shared wall with the viewing room (Room 109) to the bulkhead along the face of the retorts.

Question 44

Geotechnical report states the topsoil's depths provided are "not considered sufficient for estimating quantities or associated cost". Please provide a topsoil thickness that we are to use for this tender.

Answer 44

Refer to geotechnical report for topsoil depth at borehole location and to determine the average topsoil depth.

Question 45

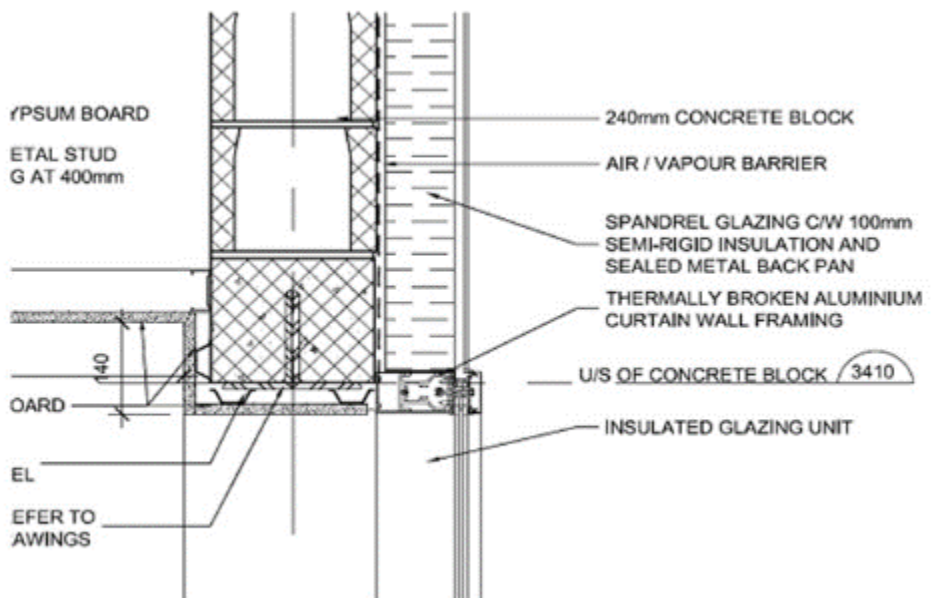
Vestibule frame SC3 calls for Hollow Metal on the screen schedule but door 102A is calling for aluminum frame and door on door schedule above. Please confirm if it's hollow metal or aluminum frame and door?

Answer 45

The material for screen SC3 is to be aluminum. Refer to Item #7.

Question 46

For SG-1/SG-2 spandrel glass, I would interpret this detail below as single spandrel with backpan. Can you confirm if they are, or are they sealed units with backpan?



Answer 46

Spandrel Glass SG-1 / SG-2 is to be a single spandrel with an insulated back pan. Refer to items 2 and 5.

Question 47

Are all windows are curtain wall based on detail above and none are bullnose 970 series as mentioned on the specs?

Answer 47

As per the window frame types/schedule, window W9 is to be an aluminium frame (970 series).

Question 48

Are all windows are fixed, and non-operable? 1/A3.00 has a note "Firefighting Access", please clarify what it means.

Answer 48

All windows are fixed and non-operable. The note "Firefighting Access" just denoted a window that, when broken, is of sufficient size to satisfy the building code requirement for fire fighting access to the building.

Question 49

Fire rated glass are ceramic and not Georgian Wire Glass, correct?

Answer 49

All fire rated glass is to be ceramic. Refer to item #5.

Question 50

Please confirm Heavy Duty Asphalt detail on Drawing A1.20 is to read a total thickness of 720mm instead of 550mm.

Answer 50

Overall thickness of the Heavy Duty asphalt is to be 720mm.

Question 51

It is unclear whether excavated native backfill is suitable for site servicing backfill under proposed pavement areas (ie, the zone from 300mm above top of pipe to subgrade) . Please confirm whether bidders are to backfill site servicing with excavated native soils or granular B.

Answer 51

Native fill can be used for trench backfill if it is suitable.

Question 52

There is a large landscape area north of the "heavy duty asphalt fire truck turn around area" with an annotation stating "Area to be regraded to promote drainage toward proposed asphalt roadway". Will it be permissible to use topsoil as fill in this area to achieve the proposed grades indicated per C102 & C103?

Answer 52

Topsoil can be used to meet grades within landscaped areas.

Question 53

Section 02210 "Site Grading", 3. "Grading" note 5 shows rough grading under grassed areas as 150mm below finish grades. Landscape drawing L-1 has annotations pointing to the grassed areas with a requirement on 200mm of topsoil. Please confirm depth what bidders are to assume as depth of topsoil in grassed areas.

Answer 53

Grassed areas to receive 200mm of topsoil as per the landscape drawings.

Question 54

1. Will any work pertaining to work inside the regional flood line of Ex. Watercourse SMT-1 such as the installation of a temporary crossing and/or the work involved to install the 6000mm x 1500mm precast box culvert be subject to any kind of a "in-water working window"? Do you have a permit with the conservation authority?

Answer 54

A Conservation Authority Permit has been issued for the work. In Creek works are subject to the "in-water working window".

Question 55

Drawing C108 says that the dewatering pumps are to be sized by others. Is there any information of flows that can be provided?

Answer 55

Refer to question #42.

Question 56

When is the anticipated start date of this project?

Answer 56

It is anticipated that the contractor will start onsite mid November 2023 (November 15).

Question 57

Specification says to stock pile topsoil onsite and to retain top soil onsite. Please provide area where topsoil is to be stockpiled?

Answer 57

Location of topsoil stockpile is to be coordinated with architect onsite after tender award.

Question 58

The Geo –technical report is dated October 9, 2014. Is this report currently accurate? Has any work onsite occurred such as stripping, etc. that would affect the findings in the borehole logs?

Answer 58

The only work that has occurred onsite has been to the south of the creek. No work has been performed on the north side of the creek where the crematorium is located.

Question 59

There is no analytical testing on the soils. Are we to assume that all excess soil is to remain onsite and if so where will it be stockpiled?

Answer 59

Refer to question #57.

Question 60

Specifications call for clear stone to the underside of the building slab and exterior concrete slabs and the structural and architectural drawing calls for granular limestone. Please advise which is correct?

Answer 60

For the underside of slabs on grade clear crushed stone is to be used as indicated in the specification and drawings S0.0,

Question 61

Is there a comms spec, or a specific structured cabling system manufacturer required? Are patch cables required? If so, what quantities and lengths? Can all work be done during regular business hours?

Answer 61

Refer to electrical addendum E4

Question 62

I can't find the distributor for **(PT) American Olean, Graniti Fiandre - Urban Active, 24"x24", Slate Finish** I have contacted Daltile (distributor for American Olean) and Shnier (distributor for Graniti Fiandre) and they both said it's not theirs. Can you clarify with the designer please?

Answer 62

Refer to Item #8

Question 63

The room Finish Schedule show The Circulation room 110 to have epoxy floor and the Retort room 121 to have sealed concrete – Drawing A 2.00 show these rooms to be the same room (see below) – can you please identify which floor type is to be in this area?

Answer 63

Refer to Item #9

End of Addendum No. 4

**Holy Family Cemetery
Crematorium Building
2523 Lower Base Line Road, Milton ON**

October 20, 2023

ELECTRICAL ADDENDUM #E3

NRG Consultants Inc.

This addendum issued before the closing of tenders, comprises clarifications and changes to the specifications and drawings and is hereby made a part thereof.

Questions & Responses

- Q1. Please provide further information and detail regarding the feeder from the existing Administration Basement Utility Room 002 to the 200A disconnect switch in the Crematorium Building. We need the following clarified and more information to be provided to accurately quote:*
- a) Who is responsible for the tie-in of this feeder to the existing equipment in the Administration Basement Utility Room 002? If by Electrical Contractor, we need to know what we are tying into. Is it during afterhours? Do we need to supply and install an over-current device in existing equipment? If so, we require photos and information of the existing equipment.*
 - b) No detail or information is provided on how the feeder will enter the existing Administration Building and what routing is required inside the building to the Basement Utility Room 002. Please provide this information as Electrical Contractor cannot quote this based on assumptions.*
 - c) Please confirm the distance provided of 2,100 ft. on the Site Plan on Drawing E02 is for the underground duct bank section only from building to building. Confirm this distance does not include any additional conduit and wire required from underground to electrical equipment in the buildings*
- R1.**
- a) Tie-in of feeder to the existing equipment in the Administration Building Basement Utility Room 002 is by the Electrical Contractor. Tie-in will be to an existing 200A-3P breaker in existing 800A Square D Switchboard PP-1. Tie-in connection may be performed during regular day-time hours. A new over-current device is not required.
 - b) From the existing Administration Building Basement Utility Room 002, five (5) conduit stub-outs to match requirements of Underground Duct Bank Section C-C are provided through the basement wall terminating underground at an exterior point 2000mm to the west of the basement wall. Within the existing Administration Building Basement Utility Room 002 allow for two (2) 3000mm runs of 100mm (4") EMT conduit c/w power cables from the stub-outs to existing Switchboard PP-1.
 - c) The distance provided of 2,100 ft. on the Site Plan on Drawing E03 is from the Administration Building Basement Utility Room 002 exterior conduit stub-outs to the Crematorium Building Elect / Mech Room 117 exterior wall only.

- Q2. *Please confirm all EMT conduit fittings inside the building must be watertight per specification.*
- R2. All EMT conduit fitting inside both building shall be watertight type. Set-screw type are not permitted.
- Q3. *Please confirm supply and install of all hand dryers is not part of the electrical scope of work.*
- R3. All hand dryers shown on the drawings are to be supplied and installed by the Electrical Contractor.
- Q4. *Please clarify that Electrical Contractor to include for all communication rough-in which includes conduit stub-up to ceiling space only. Confirm no conduit is required in the ceiling space and J-hooks are not required. If, so provide what is required and to what location.*
- R4. All data and telephone outlets shown on the drawings to consist of recessed outlet box and conduit stub-up into ceiling space only. No above ceiling conduits or J-hooks are required.
- Q5. *Please clarify that Electrical Contractor to include for all security rough-in which includes conduit stub-up to ceiling space only. Confirm no conduit is required in the ceiling space and J-hooks are not required. If, so provide what is required and to what location.*
- R5. All security device outlets shown on the drawings to consist of recessed outlet box and conduit stub-up into ceiling space only. No above ceiling conduits or J-hooks are required.
- Q6. *Electrical specification speaks to wiremold to be installed in exposed areas. Electrical drawings do not show any wiremold or what locations require wiremold. Please revise electrical drawings to show wiremold in every location that it is required. This includes all vertical and horizontal runs, please also provide a detail showing how the design is intended with transitions to conduit.*
- R6. Conduits to be concealed in all Public Areas. Surface wiremold may be used in Public Areas only if concealed conduits are not possible. Architect's and Engineer's prior approval required before installation.
- Q7. *Electrical Contractor needs further detail including a detail drawing showing how the duct bank and all conduits are transitioning from underground to inside of Administration Building. We also required information on the existing building exterior for penetrations to enter the building. A detailed drawings is required to show routing inside The Administration Building from penetration location to existing Panel PP-1.*
- R7. Refer to response R1 (b) above

- Q8. *Electrical Contractor requires pictures and information of the existing Panel PP-1 and existing manufacturer information to quote the correct 200A-3P breaker.*
- R8. Refer to response R1 (a) above.
- Q9. *Electrical Contractor needs clarification if all work in Administration Building, including power shut-down, is to be done during regular business hours.*
- R9. Refer to response R1 (a) above.
- Q10. *Duct Bank Note #8 on Drawing E02 says to fix spacers to avoid floating during concreting. However, in the Section, it is clean sand filling. Please confirm whether we go for sand filling or concreting?*
- R10. Clean sand filling is to be used.
- Q11. *Can we use directional drilling with HDPE conduits in highlighted area, instead of directional boring with steel casing? Directional drilling is only HDPE conduits, while directional boring is steel casing has conduits. Could you please provide us with more information.*
- R11. Directional drilling with HDPE conduits is preferred.
- Q12. *The 200A feeder shown to feed the new Crematorium Building from the Administration Building Basement Utility Room is not sized properly. This run will require an additional parallel run which will increase our duct bank size as shown and we will need to add an additional spare conduit.*
- R12. Refer to Drawing E02, Underground Duct Bank Section C-C: Revise Duct #2 use for Power Service Cables. (No spare 100mm duct required).
Refer to Drawing E04, Conduit & Wire Schedule: Revise Item # 1 to 8 - #350MCM RWU90 Copper + GND in 2 – 100mm (4”) Dia. PVC DB-II underground ducts. (ie. Parallel cable run).
Refer to Drawing E04, Conduit & Wire Schedule: Revise Item # 2 to 8 - #350MCM RWU90 Copper + GND in 2 – 76mm (3”) Dia. EMT conduits. (ie. Parallel cable run).
- Q13. *We are also concerned with the difficulty of pulling the feeders from the second manhole to the new Crematorium Building as this is a great distance. We propose installing an additional 1 – 2 manholes along the roadway leading to the building from the second manhole. This will decrease the distance of the greatest pull.*
- R13. Provide one (1) additional manhole between the existing Administration Building and the first manhole shown. Provide two (2) additional manholes between the second manhole shown and the new Crematorium Building.

Q14. Will splices of the building feeder done inside the manholes be accepted? If so, are there any specific requirements for these splices?

R14. Splices will not be accepted.

Q15. Will aluminum cabling be accepted for all feeders above 100A?

R15. All cables to be copper.

General

1. Drawing E01, Electrical Notes, Item #19 – Electrical Cash Allowances: Revise two (2) items as follows:
 1. \$50,000 For Connection of Power Service.
 5. \$75,000 For Possible Additional Electrical Work.

**Holy Family Cemetery
Crematorium Building
2523 Lower Base Line Road, Milton ON**

October 23, 2023

ELECTRICAL ADDENDUM #E4

NRG Consultants Inc.

This addendum issued before the closing of tenders, comprises clarifications and changes to the specifications and drawings and is hereby made a part thereof.

Questions & Responses

- Q1. (a) Is there a Communications Specification, or a specific Structured Cabling System Manufacturer required? Are patch cables required? If so, what quantities and lengths?*
- (b) Can all work be done during regular business hours?*
- R1. (a) There is no specific Communications Specification nor specific Structured Cabling System Manufacturer. Electrical Contractor to provide data outlet boxes c/w conduits to T-Bar ceiling space in locations shown on the drawings. Data jacks, Cat. 6 wiring, terminations, testing and patch cables by Owner's Data Subcontractor.
- (b) All work can be performed during regular business hours.

END OF ELECTRICAL ADDENDUM #E4

NRG Consultants Inc.



S. LLEWELLYN & ASSOCIATES LIMITED
CONSULTING ENGINEERS

Stormwater Management Report

HOLY FAMILY CATHOLIC CEMETERY PHASE 2 (CREMATORIUM BUILDING)

THE CATHOLIC CEMETERIES
OF THE DIOCESE OF HAMILTON

TOWN OF MILTON

Revised: July 2022
June 2021

SLA File: 13084

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1.0 INTRODUCTION AND BACKGROUND

1.1 OVERVIEW

S. Llewellyn & Associates Limited has been retained by The Catholic Cemeteries of the Dioceses of Hamilton to provide consulting engineering services for the proposed Phase 2 portion of the Holy Family Catholic Cemetery development at the corner of Regional Road No. 25 and Lower Baseline Road in the Town of Milton (see Figure 1.0 for location plan). This report will outline the stormwater management strategy for the proposed development.

The proposed Phase 2 portion of the development consists of constructing one (1) single storey building for use as a crematorium facility. Additionally, there will be an associated asphalt parking lot with concrete curbing/sidewalks, landscaped areas and an asphalt roadway which will connect to the previously completed portion of the cemetery.

This Stormwater Management Report will provide detailed information of the proposed servicing scheme for this development. Please refer to the site engineering plans prepared by S. Llewellyn and Associates Limited and the site plan prepared by Grguric Architects for additional information.

1.2 BACKGROUND INFORMATION

The following documents were referenced in the preparation of this report:

- Ref. 1: MOE Stormwater Management Practices Planning and Design Manual (Ministry of Environment, March 2003)
- Ref. 2: Guidelines for Site Plan Approval (Town of Milton, January 2020)
- Ref. 3: Stormwater Management Report for the Proposed Developments at Regional Road No. 25 and lower baseline Road, Milton, Ontario (AMEC Environmental, February 2012)
- Ref. 4: Hydrogeological Investigation Proposed Holy Family Catholic Cemetery (First Phase) Part of Lot 1 Concession 2, Town of Milton, Ontario (Terraprobe, May 2014)
- Ref. 5: Erosion & Sediment Control Guidelines for Urban Construction (December 2006)



Figure 1.0 – Location Plan

2.0 STORMWATER MANAGEMENT

The following stormwater management (SWM) criteria will be applied to the site, in accordance with the Town of Milton:

Quantity Control

The stormwater discharge rate from the proposed site shall be controlled to the discharge rate that was previously modeled in the “Stormwater Management Report for the Proposed Cemetery Developments at Regional Road No. 25 and Lower Baseline Road, Milton, Ontario” (October 2012), prepared by AMEC Environmental for the correlating catchment area.

Quality Control

The stormwater runoff from the proposed parking areas on site must meet Level 1 (Enhanced) stormwater quality control (80% TSS removal, 90% average annual runoff treatment). Quality control is not warranted for the asphalt road system on site as vehicular traffic is generally limited. These criteria are in accordance with the “Stormwater Management Report for the Proposed Cemetery Developments at Regional Road No. 25 and Lower Baseline Road, Milton, Ontario” (October 2012), prepared by AMEC Environmental.

Erosion Control

Erosion and sediment control measures will be implemented in accordance with the standards of the Town of Milton.

3.0 EXISTING CONDITIONS

In the existing condition, the 4.1-hectare area comprising the Phase 2 portion of the site consists entirely of agricultural land. The site is bound by Regional Road No. 25 to the north, Lower Base line Road to the east, and existing agricultural lands to the west and south. Discharge from this section of the site sheet drains towards the watercourse SMT-4 previously defined in the 2009 report titled “Meander Belt Width Assessment” completed by Parish Geomorphoc for this development. This watercourse ultimately discharges to Sixteen Mile Creek.

One catchment area, Catchment 101, has been identified in the existing condition. Catchment 101 represents the drainage area for the entire Phase 2 portion of the site which discharges to watercourse SMT-4. See Table 3.1 below and the Pre-Development Drainage Area Plan in Appendix A for details.

Catchment ID	Description	Area (ha)	Percent Impervious	Run-off Coefficient
101	Sheet drainage to Watercourse SMT-4	4.1	0%	0.25

An analysis was performed on Catchment 101 using the SWMHYMO hydrologic modeling program developed by J.F. Sabourin & Associates for the 2-year to 100-year design storms. In order to stay consistent with the SWMHYMO modeling previously completed by AMEC, the same Town of Milton 12 hr SCS storm files were utilized in the SWMHYMO modeling carried out in this report. Additionally, the same CN values and weighted initial abstraction calculations from the AMEC stormwater management report were also utilized. A summary of the results can be found in Table 3.2 and detailed SWMHYMO input/output information can be found in Appendix C.

Storm Event	Catchment 101 Discharge (m ³ /s)
2-Yr Event	0.175
5-Yr Event	0.308
10-Yr Event	0.403
25-Yr Event	0.526
50-Yr Event	0.619
100-Yr Event	0.713

4.0 PROPOSED CONDITIONS

The proposed Phase 2 portion of the development consists of constructing one (1) single storey building for use as a crematorium facility. Additionally, there will be an associated asphalt parking lot with concrete curbing/sidewalks, landscaped areas and an asphalt roadway which will connect to the previously completed portion of the cemetery. Furthermore, this catchment also includes the future development of a mausoleum building with an associated asphalt parking lot with concrete curbing/sidewalks and landscaped areas. It is proposed to service the site with a private storm sewer system designed and constructed in accordance with the standards and specifications of the Town of Milton.

SWMHYMO modeling for the catchment area encompassing Phase 2 was previously completed as part of the “Stormwater Management Report for the Proposed Cemetery Developments at Regional Road No. 25 and Lower Baseline Road, Milton, Ontario” (October 2012), prepared by AMEC Environmental. The discharge rates for the 2-100 year and regional storm events for Catchment area 201 have been controlled to the discharge rates for the correlating catchment area in the AMEC Stormwater Management Report. The detailed SWMHYMO input/output file for Catchment B1d can be found in Appendix B with the summary results in Table 4.1 below:

Storm Event	Catchment B1d Controlled Discharge (m ³ /s)	Required Storage (m ³)
2-Yr	0.103	482
5-Yr	0.160	767
10-Yr	0.194	983
25-Yr	0.227	1266
50-Yr	0.249	1484
100-Yr	0.269	1709
Regional Storm	0.467	2231

One catchment area, Catchment 201, has been identified in the proposed condition. Catchment 201 represents the drainage area for the proposed development which will be captured and controlled by the proposed storm sewer system & detention pond before ultimately discharging to the existing watercourse SMT-4. See Table 4.2 below and the Post-Development Drainage Area Plan in Appendix A for details.

Catchment ID	Description	Area (ha)	Percent Impervious	Run-off Coefficient
201	Controlled discharge to watercourse SMT-4	4.1	36%	0.49

4.1 WATER QUANTITY CONTROL

It is proposed to apply quantity control measures to the runoff from Catchment 201 by means of a 300mm \varnothing orifice pipe to restrict discharge from the site to the specified discharge rate in the Stormwater Management Report completed by AMEC Environmental. Refer to the Grading & Servicing Plan for the orifice location.

With the installation of on-site quantity control measures for Catchment 201, it will be required to provide stormwater storage during storm events up to and including the 100-year event. To provide the required storage, a dry detention pond has been graded at the northeast corner of the property, which will provide the required volume of stormwater storage. It should be noted that this detention pond is in accordance with the pond proposed in the Stormwater Management Report completed by AMEC for the corresponding catchment area. Furthermore, as noted in the May 2014 hydrogeological report prepared by Terraprobe, groundwater on site is generally found at approximately 1.0m below the ground surface; however, because the site consists of low permeability glacial till which will act as a natural liner there will be no significant effect on groundwater levels or groundwater quality due to the construction of the proposed pond. Furthermore, due to the native soil's impermeability characteristics pond operating levels are also not anticipated to be affected by groundwater. Details of the proposed pond can be found on the Grading & Servicing Plan. The stage-storage-discharge characteristics can be seen in Table 4.3 below and Appendix A for details.

Elevation (m)	Storage (m ³)	Discharge (m ³ /s)
177.30 (Bottom of Pond)	0	0.0033
177.50 (0.2m Depth)	310	0.0512
177.70 (0.4m Depth)	646	0.1169
177.90 (0.6m Depth)	1009	0.1650
178.10 (0.8m Depth)	1400	0.2014
178.30 (1.0m Depth)	1820	0.2322
178.50 (Top of Pond)	2270	0.5311

An analysis was performed on the proposed condition site using the SWMHYMO hydrologic modeling program to determine the volume of stormwater storage that is required during the 2-year to 100-year Town of Milton 12 hr SCS design storm and the regional storm event. As noted in section 3.0 to stay consistent with the AMEC Stormwater Management Report the same storm files, CN values and weighted initial abstractions have been utilized. A summary of the results can be found in Table 4.4 and detailed SWMHYMO input/output information can be found in Appendix C.

Storm Event	Catchment 201 Controlled Discharge (m ³ /s)	Allowable Discharge ¹ (m ³ /s)	Required Storage (m ³)
2-Yr	0.090	0.103	501
5-Yr	0.138	0.160	796
10-Yr	0.165	0.194	1011
25-Yr	0.192	0.227	1294
50-Yr	0.210	0.249	1510
100-Yr	0.226	0.269	1732
Regional Storm	0.454	0.467	2194

¹ Allowable discharge = Discharge Rate from Table 4.1

This analysis determined the following:

- The 2-year to 100-year and regional post development controlled discharge will not exceed the allowable discharge rate computed by AMEC with the installation of a 300mmØ orifice pipe.
- Catchment 201 will require 1732m³ of stormwater storage during the 100-year event, which can be accommodated by the proposed dry pond, having a volume of 2270m³ at the top of pond elevation.
- The proposed pond is in accordance with the “Stormwater Management Report for the Proposed Cemetery Developments at Regional Road No. 25 and Lower Baseline Road, Milton, Ontario” (October 2012), prepared by AMEC Environmental.
- The fill generated from the proposed pond will be distributed across Phase 2 to bring the site up to the proposed finished grades.

4.2 FLOODPLAIN MODELLING

As part of the proposed asphalt road system, it is required to cross the existing watercourse SMT-1. The proposed crossing of STM-1 will be completed using a 6000mm x 1500mm concrete box culvert. Furthermore, the proposed box culvert will be counter-sunk by 15% (225mm) in accordance with the recommendations from Conservation Halton. The HEC-RAS modeling completed as part of the AMEC Stormwater Management Report was revised to analyze the effect of the culvert crossing on SMT-1 upstream of the culvert.

The 6000mm x 1500mm box culvert exceeds the specifications set out in the AMEC report which states that the soffit of the culvert requires 0.3m freeboard from the 25-year flood elevation. The proposed culvert is not overtopped during any storm event and the minor flood plain increase immediately upstream of the culvert has been reflected on the

updated drawings. Furthermore, the HEC-RAS model shows that there will be no increase in the regional flood line elevation at the development site property limits. Please refer to the Floodplain Memo in Appendix E for further details.

4.3 WATER QUALITY CONTROL

The proposed development is required to achieve an “Enhanced” (80% TSS removal) level of water quality protection. To achieve this criteria, discharge from the parking area surrounding the proposed crematorium building will be subject to treatment from a HydroStorm oil/grit separator before ultimately discharging to the private storm sewer system. The HydroStorm sizing software was used to determine the required size of oil/grit separator unit for the site. It was determined that a HydroStorm HS10 will provide 85% TSS removal and 96% average annual runoff treatment, which satisfies the requirements for an “Enhanced” level for quality control. Refer to the Hydroworks Sizing Summary Report in Appendix D for details.

HydroStorm units require regular inspection and maintenance as per the manufacturer’s specifications to ensure the unit operates properly. See HydroStorm Maintenance Manual in Appendix D for details.

Quality control is not warranted for the asphalt road system on site as vehicular traffic is generally limited. These criteria are in accordance with the “Stormwater Management Report for the Proposed Cemetery Developments at Regional Road No. 25 and Lower Baseline Road, Milton, Ontario” (October 2012), prepared by AMEC Environmental.

5.0 SEDIMENT AND EROSION CONTROL

In order to minimize erosion during the grading and site servicing period of construction, the following measures will be implemented:

- Install silt fencing along the outer boundary of the site to ensure that sediment does not migrate to the adjacent properties;
- Install sediment control (silt sacks) in the proposed catchbasins as well as the nearby existing catchbasins to ensure that no untreated runoff enters the existing conveyance system;
- Stabilize all disturbed or landscaped areas with hydro seeding/sodding to minimize the opportunity for erosion.

To ensure and document the effectiveness of the erosion and sediment control structures, an appropriate inspection and maintenance program is necessary. The program will include the following activities:

- Inspection of the erosion and sediment controls (e.g. silt fences, sediment traps, outlets, vegetation, etc.) with follow up reports to the governing municipality; and
- The developer and/or his contractor shall be responsible for any costs incurred during the remediation of problem areas.

Prior to completion of construction, the following permanent erosion measure will be implemented:

- Place river stone as sized on the drawings at the inlet and outlet of the culvert and at the pond outlet to provide sufficient energy dissipation to prevent erosion of the watercourse and adjacent lands. Detailed stone sizing calculations are provided in Appendix A.

For details on the proposed erosion and sediment control for the proposed site, see the Grading & Servicing Plan included in the engineering drawings.

6.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the information provided herein, it is concluded that the proposed Phase 2 development of Holy Family Cemetery can be constructed to meet the requirements of the Town of Milton. Therefore, it is recommended that:

- The development be graded and serviced in accordance with the Grading & Servicing Plan prepared by S. Llewellyn & Associates Limited;
- A 300mmø orifice pipe be installed as per the Grading & Servicing Plan and this report to provide adequate quantity control for the proposed site;
- A dry detention pond be graded as per the Grading & Servicing Plan and this report to provide sufficient stormwater surface storage for the proposed development;
- A HydroStorm HS10 oil/grit separator be installed as per the Grading & Servicing Plan and this report to provide efficient stormwater quality control for the proposed development;
- Erosion and sediment controls be installed as described in this report to meet Town of Milton requirements;

We trust the information enclosed is satisfactory. Should you have any questions please do not hesitate to contact our office.

Prepared by:

S. LLEWELLYN & ASSOCIATES LIMITED



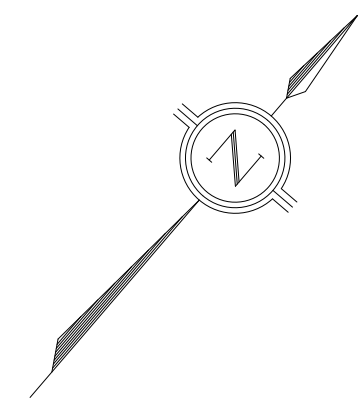
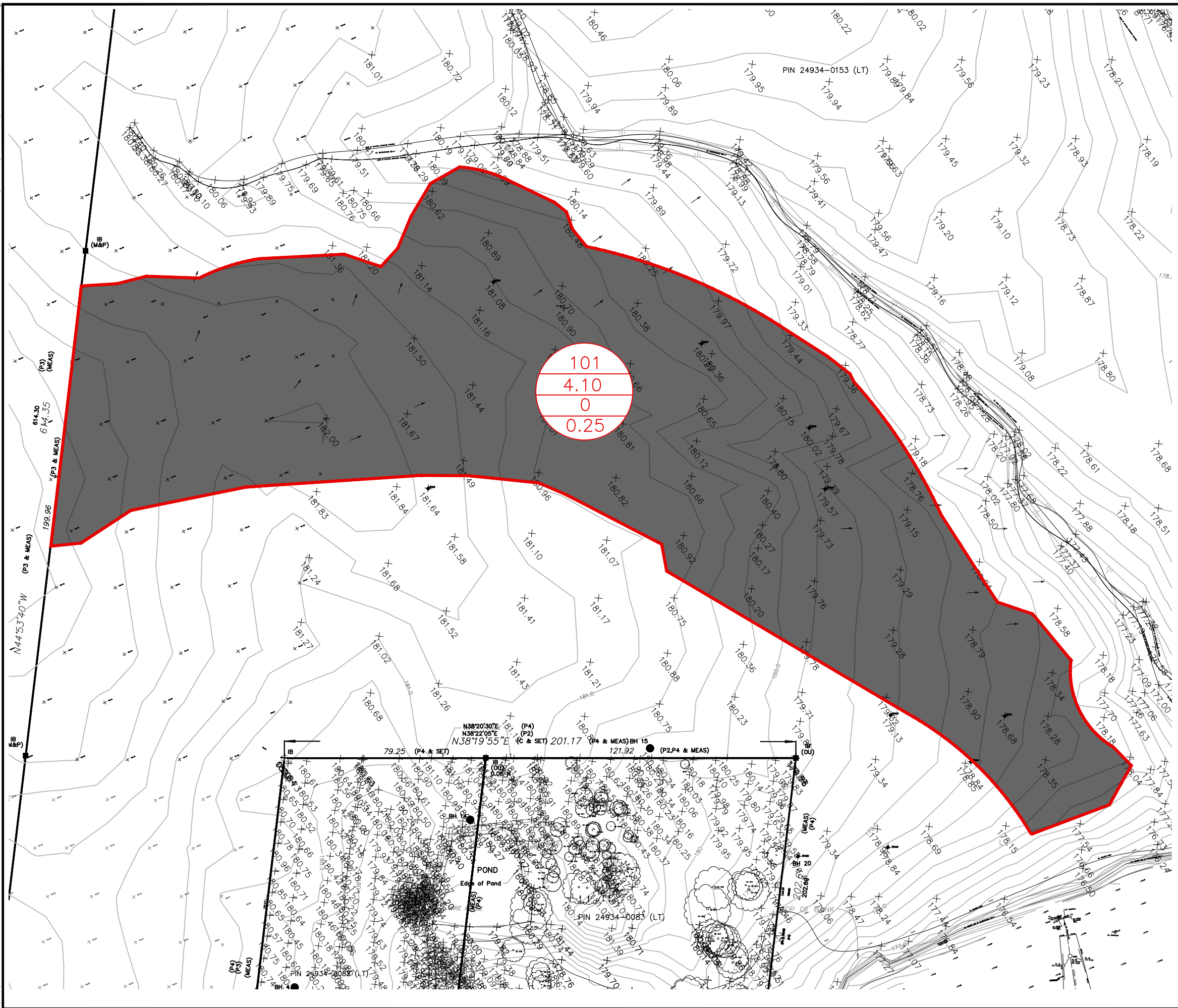
S. DeGrow, Dipl. T.



S. Frankovich, P.Eng.

APPENDIX A

STORMWATER MANAGEMENT INFORMATION




LEGEND

- PERVIOUS AREA
- | |
|------|
| 201 |
| 0.39 |
| 11 |
| 0.32 |

 DRAINAGE AREA I.D.
DRAINAGE AREA (ha)
PERCENT IMPERVIOUS
RUNOFF COEFFICENT
- DIRECTION OF SHEET FLOW

FIGURE 1.0
PRE-DEVELOPMENT STORM
DRAINAGE AREA PLAN
 SCALE: 1:1500

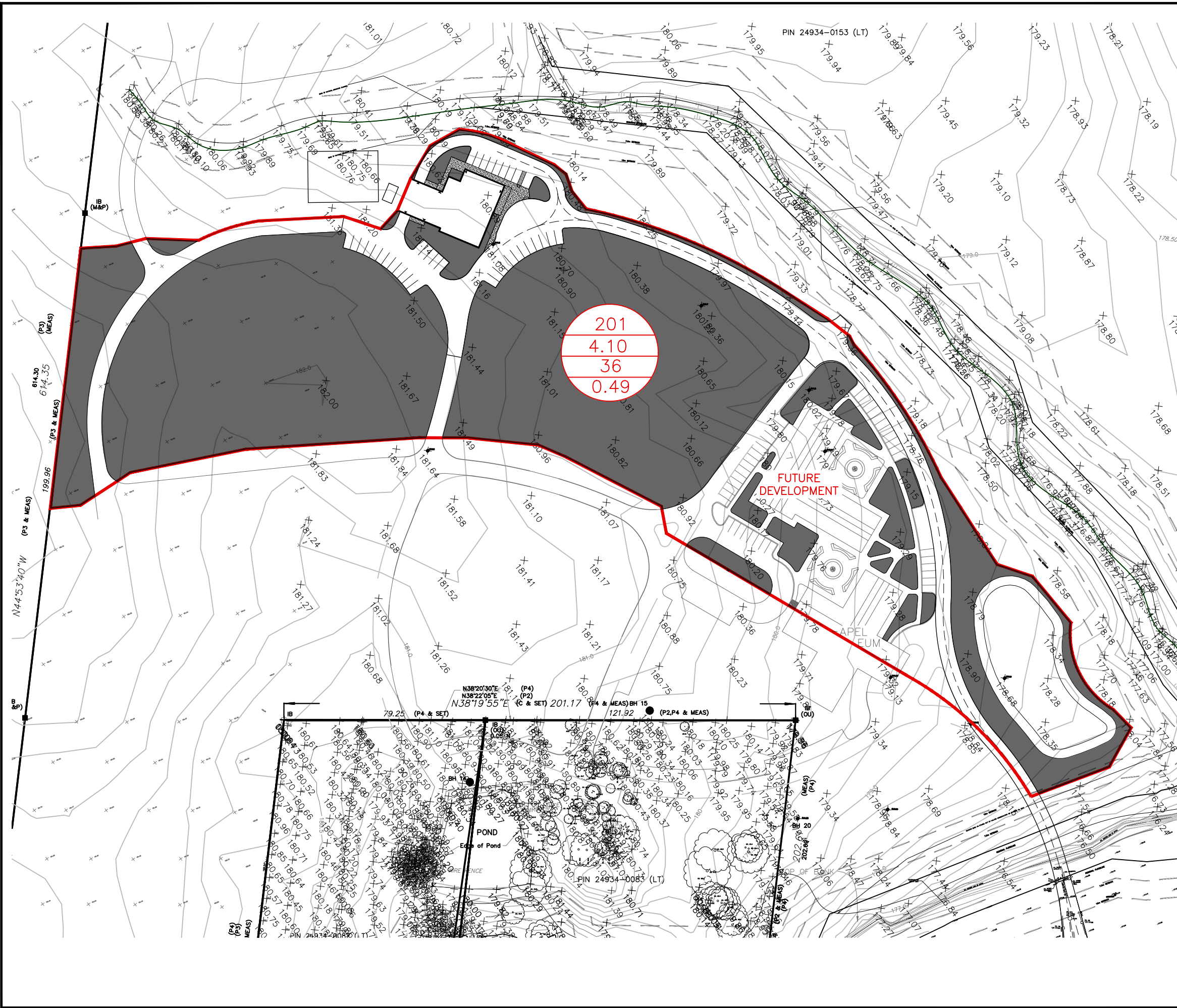
PROJECT: HOLY FAMILY CATHOLIC CEMETERY, MILTON
 PROJECT No.: 13084



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LEGEND


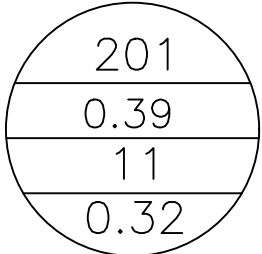

-  PERVIOUS AREA
- 
 - 201 DRAINAGE AREA I.D.
 - 0.39 DRAINAGE AREA (ha)
 - 11 PERCENT IMPERVIOUS
 - 0.32 RUNOFF COEFFICIENT
-  DIRECTION OF SHEET FLOW

FIGURE 2.0
POST-DEVELOPMENT STORM
DRAINAGE AREA PLAN
 SCALE: 1:1500
 PROJECT: HOLY FAMILY CATHOLIC CEMETERY, MILTON
 PROJECT No.: 13084

Rating Table Report 300mm Orifice Pipe

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	177.30	178.50	0.05 m

HW Elev. (m)	Discharge (m ³ /s)
177.30	0.00332
177.35	0.01071
177.40	0.02162
177.45	0.03539
177.50	0.05123
177.55	0.06822
177.60	0.08541
177.65	0.10194
177.70	0.11690
177.75	0.12997
177.80	0.14239
177.85	0.15413
177.90	0.16499
177.95	0.17481
178.00	0.18412
178.05	0.19297
178.10	0.20144
178.15	0.20956
178.20	0.21738
178.25	0.22493
178.30	0.23224
178.35	0.23932
178.40	0.24619
178.45	0.25288
178.50	0.25940

Culvert Calculator - 300mm Orifice Pipe

Solve For: Discharge

Culvert
 Discharge: 0.25940 m³/s
 Maximum Allowable HW: 178.50 m
 Tailwater Elevation: 0.00 m

Inverts
 Invert Upstream: 177.24 m
 Invert Downstream: 177.23 m
 Length: 2.50 m
 Slope: 0.004000 m/m

Section
 Shape: Circular
 Material: Corrugated HDPE (Smooth In)
 Size: 300 mm
 Number: 1
 Mannings: 0.012

Headwater Elevations
 Maximum Allowable: 178.50 m
 Computed Headwater: 178.50 m
 Inlet Control: 178.50 m
 Outlet Control: 178.45 m

Inlet
 Entrance: Beveled ring, 33.7° bevels
 Ke: 0.20

Exit Results
 Discharge: 0.25940 m³/s
 Velocity: 3.56 m/s
 Depth: 0.30 m

Buttons: OK, Cancel, Output..., Solve, Export..., Help

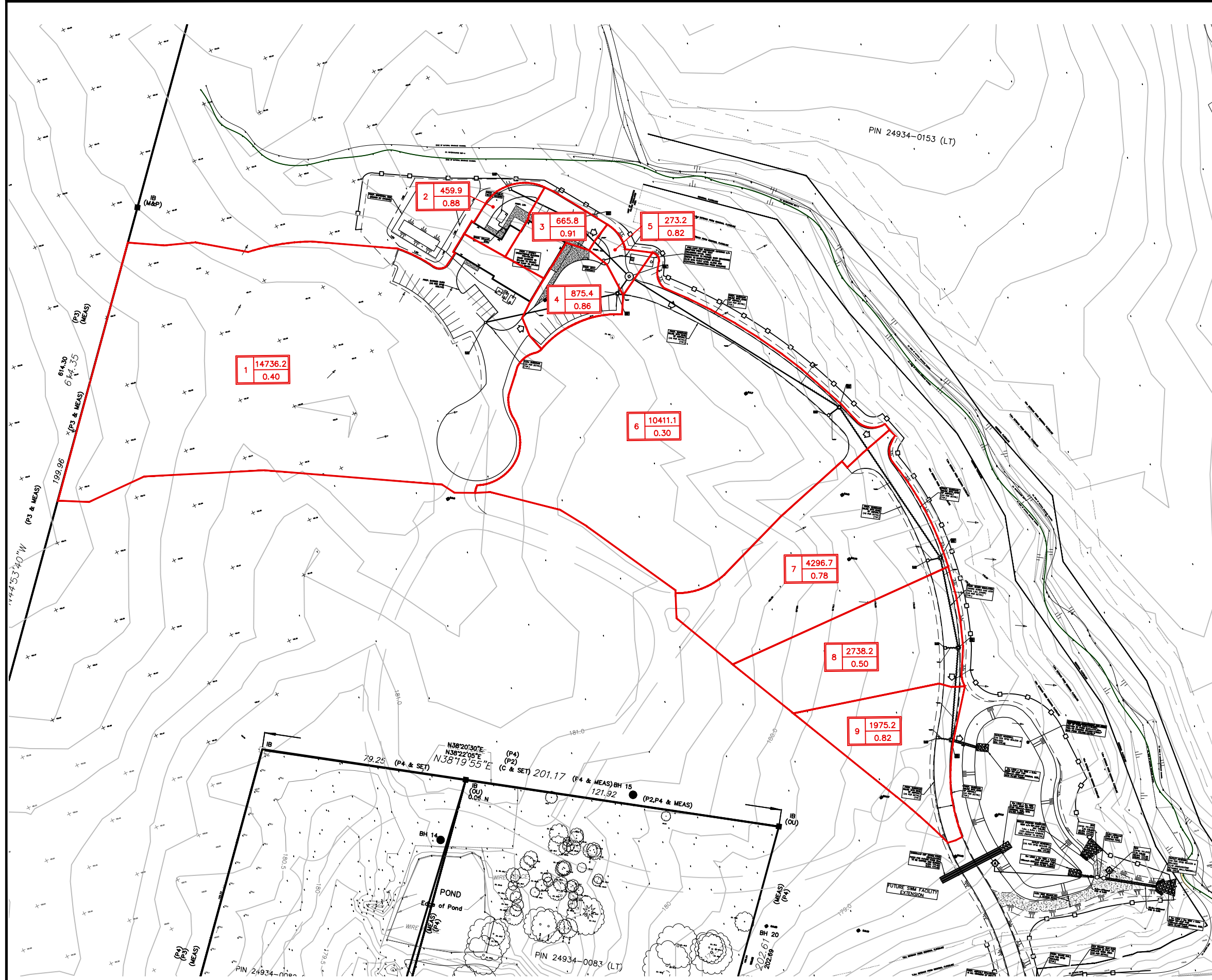
STAGE-STORAGE-DISCHARGE CALCULATIONS

Outlet Device (Quantity)

Type: Orifice Pipe 1
 Diameter (mm) 300
 Area (m²) 0.07069
 Invert Elev. (m) 177.27
 C/L Elev. (m) 177.42
 Disch. Coeff. (C_d) 0.8
 Discharge (Q) = C_d A (2 g H)^{0.5}
 Number of Orifices: 1

Type: Broad crested overflow weir
 Sill Elevation (m) 178.35
 Length (m) 2.8
 Discharge (Q)= 1.67 L H^{1.5}

	Elevation m	Pond Volumes			Outlet No. 1		Outlet No. 2		Total Discharge m ³ /s
		Pond Area m ²	Pond Increm. Volume m ³	Cumulative Tank Volume m ³	H m	Discharge m ³ /s	H m	Discharge m ³ /s	
Orifice Invert	177.27	0	0	0	0.000	0.0000			0.0000
Bottom of Pond	177.30	1491	0	0	0.030	0.0033			0.0033
0.10m Depth of ponding	177.40	1548	152	152	0.130	0.0216			0.0216
0.20m Depth of ponding	177.50	1613	158	310	0.230	0.0512			0.0512
0.30m Depth	177.60	1678	165	475	0.330	0.0854			0.0854
0.40m Depth of Ponding	177.70	1745	171	646	0.430	0.1169			0.1169
0.50m Depth of Ponding	177.80	1814	178	824	0.530	0.1424			0.1424
0.60m Depth of Ponding	177.90	1884	185	1009	0.630	0.1650			0.1650
0.70m Depth of Ponding	178.00	1955	192	1200	0.730	0.1841			0.1841
0.80m Depth	178.10	2027	199	1400	0.830	0.2014			0.2014
0.90m Depth of Ponding	178.20	2101	206	1606	0.930	0.2174			0.2174
1.00m Depth of Ponding	178.30	2176	214	1820	1.030	0.2322			0.2322
Weir Sill Elevation	178.35	2214	110	1930	1.080	0.2393	0.000	0.0000	0.2393
1.10m Depth of Ponding	178.40	2252	112	2041	1.130	0.2462	0.050	0.0523	0.2985
Top of Pond	178.50	2330	229	2270	1.230	0.2594	0.150	0.2717	0.5311



LEGEND		DRAINAGE AREA (m ²)	RUNOFF COEFFICIENT
DRAINAGE AREA I.D.	13	5000.9	0.25

PROPOSED CONDITION
 STORM SEWER DRAINAGE
 AREA PLAN
 SCALE: 1:1500

PROJECT: HOLY FAMILY CATHOLIC CEMETERY, MILTON
 PROJECT No.: 13084



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RIVER STONE SIZING WITHIN SMT-1

River Stone sizing calculations based on procedures outlined in Chapter 5 of the MTO Drainage Manual

RIVER STONE APRON HYDRUALIC CHARACTERISTICS

Consider a cross-section through the river stone apron immediately downstream of the culvert structure:

Bottom width (m) =	4.5
Long. Slope (%) (S) =	0.55
Side slope H:V =	3 : 1
Mannings 'n' =	0.030
Flow rate (m ³ /s) =	12.660 (Worst case scenario - Regional Storm)

Analysis results from HEC-RAS:

Depth of flow (m) =	1.28
Flow velocity (m/s) =	1.51
Area of flow (m ²) =	8.39
Wetted Perim. (m) =	6.77
Hydraulic Radius (m) (R) =	1.239

DETERMINE SHEAR STRESS ON CHANNEL BED AND BANK

Unit weight of water (γ) N/m³ = 9810

Mean boundary shear stress (τ_c):

$$\tau_c = \gamma R S = \quad \quad \quad \mathbf{67 \text{ N/m}^2}$$

Shear stress on channel bottom (τ_b):

$$\tau_b = K_b \tau_c = 1.43 \times 67 = \quad \quad \quad \mathbf{96 \text{ N/m}^2} \quad (\text{governs})$$

Shear stress on channel bank (τ_s):

$$\tau_s = K_{bk} \tau_c = 1.29 \times 67 = \quad \quad \quad \mathbf{86 \text{ N/m}^2}$$

Note: K_b & K_{bk} from Design Sheets 2.11 and 2.12 of the MTO Drainage Manual

DETERMINE RIVER STONE SIZING

Based on Equation 5.31 (MTO drainage manual), the critical shear stress on a particle can be determined by:

$$\tau_{cb} = 0.0642 \times D_{50} \times 9.81$$

$$\tau_{cb} = \quad \quad \quad 126$$

$$\tau_{cs} = K_{cs} \times \tau_{cb}$$

$$K_{cs} = 0.775$$

$$\tau_{cs} = 0.775 \times 126$$

Note: Equation 5.37 or Design Chart 2.14

$$\tau_{cs} = 97.65$$

$$\text{For } D_{50} \text{ (mm)} = \quad 200 \quad \tau_{cs} = \tau_{cb} \times 0.775 \quad \quad \quad \mathbf{98 \text{ N/m}^2} > \mathbf{96} \quad \dots \mathbf{O.K.}$$

Therefore, use minimum 200 mm riverstone ($D_{50} = 250$ mm) at all locations

APPENDIX B

AMEC SWMHYMO INPUT/OUTPUT INFORMATION

The Catholic Cemeteries
of the Diocese of Hamilton
Stormwater Management Report
Proposed Cemetery Development -
Regional Road 25 and Lower Baseline Road, Town of Milton
February, 2012



FUTURE LAND USE CONDITIONS WITH STORMWATER MANAGEMENT

SWM.dat

2 Metric units

```

*****
*# Project Name: [Holy Family Catholic Cemetery]   Project Number: [111063]
*# Date       : 08-16-2011
*# Modeller   : [C. Silvestri]
*# Company    : Philips Engineering Ltd
*# License #  : 3569108
*****

```

```

START          START=0.0 HRS  METOUT=2  NSTORM=1  NRUN=1
                MILSCS12.002

```

```

*
READ STORM      "STORM.001"

```

* Existing Conditions

```

* Subarea 103 - Existing Conditions Conditions Entering Property
CALIB NASHYD    ID= 1  NHYD=103  DT=5 min  AREA=42.1 ha  DWF=0.0 cms
                CN=86.0  IA=2.5 mm  N=3.0   Tp=0.399 hrs  END=-1

```

```

* Route through Channel 104
ROUTE CHANNEL   ID=2  NHYD=2104  IDIN=1  DT=5.0 min
                CHLGTH=440 m  CHSLP=1 %  FPSLP=1 %
                VSN=104  NSEG=3
                ROUGH DIST(m)
                0.04  59
                -0.03  60
                0.04  89

```

DIST(m)	ELEV(m)
0.0	179.5
18.0	178.5
59.0	178.0
59.5	177.7
60.0	178.0
89.0	178.5

```

* Subarea 104 - Creek Block Upstream of Proposed 5 acre Pond
CALIB NASHYD    ID= 3  NHYD=104  DT=5 min  AREA= 24.1 ha  DWF=0.0 cms
                CN=86.0  IA=2.5 mm  N=3.0   Tp=0.208 hrs  END=-1

```

```

ADD HYD         ID= 1  NHYD=1104  IDI= 3  IDII= 2

```

```

* Route through channel 105
ROUTE CHANNEL   ID=2  NHYD=2105  IDIN=1  DT=5.0 min
                CHLGTH=365 m  CHSLP=0.4 %  FPSLP=0.4 %
                VSN=105  NSEG=3
                ROUGH DIST(m)
                0.04  52
                -0.03  53
                0.04  100

```

DIST(m)	ELEV(m)
0.0	178.0
28.0	177.0
52.0	176.9
52.5	176.6
53.0	176.9
80.0	177.0
100.0	177.5

```

* Subarea 105 - Creek Block Upstream of Proposed Pond 2nd 5 acre pond
CALIB NASHYD    ID=3  NHYD=105  DT=5 min  AREA= 19.2 ha  DWF=0.0 cms
                CN=86.8  IA=2.5 mm  N=3.0   Tp=0.176 hrs  END=-1

```


SWM.dat

ADD HYD ID=1 NHYD=1105 IDI=3 IDII=2
 *
 ROUTE CHANNEL ID=2 NHYD=2106 IDIN=1 DT=5.0 min
 CHLGTH=385 m CHSLP=0.67 % FPSLP=0.67 %
 VSN=106 NSEG=3
 ROUGH DIST(m)
 0.04 77
 -0.03 78
 0.04 120

DIST(m)	ELEV(m)
0.0	176.0
20.0	175.5
32.0	175.0
58.0	174.5
77.0	174.5
77.5	174.2
78.0	174.5
102.0	175.0
120.0	175.5

*
 * Subarea 106 - Creek Block Upstream of Pond
 CALIB NASHYD ID= 3 NHYD=106 DT=5 min AREA= 15.3 ha DWF=0.0 cms
 CN=87.2 IA=2.5 mm N=3.0 Tp=0.168 hrs END=-1
 *
 ADD HYD ID= 1 NHYD=1106 IDI= 3 IDII= 2
 *
 * Subarea 107 - East drainage area for tributary
 CALIB STANDHYD ID= 3 NHYD=107 DT=5 min AREA= 15.27 ha
 XIMP=0.10 TIMP=0.17 DWF=0.0 cms LOSS=2 CN=88
 DPSP=2.5 mm SLPP=1.27 % LGP=717 MNP=0.250 SCP=0.0
 DPSP=1.57 mm SLPI=1.27 % LGI=100 MNI=0.017 SCI=0.0
 END=-1
 *
 ADD HYD ID=2 NHYD=1107 IDI=1 IDII=3
 *
 * Route Eastern Section of Tributary through Channel-108
 ROUTE CHANNEL ID=1 NHYD=2108 IDIN=2 DT=5.0 min
 CHLGTH=1300 m CHSLP=1.67 % FPSLP=1.67 %
 VSN=108 NSEG=3
 ROUGH DIST(m)
 0.04 65
 -0.03 66
 0.04 110

DIST(m)	ELEV(m)
0.0	172.0
42.0	167.5
51.0	160.0
65.0	159.0
65.5	158.7
66.0	159.0
88.0	165.0
110.0	170.0

*
 * Subarea 108
 CALIB NASHYD ID= 2 NHYD=108 DT=5 min AREA=33.5 ha DWF=0.0 cms
 CN=86.8 IA=2.5 mm N=3.0 Tp=0.295 hrs END=-1
 *
 ADD HYD ID=3 NHYD=004 IDI=1 IDII=2
 PRINT HYD ID=3 NPCYC=-1
 *
 * CALCULATE FLOWS ENTERING SITE FROM NORTHWEST
 * Subarea 101 -
 CALIB STANDHYD ID= 4 NHYD=101 DT=5 min AREA= 287.8 ha

SWM.dat

XIMP=0.20 TIMP=0.495 DWF=0.0 cms LOSS=2 CN=83.4
DPSP=5.0 mm SLPP=0.625 % LGP=700 MNP=0.250 SCP=0.0
DPSI=1.57 mm SLPI=0.625 % LGI=3200 MNI=0.017 SCI=0.0
END=-1

*
*

*Route NHYD=101 through channel 102

ROUTE CHANNEL ID=5 NHYD=2101 IDIN=4 DT=5.0 min
CHLGTH=700 m CHSLP=0.42 % FPSLP=0.42 %
VSN=102 NSEG=3
ROUGH DIST(m)
0.04 110
-0.03 111
0.04 160

DIST(m)	ELEV(m)
0.0	182.5
90.0	180.0
110.0	179.8
110.5	179.5
111.0	179.8
130.0	180.0
160.0	182.5

*

* Subarea 102 -
CALIB STANDHYD

ID= 4 NHYD=102 DT=5 min AREA= 272.9 ha
XIMP=0.13 TIMP=0.275 DWF=0.0 cms LOSS=2 CN=84
DPSP=5.0 mm SLPP=0.98 % LGP=1350 MNP=0.250 SCP=0.0
DPSI=1.57 mm SLPI=0.98 % LGI=40 MNI=0.017 SCI=0.0
END=-1

*

* Node 001

ADD HYD ID= 6 NHYD= 001 IDI=4 IDII=5
PRINT HYD ID= 6 NPCYC=-1

*

*Route NHYD=001 through channel 109

ROUTE CHANNEL ID=4 NHYD=2109 IDIN=6 DT=5.0 min
CHLGTH=1000 m CHSLP=0.54 % FPSLP=0.54 %
VSN=109 NSEG=3
ROUGH DIST(m)
0.04 50
-0.03 51
0.04 88

DIST(m)	ELEV(m)
0.0	176.0
14.0	175.5
18.0	175.0
26.0	174.0
42.0	173.0
50.0	173.0
50.5	172.7
51.0	173.0
58.0	173.5
88.0	174.0

* Subarea 109
CALIB NASHYD

ID= 5 NHYD=109 DT=5 min AREA= 35.1 ha DWF=0.0 cms
CN=86.8 IA=2.5 mm N=3.0 Tp=0.318 hrs END=-1

*

ADD HYD ID= 6 NHYD=1109 IDI=4 IDII=5

*

*Route NHYD=1109 through Channel 110

ROUTE CHANNEL ID=4 NHYD=2110 IDIN=6 DT=5.0 min
CHLGTH=900 m CHSLP=0.71 % FPSLP=0.71 %
VSN=110 NSEG=3

SWM.dat

ROUGH DIST(m)
0.04 61
-0.03 62
0.04 114

DIST(m) ELEV(m)
0.0 175.0
10.0 172.5
18.0 170.0
20.0 168.0
61.0 167.5
61.5 167.2
62.0 167.5
80.0 170.0
98.0 172.5
114.0 175.5

*

* Subarea 110
CALIB NASHYD

ID= 5 NHYD=110 DT=5 min AREA= 21.8 ha DWF=0.0 cms
CN=87.2 IA=2.5 mm N=3.0 Tp=0.215 hrs END=-1

*

ADD HYD

ID= 6 NHYD= 1110 IDI=4 IDII=5

*

*Route NHYD=1110 through Channel 111

ROUTE CHANNEL

ID=4 NHYD=2111 IDIN=6 DT=5.0 min
CHLGTH=920 m CHSLP=1.25 % FPSLP=1.25 %
VSN=111 NSEG=3

ROUGH DIST(m)
0.04 56
-0.03 57
0.04 105

DIST(m) ELEV(m)
0.0 172.0
16.0 170.0
44.0 159.0
56.0 159.0
56.5 158.7
57.0 159.0
84.0 170.0
105.0 175.0

*

* Subarea 111
CALIB NASHYD

ID= 1 NHYD=0111 DT=5 min AREA=17.3 ha DWF=0.0 cms
CN=86.4 IA=2.5mm N=3.0 Tp=0.235 hrs END=-1

* Node 002

ADD HYD
PRINT HYD

ID=2 NHYD= 002 IDI=1 IDII=4
ID=2 NPCYC=-1

*

*

ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN

* At confluence of two main branches

ADD HYD ID=9 NHYD=1108 IDI=3 IDII=2

*

* Calculations for South-West section of site (3 subcatchments have been created for catchment 201)

*

SUBCATCHMENT CONTAINING CEMETERY LANDS

PROPOSED IMPERVIOUSNESS LESS THAN 20%

*# THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURFACES

*#
 *#*****
 *# DRAINAGE FROM 201A (EXTERNAL)
 *#*****

```

  *%-----|-----
  CALIB NASHYD      ID=1  NHYD="201A"  DT=5 min  AREA=68.2 ha  DWF=0.0 cms
                   CN=86.0  IA=5 mm  N=3.0   Tp=0.47 hrs  END=-1
  *%-----|-----
  
```

```

  *#Route NHYD=201A through Channel SMT-2
  ROUTE CHANNEL    ID=2  NHYD="SMT-2R"  IDIN=1  DT=5.0 min
                  CHLGTH=450 m  CHSLP=0.75 %  FPSLP=0.75 %
                  VSN=CA1  NSEG=3
                  ROUGH DIST(m)
                   0.04  35
                   -0.03 45
                   0.04  90
  
```

DIST(m)	ELEV(m)
0.0	101.0
35.0	100.5
40.0	100.0
45.0	100.5
90.0	101.0

```

  *%-----|-----
  *#*****
  *# DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d
  *#*****
  
```

```

  *%-----|-----
  CALIB NASHYD      ID=1  NHYD="A1a"  DT=5 min  AREA=0.8 ha  DWF=0.0 cms
                   CN=87.69 IA=5 mm  N=3.0   Tp=0.27 hrs  END=-1
  *%-----|-----
  
```

```

  *%-----|-----
  CALIB NASHYD      ID=3  NHYD="A1b"  DT=3 min  AREA=6.1 ha  DWF=0.0 cms
                   CN=86.13 IA=5 mm  N=3.0   Tp=0.07 hrs  END=-1
  *%-----|-----
  
```

```

  *%-----|-----
  CALIB NASHYD      ID=4  NHYD="A1c"  DT=3 min  AREA=3.2 ha  DWF=0.0 cms
                   CN=87.24 IA=5 mm  N=3.0   Tp=0.14 hrs  END=-1
  *%-----|-----
  
```

```

  *%-----|-----
  CALIB NASHYD      ID=6  NHYD="A1d"  DT=5 min  AREA=5.3 ha  DWF=0.0 cms
                   CN=87.31 IA=5 mm  N=3.0   Tp=0.21 hrs  END=-1
  *%-----|-----
  
```

```

  *%-----|-----
  ROUTE RESERVOIR  IDout=[7],  NHYD=["A1d"],  IDin=[6],
                   RDT=[5](min),
  
```

TABLE of (OUTFLOW-STORAGE) values

(cms) - (ha-m)	
[0.0 , 0.0]	
[0.034, 0.028]	
[0.103, 0.043]	
[0.142, 0.059]	
[0.198, 0.093]	
[0.241, 0.129]	
[0.278, 0.168]	
[0.310, 0.209]	
[-1 , -1]	

(max twenty pts)

IDovf=[8], NHYDovf=["OVR"]

```

  *%-----|-----
  ADD HYD          IDsum=[6], NHYD=["A1dPND"], IDs to add=[7+8]
  *%-----|-----
  
```

```

  *#*****
  *# TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d
  *#*****
  
```

```

  *%-----|-----
  ADD HYD          IDsum=[5], NHYD=["SMT2"], IDs to add=[1+2+3+4+6]
  *%-----|-----
  
```

SWM.dat

```

*****
*# DRAINAGE FROM 201B (EXTERNAL)
*****
*%-----|-----
CALIB NASHYD      ID=1  NHYD="201B"  DT=5 min  AREA=13.4 ha  DWF=0.0 cms
                  CN=86.0  IA=5 mm   N=3.0   Tp=0.31 hrs  END=-1

*****
*# DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)
*****
*%-----|-----
CALIB NASHYD      ID=2  NHYD="B1a"  DT=3 min  AREA=4.6 ha  DWF=0.0 cms
                  CN=87.02 IA=5 mm   N=3.0   Tp=0.17 hrs  END=-1
*%-----|-----
ROUTE RESERVOIR  IDout=[4],  NHYD=["B1a"],  IDin=[2],
                  RDT=[5](min),
                  TABLE of ( OUTFLOW-STORAGE ) values
                                (cms) - (ha-m)
                                [ 0.0 , 0.0 ]
                                [ 0.034, 0.019 ]
                                [ 0.103, 0.029 ]
                                [ 0.142, 0.040 ]
                                [ 0.198, 0.062 ]
                                [ 0.241, 0.087 ]
                                [ 0.278, 0.114 ]
                                [ 0.310, 0.142 ]
                                [ 0.325, 0.158 ]
                                [ -1 , -1 ] (max twenty pts)
                  IDovf=[8],  NHYDovf=["OVR"]
*%-----|-----
ADD HYD           IDsum=[2],  NHYD=["B1aPND"],  IDs to add=[4+8]
*%-----|-----
ADD HYD           IDsum=[3],  NHYD=["201B"],  IDs to add=[1+2]
*%-----|-----
*# *****
*# Route NHYD=201B + B1a through Channel SMT-4
*# *****
ROUTE CHANNEL     ID=1  NHYD="SMT-4R"  IDIN=3   DT=5.0 min
                  CHLGTH=600 m  CHSLP=0.85 %  FPSLP=0.85 %
                  VSN=CB1  NSEG=3
                  ROUGH DIST(m)
                   0.04  35
                   -0.03 45
                   0.04  90

                  DIST(m)  ELEV(m)
                   0.0     101.0
                   35.0    100.5
                   40.0    100.0
                   45.0    100.5
                   90.0    101.0
*%-----|-----
CALIB NASHYD      ID=3  NHYD="B1b"  DT=3 min  AREA=5.0 ha  DWF=0.0 cms
                  CN=86.14 IA=5 mm   N=3.0   Tp=0.17 hrs  END=-1
*%-----|-----
CALIB NASHYD      ID=4  NHYD="B1c"  DT=3 min  AREA=1.0 ha  DWF=0.0 cms
                  CN=87.71 IA=5 mm   N=3.0   Tp=0.10 hrs  END=-1
*%-----|-----
ADD HYD           IDsum=[2],  NHYD=["B1b/c"],  IDs to add=[3+4]
*%-----|-----
*# *****
*# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c
*# *****
*%-----|-----
ADD HYD           IDsum=[3],  NHYD=["B1East"],  IDs to add=[1+2]

```

SWM.dat

*%-----|-----
*#*****|*****
*# DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)
*#*****|*****
*%-----|-----

CALIB STANDHYD ID=[1], NHYD=["B1d"], DT=[3](min), AREA=[4.3](ha),
XIMP=[0.2535], TIMP=[0.2535], DWF=[0.0](cms), LOSS=[2],
SCS curve number CN=[86],
Pervious surfaces: IAper=[5](mm), SLPP=[0.85](%),
LGP=[30](m), MNP=[0.035], SCP=[0](min),
Impervious surfaces: IAimp=[0.5](mm), SLPI=[0.85](%),
LGI=[50](m), MNI=[0.013], SCI=[0](min),
END=-1

*%-----|-----
ROUTE RESERVOIR IDout=[4], NHYD=["B1d"], IDin=[1],
RDT=[5](min),
TABLE of (OUTFLOW-STORAGE) values
(cms) - (ha-m)
[0.0 , 0.0]
[0.034 , 0.031]
[0.103 , 0.048]
[0.142 , 0.065]
[0.198 , 0.101]
[0.241 , 0.139]
[0.278 , 0.180]
[0.310 , 0.223]
[-1 , -1] (max twenty pts)
IDovf=[8], NHYDovf=["OVR"]

*%-----|-----
ADD HYD IDsum=[1], NHYD=["B1dPND"], IDs to add=[4+8]

*%-----|-----
CALIB NASHYD ID=2 NHYD="B1f" DT=3 min AREA=3.5 ha DWF=0.0 cms
CN=87.36 IA=5 mm N=3.0 Tp=0.11 hrs END=-1

*%-----|-----
ROUTE RESERVOIR IDout=[4], NHYD=["B1f"], IDin=[2],
RDT=[5](min),
TABLE of (OUTFLOW-STORAGE) values
(cms) - (ha-m)
[0.0 , 0.0]
[0.044 , 0.025]
[0.076 , 0.038]
[0.099 , 0.052]
[0.132 , 0.081]
[0.159 , 0.112]
[0.182 , 0.145]
[0.202 , 0.181]
[0.212 , 0.199]
[-1 , -1] (max twenty pts)
IDovf=[8], NHYDovf=["OVR"]

*%-----|-----
ADD HYD IDsum=[2], NHYD=["B1fPND"], IDs to add=[4+8]

*%-----|-----
CALIB STANDHYD ID=[7], NHYD=["B1e"], DT=[3](min), AREA=[3.6](ha),
XIMP=[0.2694], TIMP=[0.2694], DWF=[0.0](cms), LOSS=[2],
SCS curve number CN=[86],
Pervious surfaces: IAper=[5](mm), SLPP=[1.15](%),
LGP=[30](m), MNP=[0.035], SCP=[0](min),
Impervious surfaces: IAimp=[0.5](mm), SLPI=[1.15](%),
LGI=[50](m), MNI=[0.013], SCI=[0](min),
END=-1

*%-----|-----
ROUTE RESERVOIR IDout=[6], NHYD=["B1e"], IDin=[7],
RDT=[5](min),
TABLE of (OUTFLOW-STORAGE) values
(cms) - (ha-m)

```

                                SWM.dat
                                [ 0.0 , 0.0 ]
                                [ 0.034, 0.041]
                                [ 0.103, 0.062]
                                [ 0.142, 0.085]
                                [ 0.198, 0.133]
                                [ 0.241, 0.184]
                                [ 0.278, 0.240]
                                [ 0.310, 0.299]
                                [ -1 , -1 ]
                                (max twenty pts)
                                IDovf=[8], NHYDovf=["OVR"]
*%-----|-----
ADD HYD      IDsum=[7], NHYD=["B1ePND"], IDs to add=[6+8]
*%-----|-----
ADD HYD      IDsum=[2], NHYD=["B1west"], IDs to add=[1+2+7]
*%-----|-----
*#*****
*# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
*#*****
*%-----|-----
ADD HYD      IDsum=[4], NHYD=["SMT4"], IDs to add=[2+3]
*%-----|-----
*#*****
*# DRAINAGE FROM 201C (EXTERNAL)
*#*****
CALIB NASHYD ID=1 NHYD="201C" DT=5 min AREA=91.0 ha DWF=0.0 cms
              CN=86.0 IA=5 mm N=3.0 Tp=0.50 hrs END=-1
*#*****
*# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
*#*****
*%-----|-----
CALIB NASHYD ID=2 NHYD="C1a" DT=5 min AREA=7.0 ha DWF=0.0 cms
              CN=86.0 IA=5 mm N=3.0 Tp=0.21 hrs END=-1
*%-----|-----
*#*****
*# C1a SWM FACILITY
*#*****
ROUTE RESERVOIR IDout=[6], NHYD=["C1a"], IDin=[2],
                RDT=[5](min),
                TABLE of ( OUTFLOW-STORAGE ) values
                (cms) - (ha-m)
                [ 0.0 , 0.0 ]
                [ 0.034, 0.021]
                [ 0.103, 0.032]
                [ 0.142, 0.043]
                [ 0.198, 0.067]
                [ 0.241, 0.093]
                [ 0.278, 0.120]
                [ 0.310, 0.150]
                [ 0.325, 0.165]
                [ -1 , -1 ]
                (max twenty pts)
                IDovf=[8], NHYDovf=["OVR"]
*%-----|-----
*#*****
*# DISCHARGE FROM C1a SWM FACILITY
*#*****
ADD HYD      IDsum=[2], NHYD=["C1aPND"], IDs to add=[6+8]
*%-----|-----
CALIB NASHYD ID=3 NHYD="C1b" DT=2 min AREA=0.5 ha DWF=0.0 cms
              CN=86.54 IA=5 mm N=3.0 Tp=0.04 hrs END=-1
*%-----|-----
*#*****
*# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
*#*****
ADD HYD      IDsum=[2], NHYD=["EX+MC"], IDs to add=[1+2+3]
*%-----|-----

```

*# Route NHYD=201C through channel SMT-1

```
ROUTE CHANNEL      ID=1  NHYD=["SMT-1"]  IDIN=2  DT=5.0 min
                   CHLGTH=275 m  CHSLP=0.50 %  FPSLP=0.50 %
                   VSN=CC1  NSEG=3
                   ROUGH DIST(m)
                       0.04  35
                       -0.03  45
                       0.04  90
```

```
DIST(m)  ELEV(m)
    0.0    101.0
   35.0    100.5
   40.0    100.0
   45.0    100.5
   90.0    101.0
```

```
-----|-----
*%-----|-----
CALIB NASHYD      ID=7,  NHYD=["C2"],  DT=3 min,  AREA=3.8 ha,  DWF=0.0 cms,
                   CN=86.14,  IA=5 mm,  N=3.0,  Tp=0.17 hrs,  END=-1
*%-----|-----
```

*# TOTAL DRAINAGE FROM SUBCATCHMENTS

*# EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2

```
ADD HYD            IDsum=[1],  NHYD=["SMT1"],  IDs to add=[1+7]
```

```
-----|-----
*%-----|-----
*#*****|-----
*# CONFLUENCE SMT 1-4
*#*****|-----
```

```
-----|-----
*%-----|-----
ADD HYD            IDsum=[2],  NHYD=["SMT1-4"],  IDs to add=[4+1]
```

```
-----|-----
*%-----|-----
*#*****|-----
*# DRAINAGE FROM 201D (EXTERNAL)
*#*****|-----
```

```
CALIB NASHYD      ID=2  NHYD="201D"  DT=5 min  AREA=28.9 ha  DWF=0.0 cms
                   CN=86.0  IA=5 mm  N=3.0  Tp=0.41 hrs  END=-1
```

```
-----|-----
*%-----|-----
*#*****|-----
*# SUBCATCHMENT 201D ROUTED
*# THROUGH Channel SMT-3
*#*****|-----
```

*# THROUGH Channel SMT-3

```
-----|-----
*%-----|-----
```

```
ROUTE CHANNEL      ID=3  NHYD="SMT-3R"  IDIN=2  DT=5.0 min
                   CHLGTH=100 m  CHSLP=0.70 %  FPSLP=0.70 %
                   VSN=CD1  NSEG=3
                   ROUGH DIST(m)
                       0.04  10
                       -0.03  15
                       0.04  20
```

```
DIST(m)  ELEV(m)
    0.0    178.0
   26.0    177.6
   30.0    176.0
   34.0    177.57
   50.0    178.0
```

```
-----|-----
*%-----|-----
*#*****|-----
*# DRAINAGE FROM CEMETERY LANDS D1a, D1b
*#*****|-----
```

```
-----|-----
*%-----|-----
```

```
-----|-----
*%-----|-----
CALIB NASHYD      ID=2,  NHYD=["D1a"],  DT=3 min,  AREA=1.9 ha,  DWF=0.0 cms
```



```

                                SWM.dat
                                CN=87.99, IA=5 mm, N=3.0, Tp=0.13 hrs, END=-1
*%-----|-----
CALIB NASHYD                    ID=7, NHYD=["D1b"], DT=3 min, AREA=1.9 ha, DWF=0.0 cms
                                CN=86.0, IA=5 mm, N=3.0, Tp=0.09 hrs, END=-1
*%-----|-----
*#*****
*# TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b
*#*****
*%-----|-----
ADD HYD                          IDsum=[6], NHYD=["SMT3"], IDs to add=[2+3+7]
*%-----|-----
*#*****
*# CONFLUENCE SMT 1-3
*#*****
*%-----|-----
ADD HYD                          IDsum=[3], NHYD=["SMT1-3"], IDs to add=[1+4+6]
*%-----|-----
*#*****
*# TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D
*#*****
ADD HYD                          ID=[8] NHYD=["1201"] IDs to add=[1+4+6+5]
*%-----|-----
*Route NHYD=201 through Channel 202
ROUTE CHANNEL                    ID=3 NHYD=2202 IDIN=8 DT=5.0 min
                                CHLGTH=475 m CHSLP=1.05 % FPSLP=1.05 %
                                VSN=202 NSEG=3
                                ROUGH DIST(m)
                                0.04 55
                                -0.03 56
                                0.04 105

                                DIST(m) ELEV(m)
                                0.0 180.0
                                15.0 175.0
                                55.0 174.9
                                55.5 174.6
                                56.0 174.9
                                70.0 175.0
                                105.0 180.0

*
* Subarea 202
CALIB NASHYD                    ID= 4 NHYD=202 DT=5 min AREA=21.6 ha DWF=0.0 cms
                                CN=86.8 IA=2.5 mm N=3.0 Tp=0.303 hrs END=-1
*
ADD HYD                          ID=2 NHYD=1202 IDI=3 IDII=4
*
* Subarea 203
CALIB NASHYD                    ID= 3 NHYD=203 DT=5 min AREA=26.3 ha DWF=0.0 cms
                                CN=86.8 IA=2.5mm N=3.0 Tp=0.240 hrs END=-1
*
* Node 003 - exit from site
ADD HYD                          ID= 4 NHYD=003 IDI=3 IDII=2
PRINT HYD                        ID= 4 NPCYC=-1
*
*#*****
*# SUBCATCHMENT 204 AREA REVISED
*# NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha
*#*****
*
*Subarea 204 - off site
CALIB NASHYD                    ID= 2 NHYD=204 DT=5 min AREA=53.6 ha DWF=0.0 cms
                                CN=87.6 IA=5 mm N=3.0 Tp=0.626 hrs END=-1
*
ADD HYD                          ID= 3 NHYD= 1204 IDI= 2 IDII= 4
*

```

SWM.dat

```
*****  
*# ROUTE through Channel 205 ELIMINATED, OUTSIDE OF STUDY AREA  
*****  
*  
*# SUBCATCHMENT 205 ELIMINTATED, OUTSIDE OF STUDY AREA  
*****  
*  
* Confluence of tributaries off site  
*****  
*# ID REVISED TO ID=9, PREVIOUSLY ID=1  
*****  
ADD HYD          ID=2  NHYD=008  IDI=9  IDII=3  
PRINT HYD       ID=2  NPCYC=-1  
*****  
*  
START           START=0.0  HRS  METOUT=0  NSTORM=1  NRUN=2  
                MILSCS12.005  
*  
START           START=0.0  HRS  METOUT=0  NSTORM=1  NRUN=3  
                MILSCS12.010  
*  
START           START=0.0  HRS  METOUT=0  NSTORM=1  NRUN=4  
                MILSCS12.025  
*  
START           START=0.0  HRS  METOUT=0  NSTORM=1  NRUN=5  
                MILSCS12.050  
*  
START           START=0.0  HRS  METOUT=0  NSTORM=1  NRUN=6  
                MILSCS12.100
```

FINISH

```

SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM O O 9 9 9 9
SSSSS W W W M M M H H H H Y M M M O O ## 9 9 9 9 Ver. 4.02
S W W M M H H Y M M O O 9999 9999 July 1999
SSSSS W W M M H H Y M M 000 9 9 9 9 # 3569108
StormWater Management Hydrologic Model 999 999 =====

```

```

*****
***** SWMHYMO-99 Ver/4.02 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 727-5199 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****
*****

```

```

+++++++ Licensed user: Philips Engineering Ltd ++++++
+++++++ Burlington SERIAL#:3569108 ++++++
+++++++

```

```

*****
***** ++++++ PROGRAM ARRAY DIMENSIONS ++++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 15000 *****
***** Max. number of flow points : 15000 *****
*****

```

```

*** DESCRIPTION SUMMARY TABLE HEADERS (units depend on METOUT in START) ***
***-----***
*** ID: Hydrograph IDentification numbers, (1-10). ***
*** NHYD: Hydrograph reference numbers, (6 digits or characters). ***
*** AREA: Drainage area associated with hydrograph, (ac.) or (ha.). ***
*** QPEAK: Peak flow of simulated hydrograph, (ft^3/s) or (m^3/s). ***
*** TpeakDate_hh:mm is the date and time of the peak flow. ***
*** R.V.: Runoff volume of simulated hydrograph, (in) or (mm). ***
*** R.C.: Runoff Coefficient of simulated hydrograph, (ratio). ***
*** *: see WARNING or NOTE message printed at end of run. ***
*** **: see ERROR message printed at end of run. ***
*****
*****

```

```

***** SUMMARY OUTPUT *****
*****
* DATE: 2011-12-06 TIME: 12:10:18 RUN COUNTER: 000138 *
*****
* Input filename: G:\work\105128\water\SWMHYMO\2011NO~1\SWM.dat *
* Output filename: G:\work\105128\water\SWMHYMO\2011NO~1\SWM.out *
* Summary filename: G:\work\105128\water\SWMHYMO\2011NO~1\SWM.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****

```

SWM.sum

```
*****
# Project Name: [Holy Family Catholic Cemetery] Project Number: [111063]
# Date : 08-16-2011
# Modeller : [C. Silvestri]
# Company : Philips Engineering Ltd
# License # : 3569108
*****
```

RUN:COMMAND#

```
001:0001-----
START
[TZERO = .00 hrs on 0]
[METOUT= 2 (1=imperial, 2=metric output)]
[NSTORM= 1 ]
[NRUN = 1 ]
001:0002-----
READ STORM
Filename = STORM.001
Comment = TOWN OF MILTON 12 HOUR 2 YEAR SCS STORM (1998 IDF DATA)
[SDT=12.00:SDUR= 12.00:PTOT= 42.82]
001:0003-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 01:000103 42.10 1.550 No_date 6:18 19.90 .465
[CN= 86.0: N= 3.00]
[Tp= .40:DT= 6.00]
001:0004-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:000103 42.10 1.550 No_date 6:18 19.90 n/a
[RDT= 6.00] out<- 02:002104 42.10 1.365 No_date 6:30 19.90 n/a
[L/S/n= 440./1.000/.030]
{Vmax= .616:Dmax= .476}
001:0005-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 03:000104 24.10 1.349 No_date 6:06 19.90 .465
[CN= 86.0: N= 3.00]
[Tp= .21:DT= 6.00]
001:0006-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000104 24.10 1.349 No_date 6:06 19.90 n/a
+ 02:002104 42.10 1.365 No_date 6:30 19.90 n/a
[DT= 6.00] SUM= 01:001104 66.20 2.167 No_date 6:12 19.90 n/a
001:0007-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:001104 66.20 2.167 No_date 6:12 19.90 n/a
[RDT= 6.00] out<- 02:002105 66.20 1.825 No_date 6:30 19.90 n/a
[L/S/n= 365./ .400/.030]
{Vmax= .367:Dmax= .456}
001:0008-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD 03:000105 19.20 1.210 No_date 6:00 20.59 .481
[CN= 86.8: N= 3.00]
[Tp= .18:DT= 6.00]
001:0009-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000105 19.20 1.210 No_date 6:00 20.59 n/a
+ 02:002105 66.20 1.825 No_date 6:30 19.90 n/a
[DT= 6.00] SUM= 01:001105 85.40 2.302 No_date 6:12 20.06 n/a
001:0010-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:001105 85.40 2.302 No_date 6:12 20.06 n/a
[RDT= 6.00] out<- 02:002106 85.40 2.166 No_date 6:30 20.06 n/a
[L/S/n= 385./ .670/.030]
{Vmax= .536:Dmax= .448}
001:0011-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD 03:000106 15.30 1.020 No_date 6:00 20.95 .489
[CN= 87.2: N= 3.00]
[Tp= .17:DT= 6.00]
001:0012-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000106 15.30 1.020 No_date 6:00 20.95 n/a
+ 02:002106 85.40 2.166 No_date 6:30 20.06 n/a
[DT= 6.00] SUM= 01:001106 100.70 2.496 No_date 6:18 20.19 n/a
001:0013-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 03:000107 15.27 .309 No_date 6:00 24.51 .572
```

SWM.sum

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[XIMP=.10:TIMP=.17]
[LOSS= 2 :CN= 88.0]
[Pervious area: IAper= 2.50:SLPP=1.27:LGP= 717.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI=1.27:LGI= 100.:MNI=.017:SCI= .0]
001:0014-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          01:001106   100.70   2.496 No_date   6:18   20.19  n/a
                + 03:000107   15.27   .309 No_date   6:00   24.51  n/a
[DT= 6.00] SUM= 02:001107   115.97   2.662 No_date   6:18   20.76  n/a
001:0015-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL  -> 02:001107   115.97   2.662 No_date   6:18   20.76  n/a
[RDT= 6.00] out<- 01:002108   115.97   2.426 No_date   6:42   20.76  n/a
[L/S/n= 1300./1.670/.030]
{Vmax= 1.288:Dmax= .530}
001:0016-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD   02:000108   33.50   1.559 No_date   6:12   20.59  .481
[CN= 86.8: N= 3.00]
[Tp= .29:DT= 6.00]
001:0017-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          01:002108   115.97   2.426 No_date   6:42   20.76  n/a
                + 02:000108   33.50   1.559 No_date   6:12   20.59  n/a
[DT= 6.00] SUM= 03:000004   149.47   3.445 No_date   6:18   20.72  n/a
001:0018-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
PRINT HYD      03:000004   149.47   3.445 No_date   6:18   20.72  n/a
001:0019-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB STANDHYD 04:000101   287.80   4.326 No_date   6:42   25.83  .603
[XIMP=.20:TIMP=.50]
[LOSS= 2 :CN= 83.4]
[Pervious area: IAper= 5.00:SLPP= .63:LGP= 700.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI= .63:LGI=3200.:MNI=.017:SCI= .0]
001:0020-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL  -> 04:000101   287.80   4.326 No_date   6:42   25.83  n/a
[RDT= 6.00] out<- 05:002101   287.80   4.264 No_date   7:48   25.83  n/a
[L/S/n= 700./ .420/.030]
{Vmax= .508:Dmax= .579}
001:0021-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
* CALIB STANDHYD 04:000102   272.90   6.080 No_date   6:00   21.82  .510
[XIMP=.13:TIMP=.28]
[LOSS= 2 :CN= 84.0]
[Pervious area: IAper= 5.00:SLPP= .98:LGP=1350.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI= .98:LGI= 40.:MNI=.017:SCI= .0]
001:0022-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          04:000102   272.90   6.080 No_date   6:00   21.82  n/a
                + 05:002101   287.80   4.264 No_date   7:48   25.83  n/a
[DT= 6.00] SUM= 06:000001   560.70   7.428 No_date   7:42   23.88  n/a
001:0023-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
PRINT HYD      06:000001   560.70   7.428 No_date   7:42   23.88  n/a
001:0024-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL  -> 06:000001   560.70   7.428 No_date   7:42   23.88  n/a
[RDT= 6.00] out<- 04:002109   560.70   7.227 No_date   7:54   23.88  n/a
[L/S/n= 1000./ .540/.030]
{Vmax= .938:Dmax= .777}
001:0025-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD   05:000109   35.10   1.570 No_date   6:12   20.59  .481
[CN= 86.8: N= 3.00]
[Tp= .32:DT= 6.00]
001:0026-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          04:002109   560.70   7.227 No_date   7:54   23.88  n/a
                + 05:000109   35.10   1.570 No_date   6:12   20.59  n/a
[DT= 6.00] SUM= 06:001109   595.80   7.409 No_date   7:54   23.68  n/a
001:0027-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL  -> 06:001109   595.80   7.409 No_date   7:54   23.68  n/a
[RDT= 6.00] out<- 04:002110   595.80   7.199 No_date   8:12   23.68  n/a
[L/S/n= 900./ .710/.030]
{Vmax= .803:Dmax= .715}
001:0028-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-

```

ID	Description	ID	AREA	QPEAK	TpeakDate_hh:mm	R.V.	R.C.
001:0029	CALIB NASHYD [CN= 87.2: N= 3.00] [Tp= .22:DT= 6.00]	05:000110	21.80	1.270	No_date 6:06	20.95	.489
ADD HYD		04:002110	595.80	7.199	No_date 8:12	23.68	n/a
		05:000110	21.80	1.270	No_date 6:06	20.95	n/a
[DT= 6.00] SUM=		06:001110	617.60	7.301	No_date 8:06	23.59	n/a
001:0030	ROUTE CHANNEL -> [RDT= 6.00] out<- [L/s/n= 920./1.250/.030] {Vmax= 1.164:Dmax= .530}	06:001110	617.60	7.301	No_date 8:06	23.59	n/a
		04:002111	617.60	7.223	No_date 8:18	23.59	n/a
001:0031	CALIB NASHYD [CN= 86.4: N= 3.00] [Tp= .23:DT= 6.00]	01:000111	17.30	.926	No_date 6:06	20.24	.473
001:0032	ADD HYD	01:000111	17.30	.926	No_date 6:06	20.24	n/a
		04:002111	617.60	7.223	No_date 8:18	23.59	n/a
[DT= 6.00] SUM=		02:000002	634.90	7.293	No_date 8:18	23.50	n/a
001:0033	PRINT HYD	02:000002	634.90	7.293	No_date 8:18	23.50	n/a

# ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN							
001:0034	ADD HYD	03:000004	149.47	3.445	No_date 6:18	20.72	n/a
		02:000002	634.90	7.293	No_date 8:18	23.50	n/a
[DT= 6.00] SUM=		09:001108	784.37	8.531	No_date 8:06	22.97	n/a

# SUBCATCHMENT CONTAINING CEMETERY LANDS							

# PROPOSED IMPERVIOUSNESS LESS THAN 20%							
# THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURF							
#							

# DRAINAGE FROM 201A (EXTERNAL)							

001:0035	CALIB NASHYD [CN= 86.0: N= 3.00] [Tp= .47:DT= 6.00]	01:201A	68.20	2.032	No_date 6:24	18.06	.422
#Route NHYD=201A through Channel SMT-2							
001:0036	ROUTE CHANNEL -> [RDT= 6.00] out<- [L/s/n= 450./ .750/.030] {Vmax= 1.046:Dmax= .439}	01:201A	68.20	2.032	No_date 6:24	18.06	n/a
		02:SMT-2R	68.20	1.979	No_date 6:30	18.06	n/a

# DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d							

001:0037	CALIB NASHYD [CN= 87.7: N= 3.00] [Tp= .27:DT= 6.00]	01:A1a	.80	.038	No_date 6:06	19.46	.455
001:0038	* CALIB NASHYD [CN= 86.1: N= 3.00] [Tp= .07:DT= 3.00]	03:A1b	6.10	.524	No_date 6:00	18.17	.424
001:0039	CALIB NASHYD [CN= 87.2: N= 3.00] [Tp= .14:DT= 3.00]	04:A1c	3.20	.219	No_date 6:03	19.08	.446
001:0040	CALIB NASHYD	06:A1d	5.30	.290	No_date 6:06	19.14	.447

SWM.sum

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[CN= 87.3: N= 3.00]
[TP= .21:DT= 6.00]
001:0041-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 06:A1d      5.30      .290 No_date   6:06   19.14  n/a
[RD= 6.00] out<- 07:A1d      5.30      .103 No_date   6:30   19.14  n/a
overflow <= 08:OVR      .00      .000 No_date   0:00    .00  n/a
{MxStoUsed=.4308E-01, TotovfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
001:0042-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD              07:A1d      5.30      .103 No_date   6:30   19.14  n/a
+ 08:OVR              .00      .000 No_date   0:00    .00  n/a
[DT= 6.00] SUM= 06:A1dPND  5.30      .103 No_date   6:30   19.14  n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d
*****
001:0043-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD              01:A1a      .80      .038 No_date   6:06   19.46  n/a
+ 02:SMT-2R          68.20     1.979 No_date   6:30   18.06  n/a
+ 03:A1b              6.10      .524 No_date   6:00   18.17  n/a
+ 04:A1c              3.20      .219 No_date   6:03   19.08  n/a
+ 06:A1dPND           5.30      .103 No_date   6:30   19.14  n/a
[DT= 3.00] SUM= 05:SMT2    83.60     2.211 No_date   6:24   18.29  n/a
*****
# DRAINAGE FROM 201B (EXTERNAL)
*****
001:0044-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD        01:201B     13.40     .537 No_date   6:12   18.06  .422
[CN= 86.0: N= 3.00]
[TP= .31:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)
*****
001:0045-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD        02:B1a      4.60      .280 No_date   6:03   18.89  .441
[CN= 87.0: N= 3.00]
[TP= .17:DT= 3.00]
001:0046-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1a      4.60      .280 No_date   6:03   18.89  n/a
[RD= 3.00] out<- 04:B1a      4.60      .116 No_date   6:21   18.89  n/a
overflow <= 08:OVR      .00      .000 No_date   0:00    .00  n/a
{MxStoUsed=.3268E-01, TotovfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
001:0047-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD              04:B1a      4.60      .116 No_date   6:21   18.89  n/a
+ 08:OVR              .00      .000 No_date   0:00    .00  n/a
[DT= 3.00] SUM= 02:B1aPND  4.60      .116 No_date   6:21   18.89  n/a
001:0048-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD              01:201B     13.40     .537 No_date   6:12   18.06  n/a
+ 02:B1aPND           4.60      .116 No_date   6:21   18.89  n/a
[DT= 3.00] SUM= 03:201B    18.00     .642 No_date   6:12   18.28  n/a
*****
# Route NHYD=201B + B1a through Channel SMT-4
*****
001:0049-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 03:201B     18.00     .642 No_date   6:12   18.28  n/a
* [RD= 3.00] out<- 01:SMT-4R  18.00     .543 No_date   6:24   18.28  n/a
[L/s/n= 600./ .850/.030]
{Vmax= .817:Dmax= .277}
001:0050-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD        03:B1b      5.00      .291 No_date   6:03   18.17  .424
[CN= 86.1: N= 3.00]
[TP= .17:DT= 3.00]
001:0051-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD        04:B1c      1.00      .082 No_date   6:00   19.48  .455
[CN= 87.7: N= 3.00]
[TP= .10:DT= 3.00]
001:0052-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

```

```

SWM.sum
ADD HYD          03:B1b          5.00    .291 No_date    6:03    18.17    n/a
                + 04:B1c          1.00    .082 No_date    6:00    19.48    n/a
[DT= 3.00] SUM= 02:B1b/c        6.00    .366 No_date    6:03    18.39    n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c
*****
001:0053-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:SMT-4R        18.00    .543 No_date    6:24    18.28    n/a
                + 02:B1b/c          6.00    .366 No_date    6:03    18.39    n/a
[DT= 3.00] SUM= 03:B1East       24.00    .712 No_date    6:15    18.30    n/a
*****
# DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)
*****
001:0054-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 01:B1d          4.30    .415 No_date    6:00    24.21    .565
[XIMP=.25:TIMP=.25]
[LOSS= 2 :CN= 86.0]
[Pervious area: IAper= 5.00:SLPP= .85:LGP= 30.:MNP=.035:SCP= .0]
[Impervious area: IAimp= .50:SLPI= .85:LGI= 50.:MNI=.013:SCI= .0]
001:0055-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 01:B1d          4.30    .415 No_date    6:00    24.21    n/a
[RDT= 3.00] out<- 04:B1d          4.30    .103 No_date    6:15    24.21    n/a
overflow <= 08:OVR                .00    .000 No_date    0:00    .00    n/a
{MxStoUsed=.4822E-01, TotovfVol=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
001:0056-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          04:B1d          4.30    .103 No_date    6:15    24.21    n/a
                + 08:OVR                .00    .000 No_date    0:00    .00    n/a
[DT= 3.00] SUM= 01:B1dPND        4.30    .103 No_date    6:15    24.21    n/a
001:0057-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     02:B1f          3.50    .268 No_date    6:00    19.18    .448
[CN= 87.4: N= 3.00]
[Tp= .11:DT= 3.00]
001:0058-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1f          3.50    .268 No_date    6:00    19.18    n/a
[RDT= 3.00] out<- 04:B1f          3.50    .057 No_date    6:21    19.18    n/a
overflow <= 08:OVR                .00    .000 No_date    0:00    .00    n/a
{MxStoUsed=.3035E-01, TotovfVol=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
001:0059-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          04:B1f          3.50    .057 No_date    6:21    19.18    n/a
                + 08:OVR                .00    .000 No_date    0:00    .00    n/a
[DT= 3.00] SUM= 02:B1fPND        3.50    .057 No_date    6:21    19.18    n/a
001:0060-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 07:B1e          3.60    .358 No_date    6:00    24.60    .574
[XIMP=.27:TIMP=.27]
[LOSS= 2 :CN= 86.0]
[Pervious area: IAper= 5.00:SLPP=1.15:LGP= 30.:MNP=.035:SCP= .0]
[Impervious area: IAimp= .50:SLPI=1.15:LGI= 50.:MNI=.013:SCI= .0]
001:0061-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 07:B1e          3.60    .358 No_date    6:00    24.60    n/a
[RDT= 3.00] out<- 06:B1e          3.60    .053 No_date    6:24    24.60    n/a
overflow <= 08:OVR                .00    .000 No_date    0:00    .00    n/a
{MxStoUsed=.4674E-01, TotovfVol=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
001:0062-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          06:B1e          3.60    .053 No_date    6:24    24.60    n/a
                + 08:OVR                .00    .000 No_date    0:00    .00    n/a
[DT= 3.00] SUM= 07:B1ePND        3.60    .053 No_date    6:24    24.60    n/a
001:0063-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:B1dPND        4.30    .103 No_date    6:15    24.21    n/a
                + 02:B1West          3.50    .057 No_date    6:21    19.18    n/a
                + 07:B1ePND          3.60    .053 No_date    6:24    24.60    n/a
[DT= 3.00] SUM= 02:B1West        11.40    .212 No_date    6:18    22.79    n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
*****
001:0064-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

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                                SWM.sum
ADD HYD                02:B1West  11.40    .212 No_date  6:18  22.79  n/a
                    + 03:B1East  24.00    .712 No_date  6:15  18.30  n/a
    [DT= 3.00] SUM= 04:SMT4  35.40    .922 No_date  6:15  19.75  n/a
*****
# DRAINAGE FROM 201C (EXTERNAL)
*****
001:0065-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          01:201C    91.00    2.603 No_date  6:24  18.06  .422
    [CN= 86.0: N= 3.00]
    [Tp= .50:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
*****
001:0066-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          02:C1a     7.00     .360 No_date  6:06  18.06  .422
    [CN= 86.0: N= 3.00]
    [Tp= .21:DT= 6.00]
*****
# C1a SWM FACILITY
*****
001:0067-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:C1a     7.00     .360 No_date  6:06  18.06  n/a
    [RDT= 6.00] out<- 06:C1a     7.00     .149 No_date  6:30  18.06  n/a
    overflow <= 08:OVR          .00     .000 No_date  0:00    .00  n/a
    {MxStoUsed=.4651E-01, TotOvfVo=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
*****
# DISCHARGE FROM C1a SWM FACILITY
*****
001:0068-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                06:C1a     7.00     .149 No_date  6:30  18.06  n/a
                    + 08:OVR          .00     .000 No_date  0:00    .00  n/a
    [DT= 6.00] SUM= 02:C1aPND    7.00     .149 No_date  6:30  18.06  n/a
001:0069-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD          03:C1b     .50     .047 No_date  6:00  18.49  .432
    [CN= 86.5: N= 3.00]
    [Tp= .04:DT= 2.00]
*****
# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
*****
001:0070-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                01:201C    91.00    2.603 No_date  6:24  18.06  n/a
                    + 02:EX+MC     7.00     .149 No_date  6:30  18.06  n/a
                    + 03:C1b         .50     .047 No_date  6:00  18.49  n/a
    [DT= 2.00] SUM= 02:EX+MC    98.50    2.757 No_date  6:24  18.07  n/a
*****
# Route NHYD=201C through channel SMT-1
*****
001:0071-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 02:EX+MC    98.50    2.757 No_date  6:24  18.07  n/a
* [RDT= 2.00] out<- 01:SMT-1    98.50    2.704 No_date  6:28  18.07  n/a
    [L/S/n= 275./ .500/.030]
    {Vmax= .960:Dmax= .525}
001:0072-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          07:C2     3.80     .222 No_date  6:03  18.17  .424
    [CN= 86.1: N= 3.00]
    [Tp= .17:DT= 3.00]
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS
# EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2
*****
001:0073-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                01:SMT1    98.50    2.704 No_date  6:28  18.07  n/a
                    + 07:C2         3.80     .222 No_date  6:03  18.17  n/a
    [DT= 2.00] SUM= 01:SMT1   102.30    2.771 No_date  6:26  18.07  n/a
*****

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SWM.sum

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# CONFLUENCE SMT 1-4
#*****
001:0074-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          04:SMT4          35.40    .922 No_date  6:15  19.75  n/a
                + 01:SMT1          102.30   2.771 No_date  6:26  18.07  n/a
  [DT= 2.00] SUM= 02:SMT1-4      137.70   3.627 No_date  6:24  18.50  n/a
#*****
# DRAINAGE FROM 201D (EXTERNAL)
#*****
001:0075-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD     02:201D          28.90    .955 No_date  6:18  18.06  .422
  [CN= 86.0: N= 3.00]
  [Tp= .41:DT= 6.00]
#*****
# SUBCATCHMENT 201D ROUTED
# THROUGH Channel SMT-3
#*****
001:0076-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL   -> 02:201D          28.90    .955 No_date  6:18  18.06  n/a
  [RDT= 6.00] out<- 03:SMT-3R      28.90    .955 No_date  6:18  18.06  n/a
  [L/s/n= 100./ .700/.030]
  {Vmax= 1.039:Dmax= .600}
#*****
# DRAINAGE FROM CEMETERY LANDS D1a, D1b
#*****
001:0077-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD     02:D1a           1.90    .138 No_date  6:03  19.73  .461
  [CN= 88.0: N= 3.00]
  [Tp= .13:DT= 3.00]
001:0078-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  * CALIB NASHYD   07:D1b           1.90    .150 No_date  6:00  18.06  .422
  [CN= 86.0: N= 3.00]
  [Tp= .09:DT= 3.00]
#*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b
#*****
001:0079-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          02:D1a           1.90    .138 No_date  6:03  19.73  n/a
                + 03:SMT-3R      28.90    .955 No_date  6:18  18.06  n/a
                + 07:D1b           1.90    .150 No_date  6:00  18.06  n/a
  [DT= 3.00] SUM= 06:SMT3          32.70   1.034 No_date  6:18  18.16  n/a
#*****
# CONFLUENCE SMT 1-3
#*****
001:0080-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          01:SMT1          102.30   2.771 No_date  6:26  18.07  n/a
                + 04:SMT4          35.40    .922 No_date  6:15  19.75  n/a
                + 06:SMT3          32.70   1.034 No_date  6:18  18.16  n/a
  [DT= 2.00] SUM= 03:SMT1-3      170.40   4.613 No_date  6:24  18.44  n/a
#*****
# TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D
#*****
001:0081-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          01:SMT1          102.30   2.771 No_date  6:26  18.07  n/a
                + 04:SMT4          35.40    .922 No_date  6:15  19.75  n/a
                + 06:SMT3          32.70   1.034 No_date  6:18  18.16  n/a
                + 05:SMT2          83.60   2.211 No_date  6:24  18.29  n/a
  [DT= 2.00] SUM= 08:1201          254.00   6.824 No_date  6:24  18.39  n/a
001:0082-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL   -> 08:1201          254.00   6.824 No_date  6:24  18.39  n/a
  * [RDT= 2.00] out<- 03:002202      254.00   6.497 No_date  6:32  18.39  n/a
  [L/s/n= 475./1.050/.030]
  {Vmax= .937:Dmax= .439}
001:0083-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD     04:000202          21.60    .992 No_date  6:12  20.59  .481

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SWM.sum

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[CN= 86.8: N= 3.00]
[TP= .30:DT= 6.00]
001:0084-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:002202   254.00   6.497 No_date   6:32   18.39  n/a
                + 04:000202    21.60    .992 No_date   6:12   20.59  n/a
[DT= 2.00] SUM= 02:001202   275.60   7.099 No_date   6:30   18.56  n/a
001:0085-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     03:000203    26.30    1.414 No_date   6:06   20.59  .481
[CN= 86.8: N= 3.00]
[TP= .24:DT= 6.00]
001:0086-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:000203    26.30    1.414 No_date   6:06   20.59  n/a
                + 02:001202   275.60    7.099 No_date   6:30   18.56  n/a
[DT= 2.00] SUM= 04:000003   301.90    7.789 No_date   6:26   18.74  n/a
001:0087-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD        04:000003   301.90    7.789 No_date   6:26   18.74  n/a

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# SUBCATCHMENT 204 AREA REVISED
# NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha

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```

001:0088-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     02:000204    53.60    1.399 No_date   6:30   19.39  .453
[CN= 87.6: N= 3.00]
[TP= .63:DT= 6.00]
001:0089-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          02:000204    53.60    1.399 No_date   6:30   19.39  n/a
                + 04:000003   301.90    7.789 No_date   6:26   18.74  n/a
[DT= 2.00] SUM= 03:001204   355.50    9.158 No_date   6:26   18.84  n/a

```

```

# ROUTE through Channel 205 ELIMINATED, OUTSIDE OF STUDY AREA

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# SUBCATCHMENT 205 ELIMINATED, OUTSIDE OF STUDY AREA

```

```

# ID REVISED TO ID=9, PREVIOUSLY ID=1

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```

001:0090-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          09:001108   784.37    8.531 No_date   8:06   22.97  n/a
                + 03:001204   355.50    9.158 No_date   6:26   18.84  n/a
[DT= 2.00] SUM= 02:000008  1139.87   17.516 No_date   6:26   21.68  n/a
001:0091-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD        02:000008  1139.87   17.516 No_date   6:26   21.68  n/a

```

** END OF RUN : 1

RUN:COMMAND#

002:0001-----

START

```

[TZERO = .00 hrs on 0]
[METOUT= 2 (1=imperial, 2=metric output)]
[NSTORM= 1 ]
[NRUN = 2 ]

```

```

# Project Name: [Holy Family Catholic Cemetery] Project Number: [111063]
# Date : 08-16-2011
# Modeller : [c. silvestri]
# Company : Philips Engineering Ltd
# License # : 3569108

```

SWM.sum

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*****
002:0002-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
READ STORM
  Filename = STORM.001
  Comment = TOWN OF MILTON 12 HOUR 5 YEAR SCS STORM (1998 IDF DATA)
  [SDT=12.00:SDUR= 12.00:PTOT= 59.90]
002:0003-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:000103      42.10      2.620 No_date      6:18      33.36 .557
  [CN= 86.0: N= 3.00]
  [Tp= .40:DT= 6.00]
002:0004-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:000103      42.10      2.620 No_date      6:18      33.36 n/a
  [RDT= 6.00] out<- 02:002104      42.10      2.367 No_date      6:24      33.36 n/a
  [L/s/n= 440./1.000/.030]
  {Vmax= .674:Dmax= .523}
002:0005-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      03:000104      24.10      2.266 No_date      6:06      33.36 .557
  [CN= 86.0: N= 3.00]
  [Tp= .21:DT= 6.00]
002:0006-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:000104      24.10      2.266 No_date      6:06      33.36 n/a
  + 02:002104      42.10      2.367 No_date      6:24      33.36 n/a
  [DT= 6.00] SUM= 01:001104      66.20      3.774 No_date      6:12      33.36 n/a
002:0007-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:001104      66.20      3.774 No_date      6:12      33.36 n/a
  [RDT= 6.00] out<- 02:002105      66.20      3.330 No_date      6:24      33.36 n/a
  [L/s/n= 365./ .400/.030]
  {Vmax= .447:Dmax= .501}
002:0008-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:000105      19.20      2.033 No_date      6:00      34.31 .573
  [CN= 86.8: N= 3.00]
  [Tp= .18:DT= 6.00]
002:0009-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:000105      19.20      2.033 No_date      6:00      34.31 n/a
  + 02:002105      66.20      3.330 No_date      6:24      33.36 n/a
  [DT= 6.00] SUM= 01:001105      85.40      4.327 No_date      6:12      33.57 n/a
002:0010-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:001105      85.40      4.327 No_date      6:12      33.57 n/a
  [RDT= 6.00] out<- 02:002106      85.40      4.052 No_date      6:24      33.57 n/a
  [L/s/n= 385./ .670/.030]
  {Vmax= .643:Dmax= .514}
002:0011-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:000106      15.30      1.704 No_date      6:00      34.79 .581
  [CN= 87.2: N= 3.00]
  [Tp= .17:DT= 6.00]
002:0012-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:000106      15.30      1.704 No_date      6:00      34.79 n/a
  + 02:002106      85.40      4.052 No_date      6:24      33.57 n/a
  [DT= 6.00] SUM= 01:001106      100.70      4.757 No_date      6:18      33.76 n/a
002:0013-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 03:000107      15.27      .416 No_date      6:00      39.17 .654
  [XIMP=.10:TIMP=.17]
  [LOSS= 2 :CN= 88.0]
  [Pervious area: IAPER= 2.50:SLPP=1.27:LGP= 717.:MNP=.250:SCP= .0]
  [Impervious area: IAIMP= 1.57:SLPI=1.27:LGI= 100.:MNI=.017:SCI= .0]
002:0014-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:001106      100.70      4.757 No_date      6:18      33.76 n/a
  + 03:000107      15.27      .416 No_date      6:00      39.17 n/a
  [DT= 6.00] SUM= 02:001107      115.97      4.936 No_date      6:18      34.47 n/a
002:0015-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 02:001107      115.97      4.936 No_date      6:18      34.47 n/a
  [RDT= 6.00] out<- 01:002108      115.97      4.469 No_date      6:30      34.47 n/a
  [L/s/n= 1300./1.670/.030]
  {Vmax= 1.530:Dmax= .739}
002:0016-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

```

		SWM.Sum						
CALIB NASHYD	02:000108	33.50	2.609	No_date	6:12	34.31	.573	
[CN= 86.8: N= 3.00]								
[Tp= .29:DT= 6.00]								
002:0017	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ADD HYD	01:002108	115.97	4.469	No_date	6:30	34.47	n/a	
	+ 02:000108	33.50	2.609	No_date	6:12	34.31	n/a	
[DT= 6.00]	SUM= 03:000004	149.47	6.397	No_date	6:18	34.44	n/a	
002:0018	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
PRINT HYD	03:000004	149.47	6.397	No_date	6:18	34.44	n/a	
002:0019	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
CALIB STANDHYD	04:000101	287.80	5.852	No_date	6:30	40.72	.680	
[XIMP=.20:TIMP=.50]								
[LOSS= 2 :CN= 83.4]								
[Pervious area: IAper= 5.00:SLPP= .63:LGP= 700.:MNP=.250:SCP= .0]								
[Impervious area: IAimp= 1.57:SLPI= .63:LGI=3200.:MNI=.017:SCI= .0]								
002:0020	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ROUTE CHANNEL	-> 04:000101	287.80	5.852	No_date	6:30	40.72	n/a	
[RDT= 6.00]	out<- 05:002101	287.80	5.169	No_date	6:48	40.72	n/a	
[L/s/n= 700./ .420/.030]								
{Vmax= .590:Dmax= .627}								
002:0021	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
* CALIB STANDHYD	04:000102	272.90	9.096	No_date	6:00	35.71	.596	
[XIMP=.13:TIMP=.28]								
[LOSS= 2 :CN= 84.0]								
[Pervious area: IAper= 5.00:SLPP= .98:LGP=1350.:MNP=.250:SCP= .0]								
[Impervious area: IAimp= 1.57:SLPI= .98:LGI= 40.:MNI=.017:SCI= .0]								
002:0022	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ADD HYD	04:000102	272.90	9.096	No_date	6:00	35.71	n/a	
	+ 05:002101	287.80	5.169	No_date	6:48	40.72	n/a	
[DT= 6.00]	SUM= 06:000001	560.70	10.973	No_date	7:24	38.28	n/a	
002:0023	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
PRINT HYD	06:000001	560.70	10.973	No_date	7:24	38.28	n/a	
002:0024	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ROUTE CHANNEL	-> 06:000001	560.70	10.973	No_date	7:24	38.28	n/a	
[RDT= 6.00]	out<- 04:002109	560.70	10.670	No_date	7:30	38.28	n/a	
[L/s/n= 1000./ .540/.030]								
{Vmax= 1.003:Dmax= .890}								
002:0025	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
CALIB NASHYD	05:000109	35.10	2.633	No_date	6:12	34.31	.573	
[CN= 86.8: N= 3.00]								
[Tp= .32:DT= 6.00]								
002:0026	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ADD HYD	04:002109	560.70	10.670	No_date	7:30	38.28	n/a	
	+ 05:000109	35.10	2.633	No_date	6:12	34.31	n/a	
[DT= 6.00]	SUM= 06:001109	595.80	11.000	No_date	7:30	38.05	n/a	
002:0027	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ROUTE CHANNEL	-> 06:001109	595.80	11.000	No_date	7:30	38.05	n/a	
[RDT= 6.00]	out<- 04:002110	595.80	10.801	No_date	7:48	38.05	n/a	
[L/s/n= 900./ .710/.030]								
{Vmax= .849:Dmax= .763}								
002:0028	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
CALIB NASHYD	05:000110	21.80	2.112	No_date	6:06	34.79	.581	
[CN= 87.2: N= 3.00]								
[Tp= .22:DT= 6.00]								
002:0029	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ADD HYD	04:002110	595.80	10.801	No_date	7:48	38.05	n/a	
	+ 05:000110	21.80	2.112	No_date	6:06	34.79	n/a	
[DT= 6.00]	SUM= 06:001110	617.60	10.976	No_date	7:48	37.93	n/a	
002:0030	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ROUTE CHANNEL	-> 06:001110	617.60	10.976	No_date	7:48	37.93	n/a	
[RDT= 6.00]	out<- 04:002111	617.60	10.929	No_date	7:54	37.93	n/a	
[L/s/n= 920./1.250/.030]								
{Vmax= 1.316:Dmax= .648}								
002:0031	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
CALIB NASHYD	01:000111	17.30	1.556	No_date	6:06	33.83	.565	

SWM.sum

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[CN= 86.4: N= 3.00]
[TP= .23:DT= 6.00]
002:0032-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:000111    17.30    1.556 No_date    6:06    33.83  n/a
                + 04:002111    617.60   10.929 No_date    7:54    37.93  n/a
[DT= 6.00] SUM= 02:000002    634.90   11.066 No_date    7:54    37.82  n/a
002:0033-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD        02:000002    634.90   11.066 No_date    7:54    37.82  n/a
*****
# ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN
002:0034-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:000004    149.47    6.397 No_date    6:18    34.44  n/a
                + 02:000002    634.90   11.066 No_date    7:54    37.82  n/a
[DT= 6.00] SUM= 09:001108    784.37   15.005 No_date    6:24    37.18  n/a
*****
# SUBCATCHMENT CONTAINING CEMETERY LANDS
# PROPOSED IMPERVIOUSNESS LESS THAN 20%
# THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURF
#
# DRAINAGE FROM 201A (EXTERNAL)
#
002:0035-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     01:201A     68.20    3.579 No_date    6:18    31.31  .523
[CN= 86.0: N= 3.00]
[TP= .47:DT= 6.00]
#Route NHYD=201A through Channel SMT-2
002:0036-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:201A     68.20    3.579 No_date    6:18    31.31  n/a
[RDT= 6.00] out<- 02:SMT-2R  68.20    3.503 No_date    6:24    31.31  n/a
[L/S/n= 450./ .750/.030]
[Vmax= 1.190:Dmax= .534]
*****
# DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d
#
002:0037-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     01:A1a      .80      .066 No_date    6:06    33.28  .556
[CN= 87.7: N= 3.00]
[TP= .27:DT= 6.00]
002:0038-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD     03:A1b     6.10     .892 No_date    6:00    31.46  .525
[CN= 86.1: N= 3.00]
[TP= .07:DT= 3.00]
002:0039-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     04:A1c     3.20     .374 No_date    6:03    32.74  .547
[CN= 87.2: N= 3.00]
[TP= .14:DT= 3.00]
002:0040-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     06:A1d     5.30     .499 No_date    6:06    32.82  .548
[CN= 87.3: N= 3.00]
[TP= .21:DT= 6.00]
002:0041-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 06:A1d     5.30     .499 No_date    6:06    32.82  n/a
[RDT= 6.00] out<- 07:A1d     5.30     .167 No_date    6:30    32.82  n/a
overflow <= 08:OVR      .00      .000 No_date    0:00     .00  n/a
{MxStoUsed=,7395E-01, TotovfVo]=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
002:0042-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          07:A1d     5.30     .167 No_date    6:30    32.82  n/a
                + 08:OVR      .00      .000 No_date    0:00     .00  n/a
[DT= 6.00] SUM= 06:A1dPND    5.30     .167 No_date    6:30    32.82  n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d
#

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                                SWM.sum
002:0043-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  ADD HYD          01:A1a          .80          .066 No_date    6:06    33.28  n/a
                   + 02:SMT-2R    68.20         3.503 No_date    6:24    31.31  n/a
                   + 03:A1b         6.10          .892 No_date    6:00    31.46  n/a
                   + 04:A1c         3.20          .374 No_date    6:03    32.74  n/a
                   + 06:A1dPND     5.30          .167 No_date    6:30    32.82  n/a
    [DT= 3.00] SUM= 05:SMT2     83.60         3.918 No_date    6:24    31.55  n/a
*****
# DRAINAGE FROM 201B (EXTERNAL)
*****
002:0044-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  CALIB NASHYD     01:201B        13.40         .942 No_date    6:12    31.31  .523
    [CN= 86.0: N= 3.00]
    [Tp= .31:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)
*****
002:0045-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  CALIB NASHYD     02:B1a         4.60          .484 No_date    6:03    32.48  .542
    [CN= 87.0: N= 3.00]
    [Tp= .17:DT= 3.00]
002:0046-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  ROUTE RESERVOIR -> 02:B1a         4.60          .484 No_date    6:03    32.48  n/a
    [RDT= 3.00] out<- 04:B1a         4.60          .185 No_date    6:24    32.48  n/a
    overflow <= 08:OVR          .00          .000 No_date    0:00         .00  n/a
    {MxStoUsed=.5711E-01, TotOvfVol=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
002:0047-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  ADD HYD          04:B1a         4.60          .185 No_date    6:24    32.48  n/a
                   + 08:OVR          .00          .000 No_date    0:00         .00  n/a
    [DT= 3.00] SUM= 02:B1aPND     4.60          .185 No_date    6:24    32.48  n/a
002:0048-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  ADD HYD          01:201B        13.40         .942 No_date    6:12    31.31  n/a
                   + 02:B1aPND     4.60          .185 No_date    6:24    32.48  n/a
    [DT= 3.00] SUM= 03:201B        18.00         1.113 No_date    6:12    31.61  n/a
*****
# Route NHYD=201B + B1a through Channel SMT-4
*****
002:0049-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  ROUTE CHANNEL   -> 03:201B        18.00         1.113 No_date    6:12    31.61  n/a
  * [RDT= 3.00] out<- 01:SMT-4R    18.00         .979 No_date    6:21    31.61  n/a
    [L/s/n= 600./ .850/.030]
    {Vmax= .943:Dmax= .342}
002:0050-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  CALIB NASHYD     03:B1b         5.00          .509 No_date    6:03    31.47  .525
    [CN= 86.1: N= 3.00]
    [Tp= .17:DT= 3.00]
002:0051-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  CALIB NASHYD     04:B1c         1.00          .138 No_date    6:00    33.30  .556
    [CN= 87.7: N= 3.00]
    [Tp= .10:DT= 3.00]
002:0052-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  ADD HYD          03:B1b         5.00          .509 No_date    6:03    31.47  n/a
                   + 04:B1c         1.00          .138 No_date    6:00    33.30  n/a
    [DT= 3.00] SUM= 02:B1b/c         6.00          .634 No_date    6:03    31.77  n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c
*****
002:0053-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-
  ADD HYD          01:SMT-4R    18.00         .979 No_date    6:21    31.61  n/a
                   + 02:B1b/c         6.00          .634 No_date    6:03    31.77  n/a
    [DT= 3.00] SUM= 03:B1East     24.00         1.316 No_date    6:12    31.65  n/a
*****
# DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)
*****
002:0054-----ID:NHYD-----AREA---QPEAK-TpeakDate_hh:mm---R.V.-R.C.-

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SWM.sum
* CALIB STANDHYD 01:B1d 4.30 .678 No_date 6:00 38.43 .642
[XIMP=.25:TIMP=.25]
[LOSS= 2 :CN= 86.0]
[Pervious area: IAper= 5.00:SLPP= .85:LGP= 30.:MNP=.035:SCP= .0]
[Impervious area: IAimp= .50:SLPI= .85:LGI= 50.:MNI=.013:SCI= .0]
002:0055-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE RESERVOIR -> 01:B1d 4.30 .678 No_date 6:00 38.43 n/a
[RDT= 3.00] out<- 04:B1d 4.30 .160 No_date 6:15 38.43 n/a
overflow <= 08:OVR .00 .000 No_date 0:00 .00 n/a
{MxStoUsed=.7671E-01, TotOvfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
002:0056-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 04:B1d 4.30 .160 No_date 6:15 38.43 n/a
+ 08:OVR .00 .000 No_date 0:00 .00 n/a
[DT= 3.00] SUM= 01:B1dPND 4.30 .160 No_date 6:15 38.43 n/a
002:0057-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 02:B1f 3.50 .457 No_date 6:00 32.88 .549
[CN= 87.4: N= 3.00]
[Tp= .11:DT= 3.00]
002:0058-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1f 3.50 .457 No_date 6:00 32.88 n/a
[RDT= 3.00] out<- 04:B1f 3.50 .100 No_date 6:21 32.88 n/a
overflow <= 08:OVR .00 .000 No_date 0:00 .00 n/a
{MxStoUsed=.5322E-01, TotOvfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
002:0059-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 04:B1f 3.50 .100 No_date 6:21 32.88 n/a
+ 08:OVR .00 .000 No_date 0:00 .00 n/a
[DT= 3.00] SUM= 02:B1fPND 3.50 .100 No_date 6:21 32.88 n/a
002:0060-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
* CALIB STANDHYD 07:B1e 3.60 .599 No_date 6:00 38.88 .649
[XIMP=.27:TIMP=.27]
[LOSS= 2 :CN= 86.0]
[Pervious area: IAper= 5.00:SLPP=1.15:LGP= 30.:MNP=.035:SCP= .0]
[Impervious area: IAimp= .50:SLPI=1.15:LGI= 50.:MNI=.013:SCI= .0]
002:0061-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE RESERVOIR -> 07:B1e 3.60 .599 No_date 6:00 38.88 n/a
[RDT= 3.00] out<- 06:B1e 3.60 .118 No_date 6:15 38.88 n/a
overflow <= 08:OVR .00 .000 No_date 0:00 .00 n/a
{MxStoUsed=.7088E-01, TotOvfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
002:0062-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 06:B1e 3.60 .118 No_date 6:15 38.88 n/a
+ 08:OVR .00 .000 No_date 0:00 .00 n/a
[DT= 3.00] SUM= 07:B1ePND 3.60 .118 No_date 6:15 38.88 n/a
002:0063-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 01:B1dPND 4.30 .160 No_date 6:15 38.43 n/a
+ 02:B1west 3.50 .100 No_date 6:21 32.88 n/a
+ 07:B1ePND 3.60 .118 No_date 6:15 38.88 n/a
[DT= 3.00] SUM= 02:B1west 11.40 .377 No_date 6:15 36.87 n/a
#*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
#*****
002:0064-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 02:B1west 11.40 .377 No_date 6:15 36.87 n/a
+ 03:B1East 24.00 1.316 No_date 6:12 31.65 n/a
[DT= 3.00] SUM= 04:SMT4 35.40 1.691 No_date 6:12 33.33 n/a
#*****
# DRAINAGE FROM 201C (EXTERNAL)
#*****
002:0065-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 01:201C 91.00 4.591 No_date 6:24 31.31 .523
[CN= 86.0: N= 3.00]
[Tp= .50:DT= 6.00]
#*****
# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
#*****
002:0066-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-

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                                SWM.sum
CALIB NASHYD      02:C1a      7.00      .627 No_date      6:06      31.31 .523
  [CN= 86.0: N= 3.00]
  [Tp= .21:DT= 6.00]
*****
# C1a SWM FACILITY
*****
002:0067-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:C1a      7.00      .627 No_date      6:06      31.31 n/a
  [RDT= 6.00] out<- 06:C1a      7.00      .228 No_date      6:30      31.31 n/a
    overflow <= 08:OVR      .00      .000 No_date      0:00      .00 n/a
  {MxStoUsed=.8510E-01, TotovfVo=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
*****
# DISCHARGE FROM C1a SWM FACILITY
*****
002:0068-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      06:C1a      7.00      .228 No_date      6:30      31.31 n/a
      + 08:OVR      .00      .000 No_date      0:00      .00 n/a
  [DT= 6.00] SUM= 02:C1aPND      7.00      .228 No_date      6:30      31.31 n/a
002:0069-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:C1b      .50      .079 No_date      6:00      31.92 .533
  [CN= 86.5: N= 3.00]
  [Tp= .04:DT= 2.00]
*****
# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
*****
002:0070-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      01:201C      91.00      4.591 No_date      6:24      31.31 n/a
      + 02:EX+MC      7.00      .228 No_date      6:30      31.31 n/a
      + 03:C1b      .50      .079 No_date      6:00      31.92 n/a
  [DT= 2.00] SUM= 02:EX+MC      98.50      4.826 No_date      6:24      31.31 n/a
*****
# Route NHYD=201C through Channel SMT-1
*****
002:0071-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 02:EX+MC      98.50      4.826 No_date      6:24      31.31 n/a
* [RDT= 2.00] out<- 01:SMT-1      98.50      4.720 No_date      6:28      31.31 n/a
  [L/S/n= 275./ .500/.030]
  {Vmax= .988:Dmax= .620}
002:0072-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      07:C2      3.80      .387 No_date      6:03      31.47 .525
  [CN= 86.1: N= 3.00]
  [Tp= .17:DT= 3.00]
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS
# EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2
*****
002:0073-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      01:SMT1      98.50      4.720 No_date      6:28      31.31 n/a
      + 07:C2      3.80      .387 No_date      6:03      31.47 n/a
  [DT= 2.00] SUM= 01:SMT1      102.30      4.832 No_date      6:26      31.32 n/a
*****
# CONFLUENCE SMT 1-4
*****
002:0074-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      04:SMT4      35.40      1.691 No_date      6:12      33.33 n/a
      + 01:SMT1      102.30      4.832 No_date      6:26      31.32 n/a
  [DT= 2.00] SUM= 02:SMT1-4      137.70      6.342 No_date      6:24      31.84 n/a
*****
# DRAINAGE FROM 201D (EXTERNAL)
*****
002:0075-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:201D      28.90      1.681 No_date      6:18      31.31 .523
  [CN= 86.0: N= 3.00]
  [Tp= .41:DT= 6.00]
*****

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SWM.sum

SUBCATCHMENT 201D ROUTED
THROUGH Channel SMT-3

002:0076-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 02:201D 28.90 1.681 No_date 6:18 31.31 n/a
[RDT= 6.00] out<- 03:SMT-3R 28.90 1.686 No_date 6:18 31.31 n/a
[L/s/n= 100./ .700/.030]
{Vmax= 1.201:Dmax= .745}

DRAINAGE FROM CEMETERY LANDS D1a, D1b

002:0077-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 02:D1a 1.90 .234 No_date 6:03 33.65 .562
[CN= 88.0: N= 3.00]
[Tp= .13:DT= 3.00]

002:0078-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD 07:D1b 1.90 .257 No_date 6:00 31.31 .523
[CN= 86.0: N= 3.00]
[Tp= .09:DT= 3.00]

TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b

002:0079-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 02:D1a 1.90 .234 No_date 6:03 33.65 n/a
+ 03:SMT-3R 28.90 1.686 No_date 6:18 31.31 n/a
+ 07:D1b 1.90 .257 No_date 6:00 31.31 n/a
[DT= 3.00] SUM= 06:SMT3 32.70 1.832 No_date 6:12 31.45 n/a

CONFLUENCE SMT 1-3

002:0080-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT1 102.30 4.832 No_date 6:26 31.32 n/a
+ 04:SMT4 35.40 1.691 No_date 6:12 33.33 n/a
+ 06:SMT3 32.70 1.832 No_date 6:12 31.45 n/a
[DT= 2.00] SUM= 03:SMT1-3 170.40 8.070 No_date 6:22 31.76 n/a

TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D

002:0081-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT1 102.30 4.832 No_date 6:26 31.32 n/a
+ 04:SMT4 35.40 1.691 No_date 6:12 33.33 n/a
+ 06:SMT3 32.70 1.832 No_date 6:12 31.45 n/a
+ 05:SMT2 83.60 3.918 No_date 6:24 31.55 n/a
[DT= 2.00] SUM= 08:1201 254.00 11.975 No_date 6:24 31.69 n/a

002:0082-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 08:1201 254.00 11.975 No_date 6:24 31.69 n/a
* [RDT= 2.00] out<- 03:002202 254.00 11.518 No_date 6:30 31.69 n/a
[L/s/n= 475./1.050/.030]
{Vmax= .996:Dmax= .547}

002:0083-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 04:000202 21.60 1.661 No_date 6:12 34.31 .573
[CN= 86.8: N= 3.00]
[Tp= .30:DT= 6.00]

002:0084-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:002202 254.00 11.518 No_date 6:30 31.69 n/a
+ 04:000202 21.60 1.661 No_date 6:12 34.31 n/a
[DT= 2.00] SUM= 02:001202 275.60 12.594 No_date 6:28 31.90 n/a

002:0085-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 03:000203 26.30 2.371 No_date 6:06 34.31 .573
[CN= 86.8: N= 3.00]
[Tp= .24:DT= 6.00]

002:0086-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000203 26.30 2.371 No_date 6:06 34.31 n/a
+ 02:001202 275.60 12.594 No_date 6:28 31.90 n/a
[DT= 2.00] SUM= 04:000003 301.90 13.840 No_date 6:24 32.11 n/a

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                                SWM.sum
002:0087-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD          04:000003   301.90   13.840 No_date   6:24   32.11 n/a
*****
# SUBCATCHMENT 204 AREA REVISED
# NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha
*****
002:0088-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:000204   53.60    2.443 No_date   6:30   33.17 .554
  [CN= 87.6: N= 3.00]
  [Tp= .63:DT= 6.00]
002:0089-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           02:000204   53.60    2.443 No_date   6:30   33.17 n/a
                + 04:000003   301.90   13.840 No_date   6:24   32.11 n/a
  [DT= 2.00] SUM= 03:001204   355.50   16.223 No_date   6:24   32.27 n/a
*****
# ROUTE through Channel 205 ELIMINATED, OUTSIDE OF STUDY AREA
*****
# SUBCATCHMENT 205 ELIMINTATED, OUTSIDE OF STUDY AREA
*****
# ID REVISED TO ID=9, PREVIOUSLY ID=1
*****
002:0090-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           09:001108   784.37   15.005 No_date   6:24   37.18 n/a
                + 03:001204   355.50   16.223 No_date   6:24   32.27 n/a
  [DT= 2.00] SUM= 02:000008  1139.87   31.228 No_date   6:24   35.64 n/a
002:0091-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD         02:000008  1139.87   31.228 No_date   6:24   35.64 n/a
*****
** END OF RUN : 2

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RUN:COMMAND#

```

003:0001-----
START
  [TZERO = .00 hrs on 0]
  [METOUT= 2 (1=imperial, 2=metric output)]
  [NSTORM= 1 ]
  [NRUN = 3 ]
*****
# Project Name: [Holy Family Catholic Cemetery] Project Number: [111063]
# Date : 08-16-2011
# Modeller : [C. Silvestri]
# Company : Philips Engineering Ltd
# License # : 3569108
*****

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003:0002-----
READ STORM
  Filename = STORM.001
  Comment = TOWN OF MILTON 12 HOUR 10 YEAR SCS STORM (1998 IDF DATA)
  [SDT=12.00:SDUR= 12.00:PTOT= 71.35]
003:0003-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:000103   42.10    3.384 No_date   6:18   43.02 .603
  [CN= 86.0: N= 3.00]
  [Tp= .40:DT= 6.00]
003:0004-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:000103   42.10    3.384 No_date   6:18   43.02 n/a
  [RDT= 6.00] out<- 02:002104   42.10    3.104 No_date   6:24   43.02 n/a
  [L/s/n= 440./1.000/.030]

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SWM.sum

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{Vmax= .706:Dmax= .548}
003:0005-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD      03:000104    24.10    2.918 No_date    6:06    43.02 .603
[CN= 86.0: N= 3.00]
[Tp= .21:DT= 6.00]
003:0006-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          03:000104    24.10    2.918 No_date    6:06    43.02 n/a
                + 02:002104    42.10    3.104 No_date    6:24    43.02 n/a
[DT= 6.00] SUM= 01:001104    66.20    4.951 No_date    6:12    43.02 n/a
003:0007-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL   -> 01:001104    66.20    4.951 No_date    6:12    43.02 n/a
[RDT= 6.00] out<- 02:002105    66.20    4.443 No_date    6:24    43.02 n/a
[L/S/n= 365./ .400/.030]
{Vmax= .485:Dmax= .528}
003:0008-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
* CALIB NASHYD   03:000105    19.20    2.617 No_date    6:00    44.11 .618
[CN= 86.8: N= 3.00]
[Tp= .18:DT= 6.00]
003:0009-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          03:000105    19.20    2.617 No_date    6:00    44.11 n/a
                + 02:002105    66.20    4.443 No_date    6:24    43.02 n/a
[DT= 6.00] SUM= 01:001105    85.40    5.810 No_date    6:12    43.26 n/a
003:0010-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL   -> 01:001105    85.40    5.810 No_date    6:12    43.26 n/a
[RDT= 6.00] out<- 02:002106    85.40    5.445 No_date    6:24    43.26 n/a
[L/S/n= 385./ .670/.030]
{Vmax= .688:Dmax= .549}
003:0011-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
* CALIB NASHYD   03:000106    15.30    2.188 No_date    6:00    44.67 .626
[CN= 87.2: N= 3.00]
[Tp= .17:DT= 6.00]
003:0012-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          03:000106    15.30    2.188 No_date    6:00    44.67 n/a
                + 02:002106    85.40    5.445 No_date    6:24    43.26 n/a
[DT= 6.00] SUM= 01:001106    100.70   6.468 No_date    6:12    43.48 n/a
003:0013-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
* CALIB STANDHYD 03:000107    15.27    .543 No_date    7:18    49.47 .693
[XIMP=.10:TIMP=.17]
[LOSS= 2 :CN= 88.0]
[Pervious area: IAper= 2.50:SLPP=1.27:LGP= 717.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI=1.27:LGI= 100.:MNI=.017:SCI= .0]
003:0014-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          01:001106    100.70   6.468 No_date    6:12    43.48 n/a
                + 03:000107    15.27    .543 No_date    7:18    49.47 n/a
[DT= 6.00] SUM= 02:001107    115.97   6.740 No_date    6:12    44.27 n/a
003:0015-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL   -> 02:001107    115.97   6.740 No_date    6:12    44.27 n/a
[RDT= 6.00] out<- 01:002108    115.97   6.271 No_date    6:24    44.27 n/a
[L/S/n= 1300./1.670/.030]
{Vmax= 1.756:Dmax= .885}
003:0016-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD     02:000108    33.50    3.352 No_date    6:12    44.11 .618
[CN= 86.8: N= 3.00]
[Tp= .29:DT= 6.00]
003:0017-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD          01:002108    115.97   6.271 No_date    6:24    44.27 n/a
                + 02:000108    33.50    3.352 No_date    6:12    44.11 n/a
[DT= 6.00] SUM= 03:000004    149.47   8.909 No_date    6:18    44.23 n/a
003:0018-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
PRINT HYD       03:000004    149.47   8.909 No_date    6:18    44.23 n/a
003:0019-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB STANDHYD  04:000101    287.80   7.769 No_date    6:30    51.12 .716
[XIMP=.20:TIMP=.50]
[LOSS= 2 :CN= 83.4]
[Pervious area: IAper= 5.00:SLPP= .63:LGP= 700.:MNP=.250:SCP= .0]

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SWM.sum

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[Impervious area: IAimp= 1.57:SLPI= .63:LGI=3200.:MNI=.017:SCI= .0]
003:0020-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL -> 04:000101 287.80 7.769 No_date 6:30 51.12 n/a
[RD= 6.00] out<- 05:002101 287.80 7.095 No_date 8:06 51.12 n/a
[L/S/n= 700./ .420/.030]
{Vmax= .629:Dmax= .665}
003:0021-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
* CALIB STANDHYD 04:000102 272.90 11.431 No_date 6:00 45.60 .639
[XIMP=.13:TIMP=.28]
[LOSS= 2 :CN= 84.0]
[Pervious area: IAper= 5.00:SLPP= .98:LGP=1350.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI= .98:LGI= 40.:MNI=.017:SCI= .0]
003:0022-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 04:000102 272.90 11.431 No_date 6:00 45.60 n/a
+ 05:002101 287.80 7.095 No_date 8:06 51.12 n/a
[DT= 6.00] SUM= 06:000001 560.70 15.616 No_date 7:12 48.44 n/a
003:0023-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
PRINT HYD 06:000001 560.70 15.616 No_date 7:12 48.44 n/a
003:0024-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL -> 06:000001 560.70 15.616 No_date 7:12 48.44 n/a
[RD= 6.00] out<- 04:002109 560.70 15.100 No_date 7:18 48.44 n/a
[L/S/n= 1000./ .540/.030]
{Vmax= 1.061:Dmax= .999}
003:0025-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 05:000109 35.10 3.387 No_date 6:12 44.11 .618
[CN= 86.8: N= 3.00]
[Tp= .32:DT= 6.00]
003:0026-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 04:002109 560.70 15.100 No_date 7:18 48.44 n/a
+ 05:000109 35.10 3.387 No_date 6:12 44.11 n/a
[DT= 6.00] SUM= 06:001109 595.80 15.601 No_date 7:18 48.18 n/a
003:0027-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL -> 06:001109 595.80 15.601 No_date 7:18 48.18 n/a
[RD= 6.00] out<- 04:002110 595.80 15.282 No_date 7:30 48.18 n/a
[L/S/n= 900./ .710/.030]
{Vmax= .917:Dmax= .824}
003:0028-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 05:000110 21.80 2.707 No_date 6:06 44.67 .626
[CN= 87.2: N= 3.00]
[Tp= .22:DT= 6.00]
003:0029-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 04:002110 595.80 15.282 No_date 7:30 48.18 n/a
+ 05:000110 21.80 2.707 No_date 6:06 44.67 n/a
[DT= 6.00] SUM= 06:001110 617.60 15.506 No_date 7:30 48.06 n/a
003:0030-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL -> 06:001110 617.60 15.506 No_date 7:30 48.06 n/a
[RD= 6.00] out<- 04:002111 617.60 15.514 No_date 7:36 48.06 n/a
[L/S/n= 920./1.250/.030]
{Vmax= 1.570:Dmax= .794}
003:0031-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 01:000111 17.30 2.004 No_date 6:06 43.56 .610
[CN= 86.4: N= 3.00]
[Tp= .23:DT= 6.00]
003:0032-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 01:000111 17.30 2.004 No_date 6:06 43.56 n/a
+ 04:002111 617.60 15.514 No_date 7:36 48.06 n/a
[DT= 6.00] SUM= 02:000002 634.90 15.688 No_date 7:36 47.93 n/a
003:0033-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
PRINT HYD 02:000002 634.90 15.688 No_date 7:36 47.93 n/a
#*****
# ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN
003:0034-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 03:000004 149.47 8.909 No_date 6:18 44.23 n/a
+ 02:000002 634.90 15.688 No_date 7:36 47.93 n/a
[DT= 6.00] SUM= 09:001108 784.37 20.743 No_date 6:24 47.23 n/a

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SWM.sum

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*****
# SUBCATCHMENT CONTAINING CEMETERY LANDS
*****
# PROPOSED IMPERVIOUSNESS LESS THAN 20%
# THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURF
#
*****
# DRAINAGE FROM 201A (EXTERNAL)
*****
003:0035-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:201A      68.20    4.704 No_date    6:18    40.88 .573
  [CN= 86.0: N= 3.00]
  [Tp= .47:DT= 6.00]
#Route NHYD=201A through Channel SMT-2
003:0036-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 01:201A      68.20    4.704 No_date    6:18    40.88 n/a
  [RDT= 6.00] out<- 02:SMT-2R    68.20    4.572 No_date    6:24    40.88 n/a
  [L/s/n= 450./ .750/.030]
  {Vmax= 1.219:Dmax= .580}
*****
# DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d
*****
003:0037-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:A1a        .80      .085 No_date    6:06    43.16 .605
  [CN= 87.7: N= 3.00]
  [Tp= .27:DT= 6.00]
003:0038-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:A1b        6.10     1.150 No_date    6:00    41.05 .575
  [CN= 86.1: N= 3.00]
  [Tp= .07:DT= 3.00]
003:0039-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      04:A1c        3.20     .483 No_date    6:03    42.54 .596
  [CN= 87.2: N= 3.00]
  [Tp= .14:DT= 3.00]
003:0040-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      06:A1d        5.30     .647 No_date    6:06    42.63 .597
  [CN= 87.3: N= 3.00]
  [Tp= .21:DT= 6.00]
003:0041-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 06:A1d        5.30     .647 No_date    6:06    42.63 n/a
  [RDT= 6.00] out<- 07:A1d        5.30     .204 No_date    6:30    42.63 n/a
  overflow <= 08:OVR          .00      .000 No_date    0:00     .00 n/a
  {MxStoUsed=.9833E-01, TotOvfVol=.0000E+00, N-Ovf= 0, TotDurovf= 0.hrs}
003:0042-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           07:A1d        5.30     .204 No_date    6:30    42.63 n/a
  + 08:OVR          .00      .000 No_date    0:00     .00 n/a
  [DT= 6.00] SUM= 06:A1dPND      5.30     .204 No_date    6:30    42.63 n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d
*****
003:0043-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:A1a        .80      .085 No_date    6:06    43.16 n/a
  + 02:SMT-2R      68.20    4.572 No_date    6:24    40.88 n/a
  + 03:A1b         6.10     1.150 No_date    6:00    41.05 n/a
  + 04:A1c         3.20     .483 No_date    6:03    42.54 n/a
  + 06:A1dPND      5.30     .204 No_date    6:30    42.63 n/a
  [DT= 3.00] SUM= 05:SMT2      83.60    5.093 No_date    6:24    41.14 n/a
*****
# DRAINAGE FROM 201B (EXTERNAL)
*****
003:0044-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:201B      13.40    1.232 No_date    6:12    40.88 .573
  [CN= 86.0: N= 3.00]
  [Tp= .31:DT= 6.00]

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SWM.sum

DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)

003:0045-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 02:B1a 4.60 .629 No_date 6:03 42.24 .592
[CN= 87.0: N= 3.00]
[Tp= .17:DT= 3.00]

003:0046-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1a 4.60 .629 No_date 6:03 42.24 n/a
[RDT= 3.00] out<- 04:B1a 4.60 .222 No_date 6:24 42.24 n/a
overflow <= 08:OVR .00 .000 No_date 0:00 .00 n/a
{MxStoUsed=.7621E-01, TotOvfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}

003:0047-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 04:B1a 4.60 .222 No_date 6:24 42.24 n/a
+ 08:OVR .00 .000 No_date 0:00 .00 n/a
[DT= 3.00] SUM= 02:B1aPND 4.60 .222 No_date 6:24 42.24 n/a

003:0048-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:201B 13.40 1.232 No_date 6:12 40.88 n/a
+ 02:B1aPND 4.60 .222 No_date 6:24 42.24 n/a
[DT= 3.00] SUM= 03:201B 18.00 1.440 No_date 6:12 41.23 n/a

Route NHYD=201B + B1a through Channel SMT-4

003:0049-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 03:201B 18.00 1.440 No_date 6:12 41.23 n/a
* [RDT= 3.00] out<- 01:SMT-4R 18.00 1.283 No_date 6:21 41.23 n/a
[L/S/n= 600./ .850/.030]
{Vmax= 1.004:Dmax= .376}

003:0050-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 03:B1b 5.00 .663 No_date 6:03 41.06 .575
[CN= 86.1: N= 3.00]
[Tp= .17:DT= 3.00]

003:0051-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 04:B1c 1.00 .178 No_date 6:00 43.19 .605
[CN= 87.7: N= 3.00]
[Tp= .10:DT= 3.00]

003:0052-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:B1b 5.00 .663 No_date 6:03 41.06 n/a
+ 04:B1c 1.00 .178 No_date 6:00 43.19 n/a
[DT= 3.00] SUM= 02:B1b/c 6.00 .824 No_date 6:03 41.42 n/a

TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c

003:0053-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT-4R 18.00 1.283 No_date 6:21 41.23 n/a
+ 02:B1b/c 6.00 .824 No_date 6:03 41.42 n/a
[DT= 3.00] SUM= 03:B1East 24.00 1.746 No_date 6:12 41.27 n/a

DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)

003:0054-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 01:B1d 4.30 .891 No_date 6:00 48.48 .679
[XIMP=.25:TIMP=.25]
[LOSS= 2 :CN= 86.0]
[Pervious area: IAPER= 5.00:SLPP= .85:LGP= 30.:MNP=.035:SCP= .0]
[Impervious area: IAIMP= .50:SLPI= .85:LGI= 50.:MNI=.013:SCI= .0]

003:0055-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 01:B1d 4.30 .891 No_date 6:00 48.48 n/a
[RDT= 3.00] out<- 04:B1d 4.30 .194 No_date 6:12 48.48 n/a
overflow <= 08:OVR .00 .000 No_date 0:00 .00 n/a

{MxStoUsed=.9826E-01, TotOvfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}

003:0056-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 04:B1d 4.30 .194 No_date 6:12 48.48 n/a
+ 08:OVR .00 .000 No_date 0:00 .00 n/a
[DT= 3.00] SUM= 01:B1dPND 4.30 .194 No_date 6:12 48.48 n/a

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SWM.sum
003:0057-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:B1f      3.50      .591 No_date      6:00      42.70 .598
[CN= 87.4: N= 3.00]
[TP= .11:DT= 3.00]
003:0058-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1f      3.50      .591 No_date      6:00      42.70 n/a
[RDT= 3.00] out<- 04:B1f      3.50      .120 No_date      6:21      42.70 n/a
overflow <= 08:OVR      .00      .000 No_date      0:00      .00 n/a
{MxStoUsed=.7078E-01, TotovfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
003:0059-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          04:B1f      3.50      .120 No_date      6:21      42.70 n/a
+ 08:OVR      .00      .000 No_date      0:00      .00 n/a
[DT= 3.00] SUM= 02:B1fPND      3.50      .120 No_date      6:21      42.70 n/a
003:0060-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 07:B1e      3.60      .757 No_date      6:00      48.95 .686
[XIMP=.27:TIMP=.27]
[LOSS= 2 :CN= 86.0]
[Pervious area: IAper= 5.00:SLPP=1.15:LGP= 30.:MNP=.035:SCP= .0]
[Impervious area: IAimp= .50:SLPI=1.15:LGI= 50.:MNI=.013:SCI= .0]
003:0061-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 07:B1e      3.60      .757 No_date      6:00      48.95 n/a
[RDT= 3.00] out<- 06:B1e      3.60      .147 No_date      6:12      48.95 n/a
overflow <= 08:OVR      .00      .000 No_date      0:00      .00 n/a
{MxStoUsed=.8931E-01, TotovfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
003:0062-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          06:B1e      3.60      .147 No_date      6:12      48.95 n/a
+ 08:OVR      .00      .000 No_date      0:00      .00 n/a
[DT= 3.00] SUM= 07:B1ePND      3.60      .147 No_date      6:12      48.95 n/a
003:0063-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:B1dPND      4.30      .194 No_date      6:12      48.48 n/a
+ 02:B1West      3.50      .120 No_date      6:21      42.70 n/a
+ 07:B1ePND      3.60      .147 No_date      6:12      48.95 n/a
[DT= 3.00] SUM= 02:B1West      11.40      .459 No_date      6:15      46.86 n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
*****
003:0064-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          02:B1West      11.40      .459 No_date      6:15      46.86 n/a
+ 03:B1East      24.00      1.746 No_date      6:12      41.27 n/a
[DT= 3.00] SUM= 04:SMT4      35.40      2.203 No_date      6:12      43.07 n/a
*****
# DRAINAGE FROM 201C (EXTERNAL)
*****
003:0065-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:201C      91.00      6.019 No_date      6:24      40.88 .573
[CN= 86.0: N= 3.00]
[TP= .50:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
*****
003:0066-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:C1a      7.00      .817 No_date      6:06      40.88 .573
[CN= 86.0: N= 3.00]
[TP= .21:DT= 6.00]
*****
# C1a SWM FACILITY
*****
003:0067-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:C1a      7.00      .817 No_date      6:06      40.88 n/a
[RDT= 6.00] out<- 06:C1a      7.00      .272 No_date      6:30      40.88 n/a
overflow <= 08:OVR      .00      .000 No_date      0:00      .00 n/a
{MxStoUsed=.1155E+00, TotovfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
*****
# DISCHARGE FROM C1a SWM FACILITY
*****

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                                SWM. sum
003:0068-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                06:C1a          7.00    .272 No_date    6:30    40.88  n/a
                        + 08:OVR          .00    .000 No_date    0:00     .00   n/a
  [DT= 6.00]  SUM= 02:C1aPND          7.00    .272 No_date    6:30    40.88  n/a
003:0069-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD          03:C1b           .50    .101 No_date    6:00    41.59  .583
  [CN= 86.5: N= 3.00]
  [Tp= .04:DT= 2.00]
#*****
# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
#*****
003:0070-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                01:201C         91.00    6.019 No_date    6:24    40.88  n/a
                        + 02:EX+MC         7.00    .272 No_date    6:30    40.88  n/a
                        + 03:C1b           .50    .101 No_date    6:00    41.59  n/a
  [DT= 2.00]  SUM= 02:EX+MC         98.50    6.300 No_date    6:24    40.88  n/a
#*****
# Route NHYD=201C through channel SMT-1
#*****
003:0071-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL  -> 02:EX+MC         98.50    6.300 No_date    6:24    40.88  n/a
* [RDT= 2.00] out<- 01:SMT-1         98.50    6.156 No_date    6:28    40.88  n/a
  [L/s/n= 275./ .500/.030]
  {Vmax= .972:Dmax= .669}
003:0072-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD          07:C2           3.80    .504 No_date    6:03    41.06  .575
  [CN= 86.1: N= 3.00]
  [Tp= .17:DT= 3.00]
#*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS
# EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2
#*****
003:0073-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                01:SMT1         98.50    6.156 No_date    6:28    40.88  n/a
                        + 07:C2           3.80    .504 No_date    6:03    41.06  n/a
  [DT= 2.00]  SUM= 01:SMT1        102.30    6.302 No_date    6:26    40.89  n/a
#*****
# CONFLUENCE SMT 1-4
#*****
003:0074-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                04:SMT4         35.40    2.203 No_date    6:12    43.07  n/a
                        + 01:SMT1        102.30    6.302 No_date    6:26    40.89  n/a
  [DT= 2.00]  SUM= 02:SMT1-4        137.70    8.236 No_date    6:24    41.45  n/a
#*****
# DRAINAGE FROM 201D (EXTERNAL)
#*****
003:0075-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD          02:201D         28.90    2.202 No_date    6:18    40.88  .573
  [CN= 86.0: N= 3.00]
  [Tp= .41:DT= 6.00]
#*****
# SUBCATCHMENT 201D ROUTED
# THROUGH channel SMT-3
#*****
003:0076-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL  -> 02:201D         28.90    2.202 No_date    6:18    40.88  n/a
  [RDT= 6.00] out<- 03:SMT-3R         28.90    2.209 No_date    6:18    40.88  n/a
  [L/s/n= 100./ .700/.030]
  {Vmax= 1.285:Dmax= .824}
#*****
# DRAINAGE FROM CEMETERY LANDS D1a, D1b
#*****
003:0077-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD          02:D1a           1.90    .301 No_date    6:03    43.58  .611
  [CN= 88.0: N= 3.00]

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SWM.sum

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[Tp= .13:DT= 3.00]
003:0078-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      07:D1b      1.90      .333 No_date    6:00    40.88 .573
  [CN= 86.0: N= 3.00]
  [Tp= .09:DT= 3.00]
#*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b
#*****
003:0079-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           02:D1a      1.90      .301 No_date    6:03    43.58 n/a
                   + 03:SMT-3R    28.90     2.209 No_date    6:18    40.88 n/a
                   + 07:D1b      1.90      .333 No_date    6:00    40.88 n/a
  [DT= 3.00] SUM= 06:SMT3    32.70     2.406 No_date    6:12    41.04 n/a
#*****
# CONFLUENCE SMT 1-3
#*****
003:0080-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           01:SMT1    102.30    6.302 No_date    6:26    40.89 n/a
                   + 04:SMT4     35.40     2.203 No_date    6:12    43.07 n/a
                   + 06:SMT3     32.70     2.406 No_date    6:12    41.04 n/a
  [DT= 2.00] SUM= 03:SMT1-3  170.40   10.500 No_date    6:20    41.37 n/a
#*****
# TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D
#*****
003:0081-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           01:SMT1    102.30    6.302 No_date    6:26    40.89 n/a
                   + 04:SMT4     35.40     2.203 No_date    6:12    43.07 n/a
                   + 06:SMT3     32.70     2.406 No_date    6:12    41.04 n/a
                   + 05:SMT2     83.60     5.093 No_date    6:24    41.14 n/a
  [DT= 2.00] SUM= 08:1201    254.00   15.564 No_date    6:24    41.29 n/a
003:0082-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* ROUTE CHANNEL  -> 08:1201    254.00   15.564 No_date    6:24    41.29 n/a
  [RDT= 2.00] out<- 03:002202  254.00   15.058 No_date    6:30    41.29 n/a
  [L/S/n= 475./1.050/.030]
  {vmax= 1.038:Dmax= .608}
003:0083-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD     04:000202  21.60     2.136 No_date    6:12    44.11 .618
  [CN= 86.8: N= 3.00]
  [Tp= .30:DT= 6.00]
003:0084-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           03:002202  254.00   15.058 No_date    6:30    41.29 n/a
                   + 04:000202  21.60     2.136 No_date    6:12    44.11 n/a
  [DT= 2.00] SUM= 02:001202  275.60   16.484 No_date    6:26    41.52 n/a
003:0085-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD     03:000203  26.30     3.049 No_date    6:06    44.11 .618
  [CN= 86.8: N= 3.00]
  [Tp= .24:DT= 6.00]
003:0086-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           03:000203  26.30     3.049 No_date    6:06    44.11 n/a
                   + 02:001202  275.60   16.484 No_date    6:26    41.52 n/a
  [DT= 2.00] SUM= 04:000003  301.90   18.143 No_date    6:22    41.74 n/a
003:0087-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  PRINT HYD        04:000003  301.90   18.143 No_date    6:22    41.74 n/a
#*****
# SUBCATCHMENT 204 AREA REVISED
# NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha
#*****
003:0088-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD     02:000204  53.60     3.185 No_date    6:30    43.04 .603
  [CN= 87.6: N= 3.00]
  [Tp= .63:DT= 6.00]
003:0089-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           02:000204  53.60     3.185 No_date    6:30    43.04 n/a
                   + 04:000003  301.90   18.143 No_date    6:22    41.74 n/a
  [DT= 2.00] SUM= 03:001204  355.50   21.237 No_date    6:24    41.94 n/a

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SWM.sum

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*****
# ROUTE through Channel 205 ELIMINATED, OUTSIDE OF STUDY AREA
*****
# SUBCATCHMENT 205 ELIMINATED, OUTSIDE OF STUDY AREA
*****
# ID REVISED TO ID=9, PREVIOUSLY ID=1
*****
003:0090-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          09:001108    784.37    20.743 No_date    6:24    47.23  n/a
    + 03:001204    355.50    21.237 No_date    6:24    41.94  n/a
  [DT= 2.00] SUM= 02:000008    1139.87    41.980 No_date    6:24    45.58  n/a
003:0091-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  PRINT HYD        02:000008    1139.87    41.980 No_date    6:24    45.58  n/a
*****
** END OF RUN :    3

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RUN:COMMAND#

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004:0001-----
  START
  [TZERO = .00 hrs on 0]
  [METOUT= 2 (1=imperial, 2=metric output)]
  [NSTORM= 1 ]
  [NRUN = 4 ]
*****
# Project Name: [Holy Family Catholic Cemetery] Project Number: [111063]
# Date : 08-16-2011
# Modeller : [C. Silvestri]
# Company : Philips Engineering Ltd
# License # : 3569108
*****

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004:0002-----
  READ STORM
  Filename = STORM.001
  Comment = TOWN OF MILTON 12 HOUR 25 YEAR SCS STORM (1998 IDF DATA)
  [SDT=12.00:SDUR= 12.00:PTOT= 85.71]
004:0003-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD    01:000103    42.10    4.375 No_date    6:18    55.58  .649
  [CN= 86.0: N= 3.00]
  [Tp= .40:DT= 6.00]
004:0004-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL -> 01:000103    42.10    4.375 No_date    6:18    55.58  n/a
  [RDT= 6.00] out<- 02:002104    42.10    4.069 No_date    6:24    55.58  n/a
  [L/S/n= 440./1.000/.030]
  {Vmax= .746:Dmax= .578}
004:0005-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD    03:000104    24.10    3.761 No_date    6:06    55.58  .649
  [CN= 86.0: N= 3.00]
  [Tp= .21:DT= 6.00]
004:0006-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          03:000104    24.10    3.761 No_date    6:06    55.58  n/a
    + 02:002104    42.10    4.069 No_date    6:24    55.58  n/a
  [DT= 6.00] SUM= 01:001104    66.20    6.498 No_date    6:12    55.58  n/a
004:0007-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL -> 01:001104    66.20    6.498 No_date    6:12    55.58  n/a
  [RDT= 6.00] out<- 02:002105    66.20    5.922 No_date    6:24    55.58  n/a
  [L/S/n= 365./ .400/.030]
  {Vmax= .535:Dmax= .561}

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SWM.sum

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004:0008-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:000105   19.20   3.371 No_date   6:00   56.83 .663
  [CN= 86.8: N= 3.00]
  [Tp= .18:DT= 6.00]
004:0009-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           03:000105   19.20   3.371 No_date   6:00   56.83 n/a
    + 02:002105   66.20   5.922 No_date   6:24   55.58 n/a
  [DT= 6.00] SUM= 01:001105   85.40   7.819 No_date   6:12   55.86 n/a
004:0010-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL -> 01:001105   85.40   7.819 No_date   6:12   55.86 n/a
  [RDT= 6.00] out<- 02:002106   85.40   7.403 No_date   6:18   55.86 n/a
  [L/s/n= 385./ .670/.030]
  {Vmax= .752:Dmax= .593}
004:0011-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:000106   15.30   2.811 No_date   6:00   57.46 .670
  [CN= 87.2: N= 3.00]
  [Tp= .17:DT= 6.00]
004:0012-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           03:000106   15.30   2.811 No_date   6:00   57.46 n/a
    + 02:002106   85.40   7.403 No_date   6:18   55.86 n/a
  [DT= 6.00] SUM= 01:001106  100.70   8.785 No_date   6:12   56.11 n/a
004:0013-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD    03:000107   15.27   .773 No_date   7:00   62.69 .731
  [XIMP=.10:TIMP=.17]
  [LOSS= 2 :CN= 88.0]
  [Pervious area: IAper= 2.50:SLPP=1.27:LGP= 717.:MNP=.250:SCP= .0]
  [Impervious area: IAimp= 1.57:SLPI=1.27:LGI= 100.:MNI=.017:SCI= .0]
004:0014-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           01:001106  100.70   8.785 No_date   6:12   56.11 n/a
    + 03:000107   15.27   .773 No_date   7:00   62.69 n/a
  [DT= 6.00] SUM= 02:001107  115.97   9.202 No_date   6:12   56.97 n/a
004:0015-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL -> 02:001107  115.97   9.202 No_date   6:12   56.97 n/a
  [RDT= 6.00] out<- 01:002108  115.97   8.454 No_date   6:24   56.97 n/a
  [L/s/n= 1300./1.670/.030]
  {Vmax= 1.809:Dmax= .937}
004:0016-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD      02:000108   33.50   4.320 No_date   6:06   56.83 .663
  [CN= 86.8: N= 3.00]
  [Tp= .29:DT= 6.00]
004:0017-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           01:002108  115.97   8.454 No_date   6:24   56.97 n/a
    + 02:000108   33.50   4.320 No_date   6:06   56.83 n/a
  [DT= 6.00] SUM= 03:000004  149.47  11.991 No_date   6:18   56.94 n/a
004:0018-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  PRINT HYD         03:000004  149.47  11.991 No_date   6:18   56.94 n/a
004:0019-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB STANDHYD    04:000101  287.80  10.437 No_date   6:24   64.45 .752
  [XIMP=.20:TIMP=.50]
  [LOSS= 2 :CN= 83.4]
  [Pervious area: IAper= 5.00:SLPP= .63:LGP= 700.:MNP=.250:SCP= .0]
  [Impervious area: IAimp= 1.57:SLPI= .63:LGI=3200.:MNI=.017:SCI= .0]
004:0020-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL -> 04:000101  287.80  10.437 No_date   6:24   64.45 n/a
  [RDT= 6.00] out<- 05:002101  287.80   9.803 No_date   7:54   64.45 n/a
  [L/s/n= 700./ .420/.030]
  {Vmax= .693:Dmax= .718}
004:0021-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD    04:000102  272.90  14.475 No_date   6:00   58.41 .681
  [XIMP=.13:TIMP=.28]
  [LOSS= 2 :CN= 84.0]
  [Pervious area: IAper= 5.00:SLPP= .98:LGP=1350.:MNP=.250:SCP= .0]
  [Impervious area: IAimp= 1.57:SLPI= .98:LGI= 40.:MNI=.017:SCI= .0]
004:0022-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD           04:000102  272.90  14.475 No_date   6:00   58.41 n/a

```

```

                                SWM.sum
                                + 05:002101 287.80 9.803 No_date 7:54 64.45 n/a
                                [DT= 6.00] SUM= 06:000001 560.70 21.500 No_date 7:00 61.51 n/a
004:0023-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
PRINT HYD 06:000001 560.70 21.500 No_date 7:00 61.51 n/a
004:0024-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL -> 06:000001 560.70 21.500 No_date 7:00 61.51 n/a
[RDT= 6.00] out<- 04:002109 560.70 20.781 No_date 7:12 61.51 n/a
[L/S/n= 1000./ .540/.030]
{Vmax= 1.117:Dmax= 1.103}
004:0025-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 05:000109 35.10 4.361 No_date 6:12 56.83 .663
[CN= 86.8: N= 3.00]
[Tp= .32:DT= 6.00]
004:0026-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 04:002109 560.70 20.781 No_date 7:12 61.51 n/a
+ 05:000109 35.10 4.361 No_date 6:12 56.83 n/a
[DT= 6.00] SUM= 06:001109 595.80 21.502 No_date 7:12 61.23 n/a
004:0027-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL -> 06:001109 595.80 21.502 No_date 7:12 61.23 n/a
[RDT= 6.00] out<- 04:002110 595.80 21.186 No_date 7:24 61.23 n/a
[L/S/n= 900./ .710/.030]
{Vmax= 1.022:Dmax= .902}
004:0028-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 05:000110 21.80 3.471 No_date 6:06 57.46 .670
[CN= 87.2: N= 3.00]
[Tp= .22:DT= 6.00]
004:0029-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 04:002110 595.80 21.186 No_date 7:24 61.23 n/a
+ 05:000110 21.80 3.471 No_date 6:06 57.46 n/a
[DT= 6.00] SUM= 06:001110 617.60 21.487 No_date 7:18 61.10 n/a
004:0030-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ROUTE CHANNEL -> 06:001110 617.60 21.487 No_date 7:18 61.10 n/a
[RDT= 6.00] out<- 04:002111 617.60 21.666 No_date 7:18 61.10 n/a
[L/S/n= 920./1.250/.030]
{Vmax= 2.098:Dmax= .985}
004:0031-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 01:000111 17.30 2.582 No_date 6:06 56.20 .656
[CN= 86.4: N= 3.00]
[Tp= .23:DT= 6.00]
004:0032-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 01:000111 17.30 2.582 No_date 6:06 56.20 n/a
+ 04:002111 617.60 21.666 No_date 7:18 61.10 n/a
[DT= 6.00] SUM= 02:000002 634.90 21.913 No_date 7:18 60.97 n/a
004:0033-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
PRINT HYD 02:000002 634.90 21.913 No_date 7:18 60.97 n/a
*****
# ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN
004:0034-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
ADD HYD 03:000004 149.47 11.991 No_date 6:18 56.94 n/a
+ 02:000002 634.90 21.913 No_date 7:18 60.97 n/a
[DT= 6.00] SUM= 09:001108 784.37 29.062 No_date 6:24 60.20 n/a
*****
# SUBCATCHMENT CONTAINING CEMETERY LANDS
# PROPOSED IMPERVIOUSNESS LESS THAN 20%
# THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURF
#
# DRAINAGE FROM 201A (EXTERNAL)
004:0035-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-
CALIB NASHYD 01:201A 68.20 6.168 No_date 6:18 53.37 .623
[CN= 86.0: N= 3.00]
[Tp= .47:DT= 6.00]

```

SWM.sum

#Route NHYD=201A through Channel SMT-2

```
004:0036-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:201A      68.20   6.168 No_date   6:18   53.37 n/a
[RDT= 6.00] out<- 02:SMT-2R  68.20   5.939 No_date   6:24   53.37 n/a
[L/s/n= 450./ .750/.030]
{Vmax= 1.207:Dmax= .627}
```

DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d

```
004:0037-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:A1a      .80     .111 No_date   6:06   55.97 .653
[CN= 87.7: N= 3.00]
[Tp= .27:DT= 6.00]
```

```
004:0038-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:A1b      6.10    1.480 No_date   6:00   53.56 .625
[CN= 86.1: N= 3.00]
[Tp= .07:DT= 3.00]
```

```
004:0039-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      04:A1c      3.20    .623 No_date   6:03   55.27 .645
[CN= 87.2: N= 3.00]
[Tp= .14:DT= 3.00]
```

```
004:0040-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      06:A1d      5.30    .836 No_date   6:06   55.38 .646
[CN= 87.3: N= 3.00]
[Tp= .21:DT= 6.00]
```

```
004:0041-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 06:A1d      5.30    .836 No_date   6:06   55.38 n/a
[RDT= 6.00] out<- 07:A1d      5.30    .243 No_date   6:30   55.38 n/a
overflow <= 08:OVR      .00     .000 No_date   0:00    .00 n/a
{MxStoUsed=.1317E+00, TotOvfVol=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
```

```
004:0042-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           07:A1d      5.30    .243 No_date   6:30   55.38 n/a
+ 08:OVR          .00     .000 No_date   0:00    .00 n/a
[DT= 6.00] SUM= 06:A1dPND  5.30    .243 No_date   6:30   55.38 n/a
```

TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d

```
004:0043-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:A1a      .80     .111 No_date   6:06   55.97 n/a
+ 02:SMT-2R      68.20    5.939 No_date   6:24   53.37 n/a
+ 03:A1b         6.10    1.480 No_date   6:00   53.56 n/a
+ 04:A1c         3.20    .623 No_date   6:03   55.27 n/a
+ 06:A1dPND      5.30    .243 No_date   6:30   55.38 n/a
[DT= 3.00] SUM= 05:SMT2    83.60    6.583 No_date   6:24   53.65 n/a
```

DRAINAGE FROM 201B (EXTERNAL)

```
004:0044-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:201B    13.40    1.607 No_date   6:12   53.36 .623
[CN= 86.0: N= 3.00]
[Tp= .31:DT= 6.00]
```

DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)

```
004:0045-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:B1a      4.60    .815 No_date   6:03   54.92 .641
[CN= 87.0: N= 3.00]
[Tp= .17:DT= 3.00]
```

```
004:0046-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1a      4.60    .815 No_date   6:03   54.92 n/a
[RDT= 3.00] out<- 04:B1a      4.60    .262 No_date   6:24   54.92 n/a
overflow <= 08:OVR      .00     .000 No_date   0:00    .00 n/a
{MxStoUsed=.1027E+00, TotOvfVol=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
```

```
004:0047-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           04:B1a      4.60    .262 No_date   6:24   54.92 n/a
```

```

                                SWM.sum
                                + 08:OVR                .00    .000 No_date    0:00    .00    n/a
                                + 02:B1aPND              4.60    .262 No_date    6:24    54.92  n/a
004:0048-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                01:201B                13.40    1.607 No_date    6:12    53.36  n/a
                                + 02:B1aPND              4.60    .262 No_date    6:24    54.92  n/a
                                + 03:201B                18.00    1.853 No_date    6:12    53.76  n/a
[DT= 3.00] SUM=
*****
# Route NHYD=201B + B1a through Channel SMT-4
*****
004:0049-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL -> 03:201B                18.00    1.853 No_date    6:12    53.76  n/a
  * [RDT= 3.00] out<- 01:SMT-4R          18.00    1.679 No_date    6:18    53.76  n/a
    [L/S/n= 600./ .850/.030]
    {Vmax= 1.071:Dmax= .414}
004:0050-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD          03:B1b                5.00    .863 No_date    6:03    53.58  .625
  [CN= 86.1: N= 3.00]
  [Tp= .17:DT= 3.00]
004:0051-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD          04:B1c                1.00    .229 No_date    6:00    56.01  .653
  [CN= 87.7: N= 3.00]
  [Tp= .10:DT= 3.00]
004:0052-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                03:B1b                5.00    .863 No_date    6:03    53.58  n/a
                                + 04:B1c                1.00    .229 No_date    6:00    56.01  n/a
                                + 02:B1b/c              6.00    1.069 No_date    6:03    53.98  n/a
[DT= 3.00] SUM=
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c
*****
004:0053-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                01:SMT-4R          18.00    1.679 No_date    6:18    53.76  n/a
                                + 02:B1b/c              6.00    1.069 No_date    6:03    53.98  n/a
                                + 03:B1East            24.00    2.306 No_date    6:09    53.82  n/a
[DT= 3.00] SUM=
*****
# DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)
*****
004:0054-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  * CALIB STANDHYD      01:B1d                4.30    1.131 No_date    6:00    61.44  .717
  [XIMP=.25:TIMP=.25]
  [LOSS= 2 :CN= 86.0]
  [Pervious area: IAPER= 5.00:SLPP= .85:LGP= 30.:MNP=.035:SCP= .0]
  [Impervious area: IAimp= .50:SLPI= .85:LGI= 50.:MNI=.013:SCI= .0]
004:0055-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE RESERVOIR -> 01:B1d                4.30    1.131 No_date    6:00    61.44  n/a
  [RDT= 3.00] out<- 04:B1d                4.30    .227 No_date    6:12    61.44  n/a
  overflow <= 08:OVR                .00    .000 No_date    0:00    .00    n/a
  {MxStoUsed=.1266E+00, TotOvfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
004:0056-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                04:B1d                4.30    .227 No_date    6:12    61.44  n/a
                                + 08:OVR                .00    .000 No_date    0:00    .00    n/a
                                + 01:B1dPND            4.30    .227 No_date    6:12    61.44  n/a
[DT= 3.00] SUM=
004:0057-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD          02:B1f                3.50    .762 No_date    6:00    55.45  .647
  [CN= 87.4: N= 3.00]
  [Tp= .11:DT= 3.00]
004:0058-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE RESERVOIR -> 02:B1f                3.50    .762 No_date    6:00    55.45  n/a
  [RDT= 3.00] out<- 04:B1f                3.50    .144 No_date    6:21    55.45  n/a
  overflow <= 08:OVR                .00    .000 No_date    0:00    .00    n/a
  {MxStoUsed=.9434E-01, TotOvfVol=.0000E+00, N-ovf= 0, TotDurOvf= 0.hrs}
004:0059-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD                04:B1f                3.50    .144 No_date    6:21    55.45  n/a
                                + 08:OVR                .00    .000 No_date    0:00    .00    n/a
                                + 02:B1fPND            3.50    .144 No_date    6:21    55.45  n/a
[DT= 3.00] SUM=
004:0060-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

```

```

* CALIB STANDHYD      07:B1e      SWM.sum      3.60      .958 No_date      6:00      61.94 .723
  [XIMP=.27:TIMP=.27]
  [LOSS= 2 :CN= 86.0]
  [Pervious area: IAper= 5.00:SLPP=1.15:LGP= 30.:MNP=.035:SCP= .0]
  [Impervious area: IAimp= .50:SLPI=1.15:LGI= 50.:MNI=.013:SCI= .0]
004:0061-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 07:B1e      3.60      .958 No_date      6:00      61.94 n/a
  [RDT= 3.00] out<- 06:B1e      3.60      .176 No_date      6:12      61.94 n/a
    overflow <= 08:OVR      .00      .000 No_date      0:00      .00 n/a
  {MxStoUsed=.1140E+00, TotovfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
004:0062-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      06:B1e      3.60      .176 No_date      6:12      61.94 n/a
    + 08:OVR      .00      .000 No_date      0:00      .00 n/a
  [DT= 3.00] SUM= 07:B1ePND      3.60      .176 No_date      6:12      61.94 n/a
004:0063-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      01:B1dPND      4.30      .227 No_date      6:12      61.44 n/a
    + 02:B1west      3.50      .144 No_date      6:21      55.45 n/a
    + 07:B1ePND      3.60      .176 No_date      6:12      61.94 n/a
  [DT= 3.00] SUM= 02:B1west      11.40      .544 No_date      6:15      59.76 n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
*****
004:0064-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      02:B1west      11.40      .544 No_date      6:15      59.76 n/a
    + 03:B1East      24.00      2.306 No_date      6:09      53.82 n/a
  [DT= 3.00] SUM= 04:SMT4      35.40      2.843 No_date      6:09      55.73 n/a
*****
# DRAINAGE FROM 201C (EXTERNAL)
*****
004:0065-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:201C      91.00      7.875 No_date      6:24      53.37 .623
  [CN= 86.0: N= 3.00]
  [Tp= .50:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
*****
004:0066-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:C1a      7.00      1.064 No_date      6:06      53.36 .623
  [CN= 86.0: N= 3.00]
  [Tp= .21:DT= 6.00]
*****
# C1a SWM FACILITY
*****
004:0067-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:C1a      7.00      1.064 No_date      6:06      53.36 n/a
  [RDT= 6.00] out<- 06:C1a      7.00      .317 No_date      6:30      53.36 n/a
    overflow <= 08:OVR      .00      .000 No_date      0:00      .00 n/a
  {MxStoUsed=.1580E+00, TotovfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
*****
# DISCHARGE FROM C1a SWM FACILITY
*****
004:0068-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      06:C1a      7.00      .317 No_date      6:30      53.36 n/a
    + 08:OVR      .00      .000 No_date      0:00      .00 n/a
  [DT= 6.00] SUM= 02:C1aPND      7.00      .317 No_date      6:30      53.36 n/a
004:0069-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:C1b      .50      .129 No_date      6:00      54.18 .632
  [CN= 86.5: N= 3.00]
  [Tp= .04:DT= 2.00]
*****
# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
*****
004:0070-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD      01:201C      91.00      7.875 No_date      6:24      53.37 n/a
    + 02:EX+MC      7.00      .317 No_date      6:30      53.36 n/a

```



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                                SWM.sum
                                + 03:c1b          .50      .129 No_date  6:00  54.18  n/a
                                [DT= 2.00] SUM= 02:EX+MC 98.50   8.203 No_date  6:24  53.37  n/a
*****
# Route NHYD=201C through channel SMT-1
*****
004:0071-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 02:EX+MC  98.50   8.203 No_date  6:24  53.37  n/a
*   [RDT= 2.00] out<- 01:SMT-1  98.50   8.023 No_date  6:28  53.37  n/a
    [L/s/n= 275./ .500/.030]
    {Vmax= .962:Dmax= .719}
004:0072-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   07:C2      3.80    .656 No_date  6:03  53.58  .625
    [CN= 86.1: N= 3.00]
    [Tp= .17:DT= 3.00]
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS
# EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2
*****
004:0073-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD        01:SMT1    98.50   8.023 No_date  6:28  53.37  n/a
              + 07:C2      3.80    .656 No_date  6:03  53.58  n/a
    [DT= 2.00] SUM= 01:SMT1 102.30   8.217 No_date  6:26  53.38  n/a
*****
# CONFLUENCE SMT 1-4
*****
004:0074-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD        04:SMT4    35.40   2.843 No_date  6:09  55.73  n/a
              + 01:SMT1   102.30   8.217 No_date  6:26  53.38  n/a
    [DT= 2.00] SUM= 02:SMT1-4 137.70  10.672 No_date  6:24  53.98  n/a
*****
# DRAINAGE FROM 201D (EXTERNAL)
*****
004:0075-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   02:201D   28.90   2.879 No_date  6:18  53.37  .623
    [CN= 86.0: N= 3.00]
    [Tp= .41:DT= 6.00]
*****
# SUBCATCHMENT 201D ROUTED
# THROUGH Channel SMT-3
*****
004:0076-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 02:201D   28.90   2.879 No_date  6:18  53.37  n/a
    [RDT= 6.00] out<- 03:SMT-3R  28.90   2.890 No_date  6:18  53.37  n/a
    [L/s/n= 100./ .700/.030]
    {Vmax= 1.374:Dmax= .911}
*****
# DRAINAGE FROM CEMETERY LANDS D1a, D1b
*****
004:0077-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   02:D1a     1.90    .386 No_date  6:00  56.45  .659
    [CN= 88.0: N= 3.00]
    [Tp= .13:DT= 3.00]
004:0078-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD   07:D1b     1.90    .431 No_date  6:00  53.36  .623
    [CN= 86.0: N= 3.00]
    [Tp= .09:DT= 3.00]
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b
*****
004:0079-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD        02:D1a     1.90    .386 No_date  6:00  56.45  n/a
              + 03:SMT-3R  28.90   2.890 No_date  6:18  53.37  n/a
              + 07:D1b     1.90    .431 No_date  6:00  53.36  n/a
    [DT= 3.00] SUM= 06:SMT3   32.70   3.153 No_date  6:12  53.55  n/a
*****

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SWM.sum

CONFLUENCE SMT 1-3

004:0080-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT1 102.30 8.217 No_date 6:26 53.38 n/a
+ 04:SMT4 35.40 2.843 No_date 6:09 55.73 n/a
+ 06:SMT3 32.70 3.153 No_date 6:12 53.55 n/a
[DT= 2.00] SUM= 03:SMT1-3 170.40 13.656 No_date 6:20 53.90 n/a

TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D

004:0081-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT1 102.30 8.217 No_date 6:26 53.38 n/a
+ 04:SMT4 35.40 2.843 No_date 6:09 55.73 n/a
+ 06:SMT3 32.70 3.153 No_date 6:12 53.55 n/a
+ 05:SMT2 83.60 6.583 No_date 6:24 53.65 n/a
[DT= 2.00] SUM= 08:1201 254.00 20.162 No_date 6:24 53.82 n/a
004:0082-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 08:1201 254.00 20.162 No_date 6:24 53.82 n/a
* [RDT= 2.00] out<- 03:002202 254.00 19.614 No_date 6:28 53.82 n/a
[L/s/n= 475./1.050/.030]
{Vmax= 1.089:Dmax= .643}
004:0083-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 04:000202 21.60 2.748 No_date 6:12 56.83 .663
[CN= 86.8: N= 3.00]
[Tp= .30:DT= 6.00]
004:0084-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:002202 254.00 19.614 No_date 6:28 53.82 n/a
+ 04:000202 21.60 2.748 No_date 6:12 56.83 n/a
[DT= 2.00] SUM= 02:001202 275.60 21.497 No_date 6:26 54.05 n/a
004:0085-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 03:000203 26.30 3.924 No_date 6:06 56.83 .663
[CN= 86.8: N= 3.00]
[Tp= .24:DT= 6.00]
004:0086-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000203 26.30 3.924 No_date 6:06 56.83 n/a
+ 02:001202 275.60 21.497 No_date 6:26 54.05 n/a
[DT= 2.00] SUM= 04:000003 301.90 23.708 No_date 6:22 54.29 n/a
004:0087-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD 04:000003 301.90 23.708 No_date 6:22 54.29 n/a

SUBCATCHMENT 204 AREA REVISED
NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha

004:0088-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 02:000204 53.60 4.144 No_date 6:30 55.83 .651
[CN= 87.6: N= 3.00]
[Tp= .63:DT= 6.00]
004:0089-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 02:000204 53.60 4.144 No_date 6:30 55.83 n/a
+ 04:000003 301.90 23.708 No_date 6:22 54.29 n/a
[DT= 2.00] SUM= 03:001204 355.50 27.701 No_date 6:24 54.53 n/a

ROUTE through channel 205 ELIMINATED, OUTSIDE OF STUDY AREA

SUBCATCHMENT 205 ELIMINATED, OUTSIDE OF STUDY AREA

ID REVISED TO ID=9, PREVIOUSLY ID=1

004:0090-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 09:001108 784.37 29.062 No_date 6:24 60.20 n/a
+ 03:001204 355.50 27.701 No_date 6:24 54.53 n/a
[DT= 2.00] SUM= 02:000008 1139.87 56.763 No_date 6:24 58.43 n/a
004:0091-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

SWM.sum

PRINT HYD 02:000008 1139.87 56.763 No_date 6:24 58.43 n/a

** END OF RUN : 4

RUN:COMMAND#

005:0001-----

START

[TZERO = .00 hrs on 0]

[METOUT= 2 (1=imperial, 2=metric output)]

[NSTORM= 1]

[NRUN = 5]

Project Name: [Holy Family Catholic Cemetery] Project Number: [111063]

Date : 08-16-2011

Modeller : [C. Silvestri]

Company : Philips Engineering Ltd

License # : 3569108

005:0002-----

READ STORM

Filename = STORM.001

Comment = TOWN OF MILTON 12 HOUR 50 YEAR SCS STORM (1998 IDF DATA)

[SDT=12.00:SDUR= 12.00:PTOT= 96.33]

005:0003-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

CALIB NASHYD 01:000103 42.10 5.123 No_date 6:18 65.13 .676

[CN= 86.0: N= 3.00]

[Tp= .40:DT= 6.00]

005:0004-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

ROUTE CHANNEL -> 01:000103 42.10 5.123 No_date 6:18 65.13 n/a

[RDT= 6.00] out<- 02:002104 42.10 4.792 No_date 6:24 65.13 n/a

[L/S/n= 440./1.000/.030]

{Vmax= .770:Dmax= .596}

005:0005-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

CALIB NASHYD 03:000104 24.10 4.395 No_date 6:06 65.13 .676

[CN= 86.0: N= 3.00]

[Tp= .21:DT= 6.00]

005:0006-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

ADD HYD 03:000104 24.10 4.395 No_date 6:06 65.13 n/a

+ 02:002104 42.10 4.792 No_date 6:24 65.13 n/a

[DT= 6.00] SUM= 01:001104 66.20 7.676 No_date 6:12 65.13 n/a

005:0007-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

ROUTE CHANNEL -> 01:001104 66.20 7.676 No_date 6:12 65.13 n/a

[RDT= 6.00] out<- 02:002105 66.20 7.046 No_date 6:18 65.13 n/a

[L/S/n= 365./ .400/.030]

{Vmax= .565:Dmax= .583}

005:0008-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

* CALIB NASHYD 03:000105 19.20 3.938 No_date 6:00 66.47 .690

[CN= 86.8: N= 3.00]

[Tp= .18:DT= 6.00]

005:0009-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

ADD HYD 03:000105 19.20 3.938 No_date 6:00 66.47 n/a

+ 02:002105 66.20 7.046 No_date 6:18 65.13 n/a

[DT= 6.00] SUM= 01:001105 85.40 9.318 No_date 6:12 65.43 n/a

005:0010-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

ROUTE CHANNEL -> 01:001105 85.40 9.318 No_date 6:12 65.43 n/a

[RDT= 6.00] out<- 02:002106 85.40 8.847 No_date 6:18 65.43 n/a

[L/S/n= 385./ .670/.030]

{Vmax= .784:Dmax= .620}

005:0011-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

		SWM.sum					
* CALIB NASHYD	03:000106	15.30	3.279	No_date	6:00	67.15	.697
[CN= 87.2: N= 3.00]							
[Tp= .17:DT= 6.00]							
005:0012	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
ADD HYD	03:000106	15.30	3.279	No_date	6:00	67.15	n/a
	+ 02:002106	85.40	8.847	No_date	6:18	65.43	n/a
[DT= 6.00]	SUM= 01:001106	100.70	10.545	No_date	6:12	65.69	n/a
005:0013	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.	R.C.
* CALIB STANDHYD	03:000107	15.27	.957	No_date	6:54	72.64	.754
[XIMP=.10:TIMP=.17]							
[LOSS= 2 :CN= 88.0]							
[Pervious area: IAper= 2.50:SLPP=1.27:LGP= 717.:MNP=.250:SCP= .0]							
[Impervious area: IAimp= 1.57:SLPI=1.27:LGI= 100.:MNI=.017:SCI= .0]							
005:0014	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
ADD HYD	01:001106	100.70	10.545	No_date	6:12	65.69	n/a
	+ 03:000107	15.27	.957	No_date	6:54	72.64	n/a
[DT= 6.00]	SUM= 02:001107	115.97	11.089	No_date	6:12	66.60	n/a
005:0015	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
ROUTE CHANNEL	-> 02:001107	115.97	11.089	No_date	6:12	66.60	n/a
[RDT= 6.00]	out<- 01:002108	115.97	10.128	No_date	6:24	66.60	n/a
[L/s/n= 1300./1.670/.030]							
{Vmax= 1.852:Dmax= .977}							
005:0016	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
CALIB NASHYD	02:000108	33.50	5.055	No_date	6:06	66.47	.690
[CN= 86.8: N= 3.00]							
[Tp= .29:DT= 6.00]							
005:0017	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
ADD HYD	01:002108	115.97	10.128	No_date	6:24	66.60	n/a
	+ 02:000108	33.50	5.055	No_date	6:06	66.47	n/a
[DT= 6.00]	SUM= 03:000004	149.47	14.265	No_date	6:18	66.57	n/a
005:0018	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
PRINT HYD	03:000004	149.47	14.265	No_date	6:18	66.57	n/a
005:0019	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
CALIB STANDHYD	04:000101	287.80	12.760	No_date	6:24	74.47	.773
[XIMP=.20:TIMP=.50]							
[LOSS= 2 :CN= 83.4]							
[Pervious area: IAper= 5.00:SLPP= .63:LGP= 700.:MNP=.250:SCP= .0]							
[Impervious area: IAimp= 1.57:SLPI= .63:LGI=3200.:MNI=.017:SCI= .0]							
005:0020	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
ROUTE CHANNEL	-> 04:000101	287.80	12.760	No_date	6:24	74.47	n/a
[RDT= 6.00]	out<- 05:002101	287.80	12.373	No_date	7:42	74.47	n/a
[L/s/n= 700./ .420/.030]							
{Vmax= .759:Dmax= .765}							
005:0021	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
* CALIB STANDHYD	04:000102	272.90	14.347	No_date	6:00	68.10	.707
[XIMP=.13:TIMP=.28]							
[LOSS= 2 :CN= 84.0]							
[Pervious area: IAper= 5.00:SLPP= .98:LGP=1350.:MNP=.250:SCP= .0]							
[Impervious area: IAimp= 1.57:SLPI= .98:LGI= 40.:MNI=.017:SCI= .0]							
005:0022	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
ADD HYD	04:000102	272.90	14.347	No_date	6:00	68.10	n/a
	+ 05:002101	287.80	12.373	No_date	7:42	74.47	n/a
[DT= 6.00]	SUM= 06:000001	560.70	21.656	No_date	7:48	71.37	n/a
005:0023	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
PRINT HYD	06:000001	560.70	21.656	No_date	7:48	71.37	n/a
005:0024	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
ROUTE CHANNEL	-> 06:000001	560.70	21.656	No_date	7:48	71.37	n/a
[RDT= 6.00]	out<- 04:002109	560.70	21.245	No_date	8:00	71.37	n/a
[L/s/n= 1000./ .540/.030]							
{Vmax= 1.118:Dmax= 1.106}							
005:0025	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-
CALIB NASHYD	05:000109	35.10	5.094	No_date	6:12	66.47	.690
[CN= 86.8: N= 3.00]							
[Tp= .32:DT= 6.00]							
005:0026	-----ID:NHYD-----	AREA----	QPEAK-	TpeakDate_	hh:mm----	R.V.-	R.C.-

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                                SWM.Sum
ADD HYD                04:002109  560.70  21.245 No_date  8:00  71.37 n/a
                        + 05:000109  35.10   5.094 No_date  6:12  66.47 n/a
[DT= 6.00] SUM= 06:001109  595.80  21.750 No_date  8:00  71.08 n/a
005:0027-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 06:001109  595.80  21.750 No_date  8:00  71.08 n/a
[RDT= 6.00] out<- 04:002110  595.80  21.511 No_date  8:06  71.08 n/a
[L/S/n= 900./ .710/.030]
{Vmax= 1.027:Dmax= .906}
005:0028-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD        05:000110  21.80   4.044 No_date  6:06  67.15 .697
[CN= 87.2: N= 3.00]
[Tp= .22:DT= 6.00]
005:0029-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                04:002110  595.80  21.511 No_date  8:06  71.08 n/a
                        + 05:000110  21.80   4.044 No_date  6:06  67.15 n/a
[DT= 6.00] SUM= 06:001110  617.60  21.806 No_date  8:06  70.94 n/a
005:0030-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 06:001110  617.60  21.806 No_date  8:06  70.94 n/a
[RDT= 6.00] out<- 04:002111  617.60  21.776 No_date  8:06  70.94 n/a
[L/S/n= 920./1.250/.030]
{Vmax= 2.102:Dmax= .990}
005:0031-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD        01:000111  17.30   3.018 No_date  6:06  65.79 .683
[CN= 86.4: N= 3.00]
[Tp= .23:DT= 6.00]
005:0032-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                01:000111  17.30   3.018 No_date  6:06  65.79 n/a
                        + 04:002111  617.60  21.776 No_date  8:06  70.94 n/a
[DT= 6.00] SUM= 02:000002  634.90  22.010 No_date  8:06  70.80 n/a
005:0033-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD            02:000002  634.90  22.010 No_date  8:06  70.80 n/a
*****
# ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN
005:0034-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                03:000004  149.47  14.265 No_date  6:18  66.57 n/a
                        + 02:000002  634.90  22.010 No_date  8:06  70.80 n/a
[DT= 6.00] SUM= 09:001108  784.37  32.959 No_date  6:18  70.00 n/a
*****
# SUBCATCHMENT CONTAINING CEMETERY LANDS
*****
# PROPOSED IMPERVIOUSNESS LESS THAN 20%
# THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURF
#
*****
# DRAINAGE FROM 201A (EXTERNAL)
*****
005:0035-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD        01:201A   68.20   7.276 No_date  6:18  62.87 .653
[CN= 86.0: N= 3.00]
[Tp= .47:DT= 6.00]
#Route NHYD=201A through Channel SMT-2
005:0036-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:201A   68.20   7.276 No_date  6:18  62.87 n/a
[RDT= 6.00] out<- 02:SMT-2R  68.20   6.982 No_date  6:24  62.87 n/a
[L/S/n= 450./ .750/.030]
{Vmax= 1.194:Dmax= .658}
*****
# DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d
*****
005:0037-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD        01:A1a    .80    .130 No_date  6:06  65.68 .682
[CN= 87.7: N= 3.00]
[Tp= .27:DT= 6.00]
005:0038-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

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* CALIB NASHYD 03:A1b SWM.sum 6.10 1.727 No_date 6:00 63.08 .655
  [CN= 86.1: N= 3.00]
  [Tp= .07:DT= 3.00]
005:0039-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 04:A1c 3.20 .727 No_date 6:03 64.92 .674
  [CN= 87.2: N= 3.00]
  [Tp= .14:DT= 3.00]
005:0040-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 06:A1d 5.30 .978 No_date 6:06 65.04 .675
  [CN= 87.3: N= 3.00]
  [Tp= .21:DT= 6.00]
005:0041-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 06:A1d 5.30 .978 No_date 6:06 65.04 n/a
  [RDT= 6.00] out<- 07:A1d 5.30 .268 No_date 6:36 65.04 n/a
    overflow <= 08:OVR .00 .000 No_date 0:00 .00 n/a
  {MxStoUsed=.1580E+00, TotOvfVo]=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
005:0042-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 07:A1d 5.30 .268 No_date 6:36 65.04 n/a
  + 08:OVR .00 .000 No_date 0:00 .00 n/a
  [DT= 6.00] SUM= 06:A1dPND 5.30 .268 No_date 6:36 65.04 n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d
*****
005:0043-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:A1a .80 .130 No_date 6:06 65.68 n/a
  + 02:SMT-2R 68.20 6.982 No_date 6:24 62.87 n/a
  + 03:A1b 6.10 1.727 No_date 6:00 63.08 n/a
  + 04:A1c 3.20 .727 No_date 6:03 64.92 n/a
  + 06:A1dPND 5.30 .268 No_date 6:36 65.04 n/a
  [DT= 3.00] SUM= 05:SMT2 83.60 7.714 No_date 6:24 63.20 n/a
*****
# DRAINAGE FROM 201B (EXTERNAL)
*****
005:0044-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 01:201B 13.40 1.891 No_date 6:12 62.87 .653
  [CN= 86.0: N= 3.00]
  [Tp= .31:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)
*****
005:0045-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 02:B1a 4.60 .954 No_date 6:03 64.55 .670
  [CN= 87.0: N= 3.00]
  [Tp= .17:DT= 3.00]
005:0046-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1a 4.60 .954 No_date 6:03 64.55 n/a
  [RDT= 3.00] out<- 04:B1a 4.60 .289 No_date 6:27 64.55 n/a
    overflow <= 08:OVR .00 .000 No_date 0:00 .00 n/a
  {MxStoUsed=.1235E+00, TotOvfVo]=.0000E+00, N-Ovf= 0, TotDurOvf= 0.hrs}
005:0047-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 04:B1a 4.60 .289 No_date 6:27 64.55 n/a
  + 08:OVR .00 .000 No_date 0:00 .00 n/a
  [DT= 3.00] SUM= 02:B1aPND 4.60 .289 No_date 6:27 64.55 n/a
005:0048-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:201B 13.40 1.891 No_date 6:12 62.87 n/a
  + 02:B1aPND 4.60 .289 No_date 6:27 64.55 n/a
  [DT= 3.00] SUM= 03:201B 18.00 2.160 No_date 6:12 63.30 n/a
*****
# Route NHYD=201B + B1a through Channel SMT-4
*****
005:0049-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 03:201B 18.00 2.160 No_date 6:12 63.30 n/a
* [RDT= 3.00] out<- 01:SMT-4R 18.00 1.969 No_date 6:18 63.30 n/a
  [L/s/n= 600./ .850/.030]
  {Vmax= 1.113:Dmax= .439}

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SWM.sum
005:0050-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      03:B1b      5.00    1.014 No_date    6:03    63.09 .655
  [CN= 86.1: N= 3.00]
  [Tp= .17:DT= 3.00]
005:0051-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      04:B1c      1.00    .267 No_date    6:00    65.72 .682
  [CN= 87.7: N= 3.00]
  [Tp= .10:DT= 3.00]
005:0052-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           03:B1b      5.00    1.014 No_date    6:03    63.09 n/a
  + 04:B1c      1.00    .267 No_date    6:00    65.72 n/a
  [DT= 3.00] SUM= 02:B1b/c    6.00    1.253 No_date    6:03    63.53 n/a
#*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c
#*****
005:0053-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:SMT-4R    18.00   1.969 No_date    6:18    63.30 n/a
  + 02:B1b/c    6.00    1.253 No_date    6:03    63.53 n/a
  [DT= 3.00] SUM= 03:B1East   24.00   2.731 No_date    6:09    63.35 n/a
#*****
# DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)
#*****
005:0054-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD  01:B1d      4.30    1.310 No_date    6:00    71.22 .739
  [XIMP=.25:TIMP=.25]
  [LOSS= 2 :CN= 86.0]
  [Pervious area: IAper= 5.00:SLPP= .85:LGP= 30.:MNP=.035:SCP= .0]
  [Impervious area: IAimp= .50:SLPI= .85:LGI= 50.:MNI=.013:SCI= .0]
005:0055-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 01:B1d      4.30    1.310 No_date    6:00    71.22 n/a
  [RDT= 3.00] out<- 04:B1d      4.30    .249 No_date    6:12    71.22 n/a
  overflow <= 08:OVR    .00    .000 No_date    0:00    .00 n/a
  {MxStoUsed=.1484E+00, TotovfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
005:0056-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           04:B1d      4.30    .249 No_date    6:12    71.22 n/a
  + 08:OVR    .00    .000 No_date    0:00    .00 n/a
  [DT= 3.00] SUM= 01:B1dPND   4.30    .249 No_date    6:12    71.22 n/a
005:0057-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:B1f      3.50    .889 No_date    6:00    65.12 .676
  [CN= 87.4: N= 3.00]
  [Tp= .11:DT= 3.00]
005:0058-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1f      3.50    .889 No_date    6:00    65.12 n/a
  [RDT= 3.00] out<- 04:B1f      3.50    .159 No_date    6:24    65.12 n/a
  overflow <= 08:OVR    .00    .000 No_date    0:00    .00 n/a
  {MxStoUsed=.1126E+00, TotovfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
005:0059-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           04:B1f      3.50    .159 No_date    6:24    65.12 n/a
  + 08:OVR    .00    .000 No_date    0:00    .00 n/a
  [DT= 3.00] SUM= 02:B1fPND   3.50    .159 No_date    6:24    65.12 n/a
005:0060-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD  07:B1e      3.60    1.108 No_date    6:00    71.75 .745
  [XIMP=.27:TIMP=.27]
  [LOSS= 2 :CN= 86.0]
  [Pervious area: IAper= 5.00:SLPP=1.15:LGP= 30.:MNP=.035:SCP= .0]
  [Impervious area: IAimp= .50:SLPI=1.15:LGI= 50.:MNI=.013:SCI= .0]
005:0061-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 07:B1e      3.60    1.108 No_date    6:00    71.75 n/a
  [RDT= 3.00] out<- 06:B1e      3.60    .197 No_date    6:12    71.75 n/a
  overflow <= 08:OVR    .00    .000 No_date    0:00    .00 n/a
  {MxStoUsed=.1328E+00, TotovfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
005:0062-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           06:B1e      3.60    .197 No_date    6:12    71.75 n/a
  + 08:OVR    .00    .000 No_date    0:00    .00 n/a
  [DT= 3.00] SUM= 07:B1ePND   3.60    .197 No_date    6:12    71.75 n/a

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                                SWM.sum
005:0063-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          01:B1dPND      4.30      .249 No_date   6:12   71.22  n/a
                   + 02:B1west    3.50      .159 No_date   6:24   65.12  n/a
                   + 07:B1ePND    3.60      .197 No_date   6:12   71.75  n/a
    [DT= 3.00] SUM= 02:B1west    11.40     .604 No_date   6:15   69.51  n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
*****
005:0064-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          02:B1west    11.40     .604 No_date   6:15   69.51  n/a
                   + 03:B1East    24.00     2.731 No_date   6:09   63.35  n/a
    [DT= 3.00] SUM= 04:SMT4     35.40     3.326 No_date   6:09   65.34  n/a
*****
# DRAINAGE FROM 201C (EXTERNAL)
*****
005:0065-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD    01:201C      91.00     9.278 No_date   6:24   62.87  .653
    [CN= 86.0: N= 3.00]
    [Tp= .50:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
*****
005:0066-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD    02:C1a        7.00      1.249 No_date   6:06   62.87  .653
    [CN= 86.0: N= 3.00]
    [Tp= .21:DT= 6.00]
*****
# C1a SWM FACILITY
*****
005:0067-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE RESERVOIR -> 02:C1a      7.00      1.249 No_date   6:06   62.87  n/a
    [RDT= 6.00] out<- 06:C1a      6.55      .325 No_date   6:18   62.87  n/a
      overflow <= 08:OVR          .45      .593 No_date   6:18   62.87  n/a
    {MxStoUsed=.1641E+00, TotOvfVo]=.2836E-01, N-Ovf= 2, TotDurOvf= 0.hrs}
*****
# DISCHARGE FROM C1a SWM FACILITY
*****
005:0068-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          06:C1a        6.55      .325 No_date   6:18   62.87  n/a
                   + 08:OVR          .45      .593 No_date   6:18   62.87  n/a
    [DT= 6.00] SUM= 02:C1aPND     7.00      .918 No_date   6:18   62.87  n/a
005:0069-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  * CALIB NASHYD    03:C1b        .50      .150 No_date   6:00   63.75  .662
    [CN= 86.5: N= 3.00]
    [Tp= .04:DT= 2.00]
*****
# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
*****
005:0070-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          01:201C      91.00     9.278 No_date   6:24   62.87  n/a
                   + 02:EX+MC      7.00      .918 No_date   6:18   62.87  n/a
                   + 03:C1b        .50      .150 No_date   6:00   63.75  n/a
    [DT= 2.00] SUM= 02:EX+MC     98.50    10.147 No_date   6:18   62.87  n/a
*****
# Route NHYD=201C through channel SMT-1
*****
005:0071-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ROUTE CHANNEL   -> 02:EX+MC     98.50    10.147 No_date   6:18   62.87  n/a
  * [RDT= 2.00] out<- 01:SMT-1    98.50     9.589 No_date   6:24   62.87  n/a
    [L/s/n= 275./ .500/.030]
    {Vmax= .962:Dmax= .760}
005:0072-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  CALIB NASHYD    07:C2         3.80      .770 No_date   6:03   63.09  .655
    [CN= 86.1: N= 3.00]
    [Tp= .17:DT= 3.00]

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SWM.sum

TOTAL DRAINAGE FROM SUBCATCHMENTS
EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2

005:0073-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT1 98.50 9.589 No_date 6:24 62.87 n/a
+ 07:C2 3.80 .770 No_date 6:03 63.09 n/a
[DT= 2.00] SUM= 01:SMT1 102.30 9.852 No_date 6:24 62.88 n/a

CONFLUENCE SMT 1-4

005:0074-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 04:SMT4 35.40 3.326 No_date 6:09 65.34 n/a
+ 01:SMT1 102.30 9.852 No_date 6:24 62.88 n/a
[DT= 2.00] SUM= 02:SMT1-4 137.70 12.820 No_date 6:22 63.51 n/a

DRAINAGE FROM 201D (EXTERNAL)

005:0075-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 02:201D 28.90 3.390 No_date 6:18 62.87 .653
[CN= 86.0: N= 3.00]
[Tp= .41:DT= 6.00]

SUBCATCHMENT 201D ROUTED
THROUGH Channel SMT-3

005:0076-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 02:201D 28.90 3.390 No_date 6:18 62.87 n/a
[RDT= 6.00] out<- 03:SMT-3R 28.90 3.403 No_date 6:18 62.87 n/a
[L/s/n= 100./ .700/.030]
{Vmax= 1.429:Dmax= .967}

DRAINAGE FROM CEMETERY LANDS D1a, D1b

005:0077-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 02:D1a 1.90 .450 No_date 6:00 66.20 .687
[CN= 88.0: N= 3.00]
[Tp= .13:DT= 3.00]

005:0078-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD 07:D1b 1.90 .504 No_date 6:00 62.87 .653
[CN= 86.0: N= 3.00]
[Tp= .09:DT= 3.00]

TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b

005:0079-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 02:D1a 1.90 .450 No_date 6:00 66.20 n/a
+ 03:SMT-3R 28.90 3.403 No_date 6:18 62.87 n/a
+ 07:D1b 1.90 .504 No_date 6:00 62.87 n/a
[DT= 3.00] SUM= 06:SMT3 32.70 3.716 No_date 6:12 63.06 n/a

CONFLUENCE SMT 1-3

005:0080-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT1 102.30 9.852 No_date 6:24 62.88 n/a
+ 04:SMT4 35.40 3.326 No_date 6:09 65.34 n/a
+ 06:SMT3 32.70 3.716 No_date 6:12 63.06 n/a
[DT= 2.00] SUM= 03:SMT1-3 170.40 16.370 No_date 6:20 63.42 n/a

TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D

005:0081-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT1 102.30 9.852 No_date 6:24 62.88 n/a
+ 04:SMT4 35.40 3.326 No_date 6:09 65.34 n/a
+ 06:SMT3 32.70 3.716 No_date 6:12 63.06 n/a

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                                SWM.sum
                                + 05:SMT2      83.60   7.714 No_date   6:24   63.20  n/a
                                [DT= 2.00] SUM= 08:1201 254.00 23.922 No_date   6:22   63.35  n/a
005:0082-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 08:1201 254.00 23.922 No_date   6:22   63.35  n/a
* [RDT= 2.00] out<- 03:002202 254.00 23.248 No_date   6:28   63.35  n/a
  [L/s/n= 475./1.050/.030]
  {Vmax= 1.134:Dmax= .672}
005:0083-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      04:000202 21.60 3.208 No_date   6:12   66.47 .690
  [CN= 86.8: N= 3.00]
  [Tp= .30:DT= 6.00]
005:0084-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           03:002202 254.00 23.248 No_date   6:28   63.35  n/a
                                + 04:000202 21.60 3.208 No_date   6:12   66.47  n/a
                                [DT= 2.00] SUM= 02:001202 275.60 25.525 No_date   6:24   63.59  n/a
005:0085-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      03:000203 26.30 4.582 No_date   6:06   66.47 .690
  [CN= 86.8: N= 3.00]
  [Tp= .24:DT= 6.00]
005:0086-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           03:000203 26.30 4.582 No_date   6:06   66.47  n/a
                                + 02:001202 275.60 25.525 No_date   6:24   63.59  n/a
                                [DT= 2.00] SUM= 04:000003 301.90 28.161 No_date   6:22   63.84  n/a
005:0087-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD         04:000003 301.90 28.161 No_date   6:22   63.84  n/a
#*****
# SUBCATCHMENT 204 AREA REVISED
# NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha
#*****
005:0088-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:000204 53.60 4.865 No_date   6:30   65.53 .680
  [CN= 87.6: N= 3.00]
  [Tp= .63:DT= 6.00]
005:0089-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           02:000204 53.60 4.865 No_date   6:30   65.53  n/a
                                + 04:000003 301.90 28.161 No_date   6:22   63.84  n/a
                                [DT= 2.00] SUM= 03:001204 355.50 32.849 No_date   6:22   64.10  n/a
#*****
# ROUTE through channel 205 ELIMINATED, OUTSIDE OF STUDY AREA
#*****
# SUBCATCHMENT 205 ELIMINTATED, OUTSIDE OF STUDY AREA
#*****
# ID REVISED TO ID=9, PREVIOUSLY ID=1
#*****
005:0090-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           09:001108 784.37 32.959 No_date   6:18   70.00  n/a
                                + 03:001204 355.50 32.849 No_date   6:22   64.10  n/a
                                [DT= 2.00] SUM= 02:000008 1139.87 65.757 No_date   6:22   68.16  n/a
005:0091-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD         02:000008 1139.87 65.757 No_date   6:22   68.16  n/a
#*****
** END OF RUN : 5
#*****

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RUN:COMMAND#
006:0001-----
START
[TZERO = .00 hrs on 0]

```

[METOUT= 2 (1=imperial, 2=metric output)]
[NSTORM= 1]
[NRUN = 6]

Project Name: [Holy Family Catholic Cemetery] Project Number: [111063]
Date : 08-16-2011
Modeller : [C. Silvestri]
Company : Philips Engineering Ltd
License # : 3569108

006:0002-----
READ STORM
Filename = STORM.001
Comment = TOWN OF MILTON 12 HOUR 100 YEAR SCS STORM (1998 IDF DATA)
[SDT=12.00:SDUR= 12.00:PTOT= 106.96]
006:0003-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 01:000103 42.10 5.881 No_date 6:18 74.84 .700
[CN= 86.0: N= 3.00]
[Tp= .40:DT= 6.00]
006:0004-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:000103 42.10 5.881 No_date 6:18 74.84 n/a
[RDT= 6.00] out<- 02:002104 42.10 5.531 No_date 6:24 74.84 n/a
[L/S/n= 440./1.000/.030]
{Vmax= .795:Dmax= .614}
006:0005-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 03:000104 24.10 5.036 No_date 6:06 74.84 .700
[CN= 86.0: N= 3.00]
[Tp= .21:DT= 6.00]
006:0006-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000104 24.10 5.036 No_date 6:06 74.84 n/a
+ 02:002104 42.10 5.531 No_date 6:24 74.84 n/a
[DT= 6.00] SUM= 01:001104 66.20 8.873 No_date 6:12 74.84 n/a
006:0007-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:001104 66.20 8.873 No_date 6:12 74.84 n/a
[RDT= 6.00] out<- 02:002105 66.20 8.238 No_date 6:18 74.84 n/a
[L/S/n= 365./ .400/.030]
{Vmax= .595:Dmax= .604}
006:0008-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD 03:000105 19.20 4.511 No_date 6:00 76.26 .713
[CN= 86.8: N= 3.00]
[Tp= .18:DT= 6.00]
006:0009-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000105 19.20 4.511 No_date 6:00 76.26 n/a
+ 02:002105 66.20 8.238 No_date 6:18 74.84 n/a
[DT= 6.00] SUM= 01:001105 85.40 10.898 No_date 6:12 75.16 n/a
006:0010-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:001105 85.40 10.898 No_date 6:12 75.16 n/a
[RDT= 6.00] out<- 02:002106 85.40 10.393 No_date 6:18 75.16 n/a
[L/S/n= 385./ .670/.030]
{Vmax= .821:Dmax= .648}
006:0011-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD 03:000106 15.30 3.750 No_date 6:00 76.98 .720
[CN= 87.2: N= 3.00]
[Tp= .17:DT= 6.00]
006:0012-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000106 15.30 3.750 No_date 6:00 76.98 n/a
+ 02:002106 85.40 10.393 No_date 6:18 75.16 n/a
[DT= 6.00] SUM= 01:001106 100.70 12.397 No_date 6:12 75.43 n/a
006:0013-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 03:000107 15.27 1.172 No_date 6:48 82.70 .773
[XIMP=.10:TIMP=.17]
[LOSS= 2 :CN= 88.0]
[Pervious area: IAper= 2.50:SLPP=1.27:LGP= 717.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI=1.27:LGI= 100.:MNI=.017:SCI= .0]
006:0014-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

		SWM.sum						
ADD HYD	01:001106	100.70	12.397	No_date	6:12	75.43	n/a	
	+ 03:000107	15.27	1.172	No_date	6:48	82.70	n/a	
[DT= 6.00] SUM=	02:001107	115.97	13.099	No_date	6:12	76.39	n/a	
006:0015	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ROUTE CHANNEL ->	02:001107	115.97	13.099	No_date	6:12	76.39	n/a	
[RDT= 6.00] out<-	01:002108	115.97	11.941	No_date	6:24	76.39	n/a	
[L/s/n= 1300./1.670/.030]								
{Vmax= 1.901:Dmax= 1.020}								
006:0016	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
CALIB NASHYD	02:000108	33.50	5.799	No_date	6:06	76.26	.713	
[CN= 86.8: N= 3.00]								
[Tp= .29:DT= 6.00]								
006:0017	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ADD HYD	01:002108	115.97	11.941	No_date	6:24	76.39	n/a	
	+ 02:000108	33.50	5.799	No_date	6:06	76.26	n/a	
[DT= 6.00] SUM=	03:000004	149.47	16.688	No_date	6:18	76.36	n/a	
006:0018	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
PRINT HYD	03:000004	149.47	16.688	No_date	6:18	76.36	n/a	
006:0019	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
CALIB STANDHYD	04:000101	287.80	15.077	No_date	6:24	84.59	.791	
[XIMP=.20:TIMP=.50]								
[LOSS= 2 :CN= 83.4]								
[Pervious area: IAper= 5.00:SLPP= .63:LGP= 700.:MNP=.250:SCP= .0]								
[Impervious area: IAimp= 1.57:SLPI= .63:LGI=3200.:MNI=.017:SCI= .0]								
006:0020	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ROUTE CHANNEL ->	04:000101	287.80	15.077	No_date	6:24	84.59	n/a	
[RDT= 6.00] out<-	05:002101	287.80	14.785	No_date	7:36	84.59	n/a	
[L/s/n= 700./ .420/.030]								
{Vmax= .799:Dmax= .801}								
006:0021	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
* CALIB STANDHYD	04:000102	272.90	16.381	No_date	6:00	77.94	.729	
[XIMP=.13:TIMP=.28]								
[LOSS= 2 :CN= 84.0]								
[Pervious area: IAper= 5.00:SLPP= .98:LGP=1350.:MNP=.250:SCP= .0]								
[Impervious area: IAimp= 1.57:SLPI= .98:LGI= 40.:MNI=.017:SCI= .0]								
006:0022	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ADD HYD	04:000102	272.90	16.381	No_date	6:00	77.94	n/a	
	+ 05:002101	287.80	14.785	No_date	7:36	84.59	n/a	
[DT= 6.00] SUM=	06:000001	560.70	26.504	No_date	7:42	81.35	n/a	
006:0023	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
PRINT HYD	06:000001	560.70	26.504	No_date	7:42	81.35	n/a	
006:0024	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ROUTE CHANNEL ->	06:000001	560.70	26.504	No_date	7:42	81.35	n/a	
[RDT= 6.00] out<-	04:002109	560.70	25.911	No_date	7:48	81.35	n/a	
[L/s/n= 1000./ .540/.030]								
{Vmax= 1.158:Dmax= 1.177}								
006:0025	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
CALIB NASHYD	05:000109	35.10	5.835	No_date	6:12	76.26	.713	
[CN= 86.8: N= 3.00]								
[Tp= .32:DT= 6.00]								
006:0026	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ADD HYD	04:002109	560.70	25.911	No_date	7:48	81.35	n/a	
	+ 05:000109	35.10	5.835	No_date	6:12	76.26	n/a	
[DT= 6.00] SUM=	06:001109	595.80	26.500	No_date	7:48	81.05	n/a	
006:0027	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ROUTE CHANNEL ->	06:001109	595.80	26.500	No_date	7:48	81.05	n/a	
[RDT= 6.00] out<-	04:002110	595.80	26.330	No_date	7:54	81.05	n/a	
[L/s/n= 900./ .710/.030]								
{Vmax= 1.131:Dmax= .969}								
006:0028	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
CALIB NASHYD	05:000110	21.80	4.622	No_date	6:06	76.98	.720	
[CN= 87.2: N= 3.00]								
[Tp= .22:DT= 6.00]								
006:0029	-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm-----R.V.-R.C.-							
ADD HYD	04:002110	595.80	26.330	No_date	7:54	81.05	n/a	

```

                                SWM.Sum
                                + 05:000110    21.80    4.622 No_date    6:06    76.98 n/a
                                [DT= 6.00] SUM= 06:001110    617.60    26.681 No_date    7:54    80.91 n/a
006:0030-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 06:001110    617.60    26.681 No_date    7:54    80.91 n/a
[RDT= 6.00] out<- 04:002111    617.60    26.569 No_date    8:00    80.91 n/a
[L/S/n= 920./1.250/.030]
{Vmax= 2.173:Dmax= 1.057}
006:0031-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   01:000111    17.30     3.458 No_date    6:06    75.55 .706
[CN= 86.4: N= 3.00]
[Tp= .23:DT= 6.00]
006:0032-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD        01:000111    17.30     3.458 No_date    6:06    75.55 n/a
                                + 04:002111    617.60    26.569 No_date    8:00    80.91 n/a
                                [DT= 6.00] SUM= 02:000002    634.90    26.845 No_date    8:00    80.76 n/a
006:0033-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD      02:000002    634.90    26.845 No_date    8:00    80.76 n/a
#*****
# ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN
006:0034-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD        03:000004    149.47    16.688 No_date    6:18    76.36 n/a
                                + 02:000002    634.90    26.845 No_date    8:00    80.76 n/a
                                [DT= 6.00] SUM= 09:001108    784.37    40.288 No_date    6:18    79.92 n/a
#*****
#*****
# SUBCATCHMENT CONTAINING CEMETERY LANDS
#*****
# PROPOSED IMPERVIOUSNESS LESS THAN 20%
# THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURF
#
#*****
# DRAINAGE FROM 201A (EXTERNAL)
#*****
006:0035-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   01:201A     68.20     8.399 No_date    6:18    72.54 .678
[CN= 86.0: N= 3.00]
[Tp= .47:DT= 6.00]
#Route NHYD=201A through Channel SMT-2
006:0036-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 01:201A     68.20     8.399 No_date    6:18    72.54 n/a
[RDT= 6.00] out<- 02:SMT-2R    68.20     8.049 No_date    6:24    72.54 n/a
[L/S/n= 450./ .750/.030]
{Vmax= 1.187:Dmax= .684}
#*****
# DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d
#*****
006:0037-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   01:A1a      .80       .149 No_date    6:06    75.54 .706
[CN= 87.7: N= 3.00]
[Tp= .27:DT= 6.00]
006:0038-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD  03:A1b      6.10     1.976 No_date    6:00    72.77 .680
[CN= 86.1: N= 3.00]
[Tp= .07:DT= 3.00]
006:0039-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   04:A1c      3.20     .832 No_date    6:03    74.73 .699
[CN= 87.2: N= 3.00]
[Tp= .14:DT= 3.00]
006:0040-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   06:A1d      5.30     1.121 No_date    6:06    74.86 .700
[CN= 87.3: N= 3.00]
[Tp= .21:DT= 6.00]
006:0041-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 06:A1d      5.30     1.121 No_date    6:06    74.86 n/a
[RDT= 6.00] out<- 07:A1d      5.30     .291 No_date    6:36    74.86 n/a

```

```

                                SWM.sum
overflow <= 08:OVR                .00      .000 No_date    0:00      .00 n/a
{MxStoUsed=.1850E+00, TotovfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
006:0042-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                07:A1d                5.30      .291 No_date    6:36      74.86 n/a
                        + 08:OVR                .00      .000 No_date    0:00      .00 n/a
[DT= 6.00] SUM= 06:A1dPND  5.30      .291 No_date    6:36      74.86 n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d
*****
006:0043-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                01:A1a                .80      .149 No_date    6:06      75.54 n/a
                        + 02:SMT-2R           68.20     8.049 No_date    6:24      72.54 n/a
                        + 03:A1b                6.10     1.976 No_date    6:00      72.77 n/a
                        + 04:A1c                3.20     .832 No_date    6:03      74.73 n/a
                        + 06:A1dPND           5.30     .291 No_date    6:36      74.86 n/a
[DT= 3.00] SUM= 05:SMT2   83.60     8.867 No_date    6:24      73.01 n/a
*****
# DRAINAGE FROM 201B (EXTERNAL)
*****
006:0044-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          01:201B           13.40     2.177 No_date    6:12      72.54 .678
[CN= 86.0: N= 3.00]
[TP= .31:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)
*****
006:0045-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          02:B1a                4.60     1.095 No_date    6:03      74.34 .695
[CN= 87.0: N= 3.00]
[TP= .17:DT= 3.00]
006:0046-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1a                4.60     1.095 No_date    6:03      74.34 n/a
[RDT= 3.00] out<- 04:B1a                4.60     .313 No_date    6:27      74.34 n/a
overflow <= 08:OVR                .00      .000 No_date    0:00      .00 n/a
{MxStoUsed=.1451E+00, TotovfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
006:0047-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                04:B1a                4.60     .313 No_date    6:27      74.34 n/a
                        + 08:OVR                .00      .000 No_date    0:00      .00 n/a
[DT= 3.00] SUM= 02:B1aPND  4.60     .313 No_date    6:27      74.34 n/a
006:0048-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                01:201B           13.40     2.177 No_date    6:12      72.54 n/a
                        + 02:B1aPND           4.60     .313 No_date    6:27      74.34 n/a
[DT= 3.00] SUM= 03:201B   18.00     2.469 No_date    6:12      73.00 n/a
*****
# Route NHYD=201B + B1a through Channel SMT-4
*****
006:0049-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 03:201B           18.00     2.469 No_date    6:12      73.00 n/a
* [RDT= 3.00] out<- 01:SMT-4R           18.00     2.268 No_date    6:18      73.00 n/a
  [L/s/n= 600./ .850/.030]
  {Vmax= 1.151:Dmax= .462}
006:0050-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          03:B1b                5.00     1.166 No_date    6:03      72.79 .680
[CN= 86.1: N= 3.00]
[TP= .17:DT= 3.00]
006:0051-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          04:B1c                1.00     .305 No_date    6:00      75.58 .707
[CN= 87.7: N= 3.00]
[TP= .10:DT= 3.00]
006:0052-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD                03:B1b                5.00     1.166 No_date    6:03      72.79 n/a
                        + 04:B1c                1.00     .305 No_date    6:00      75.58 n/a
[DT= 3.00] SUM= 02:B1b/c  6.00     1.439 No_date    6:03      73.25 n/a
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c

```

SWM.sum

```

*****
006:0053-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          01:SMT-4R    18.00    2.268 No_date    6:18    73.00 n/a
                + 02:B1b/c      6.00    1.439 No_date    6:03    73.25 n/a
  [DT= 3.00] SUM= 03:B1East    24.00    3.160 No_date    6:09    73.06 n/a

```

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*****
# DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)
*****

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006:0054-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD  01:B1d      4.30    1.489 No_date    6:00    81.14 .759
  [XIMP=.25:TIMP=.25]
  [LOSS= 2 :CN= 86.0]
  [Pervious area: IAper= 5.00:SLPP= .85:LGP= 30.:MNP=.035:SCP= .0]
  [Impervious area: IAimp= .50:SLPI= .85:LGI= 50.:MNI=.013:SCI= .0]

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006:0055-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 01:B1d      4.30    1.489 No_date    6:00    81.14 n/a
  [RDT= 3.00] out<- 04:B1d      4.30    .269 No_date    6:12    81.14 n/a
  overflow <= 08:OVR          .00    .000 No_date    0:00    .00 n/a
  {MxStoUsed=.1709E+00, TotOvfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}

```

```

006:0056-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          04:B1d      4.30    .269 No_date    6:12    81.14 n/a
                + 08:OVR          .00    .000 No_date    0:00    .00 n/a
  [DT= 3.00] SUM= 01:B1dPND    4.30    .269 No_date    6:12    81.14 n/a

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```

006:0057-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     02:B1f      3.50    1.018 No_date    6:00    74.95 .701
  [CN= 87.4: N= 3.00]
  [Tp= .11:DT= 3.00]

```

```

006:0058-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1f      3.50    1.018 No_date    6:00    74.95 n/a
  [RDT= 3.00] out<- 04:B1f      3.50    .173 No_date    6:24    74.95 n/a
  overflow <= 08:OVR          .00    .000 No_date    0:00    .00 n/a
  {MxStoUsed=.1314E+00, TotOvfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}

```

```

006:0059-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          04:B1f      3.50    .173 No_date    6:24    74.95 n/a
                + 08:OVR          .00    .000 No_date    0:00    .00 n/a
  [DT= 3.00] SUM= 02:B1fPND    3.50    .173 No_date    6:24    74.95 n/a

```

```

006:0060-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD  07:B1e      3.60    1.258 No_date    6:00    81.68 .764
  [XIMP=.27:TIMP=.27]
  [LOSS= 2 :CN= 86.0]
  [Pervious area: IAper= 5.00:SLPP=1.15:LGP= 30.:MNP=.035:SCP= .0]
  [Impervious area: IAimp= .50:SLPI=1.15:LGI= 50.:MNI=.013:SCI= .0]

```

```

006:0061-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 07:B1e      3.60    1.258 No_date    6:00    81.68 n/a
  [RDT= 3.00] out<- 06:B1e      3.60    .214 No_date    6:15    81.68 n/a
  overflow <= 08:OVR          .00    .000 No_date    0:00    .00 n/a
  {MxStoUsed=.1522E+00, TotOvfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}

```

```

006:0062-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          06:B1e      3.60    .214 No_date    6:15    81.68 n/a
                + 08:OVR          .00    .000 No_date    0:00    .00 n/a
  [DT= 3.00] SUM= 07:B1ePND    3.60    .214 No_date    6:15    81.68 n/a

```

```

006:0063-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          01:B1dPND    4.30    .269 No_date    6:12    81.14 n/a
                + 02:B1West      3.50    .173 No_date    6:24    74.95 n/a
                + 07:B1ePND      3.60    .214 No_date    6:15    81.68 n/a
  [DT= 3.00] SUM= 02:B1West    11.40    .654 No_date    6:15    79.41 n/a

```

```

*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
*****

```

```

006:0064-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
  ADD HYD          02:B1West    11.40    .654 No_date    6:15    79.41 n/a
                + 03:B1East    24.00    3.160 No_date    6:09    73.06 n/a
  [DT= 3.00] SUM= 04:SMT4      35.40    3.805 No_date    6:09    75.11 n/a

```

```

*****
# DRAINAGE FROM 201C (EXTERNAL)

```

SWM.sum

```

*****
006:0065-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:201C      91.00   10.699 No_date   6:24   72.54 .678
  [CN= 86.0: N= 3.00]
  [Tp= .50:DT= 6.00]
*****
# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
*****
006:0066-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:C1a       7.00    1.436 No_date   6:06   72.54 .678
  [CN= 86.0: N= 3.00]
  [Tp= .21:DT= 6.00]
*****
# C1a SWM FACILITY
*****
006:0067-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:C1a       7.00    1.436 No_date   6:06   72.54 n/a
  [RDT= 6.00] out<- 06:C1a       6.03    .325 No_date   6:12   72.54 n/a
    overflow <= 08:OVR          .97    .994 No_date   6:12   72.54 n/a
  {MxStoUsed=.1618E+00, TotOvfVol=.7036E-01, N-ovf= 2, TotDurOvf= 0.hrs}
*****
# DISCHARGE FROM C1a SWM FACILITY
*****
006:0068-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           06:C1a       6.03    .325 No_date   6:12   72.54 n/a
  + 08:OVR          .97    .994 No_date   6:12   72.54 n/a
  [DT= 6.00] SUM= 02:C1aPND     7.00    1.319 No_date   6:12   72.54 n/a
006:0069-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD    03:C1b       .50     .171 No_date   6:00   73.49 .687
  [CN= 86.5: N= 3.00]
  [Tp= .04:DT= 2.00]
*****
# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
*****
006:0070-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:201C      91.00   10.699 No_date   6:24   72.54 n/a
  + 02:EX+MC       7.00    1.319 No_date   6:12   72.54 n/a
  + 03:C1b         .50     .171 No_date   6:00   73.49 n/a
  [DT= 2.00] SUM= 02:EX+MC     98.50  11.713 No_date   6:18   72.55 n/a
*****
# Route NHYD=201C through Channel SMT-1
*****
006:0071-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL    -> 02:EX+MC     98.50  11.713 No_date   6:18   72.55 n/a
* [RDT= 2.00] out<- 01:SMT-1     98.50  11.183 No_date   6:22   72.55 n/a
  [L/s/n= 275./ .500/.030]
  {Vmax= .965:Dmax= .789}
006:0072-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD     07:C2       3.80    .886 No_date   6:03   72.79 .680
  [CN= 86.1: N= 3.00]
  [Tp= .17:DT= 3.00]
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS
# EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2
*****
006:0073-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:SMT1     98.50  11.183 No_date   6:22   72.55 n/a
  + 07:C2          3.80    .886 No_date   6:03   72.79 n/a
  [DT= 2.00] SUM= 01:SMT1    102.30  11.525 No_date   6:22   72.55 n/a
*****
# CONFLUENCE SMT 1-4
*****
006:0074-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           04:SMT4     35.40    3.805 No_date   6:09   75.11 n/a
  + 01:SMT1      102.30  11.525 No_date   6:22   72.55 n/a

```



```

                                SWM.sum
[DT= 2.00] SUM= 02:SMT1-4    137.70    14.977 No_date    6:20    73.21    n/a
*****
# DRAINAGE FROM 201D (EXTERNAL)
*****
006:0075-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:201D      28.90    3.907 No_date    6:18    72.54    .678
[CN= 86.0: N= 3.00]
[Tp= .41:DT= 6.00]
*****
# SUBCATCHMENT 201D ROUTED
# THROUGH Channel SMT-3
*****
006:0076-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 02:201D      28.90    3.907 No_date    6:18    72.54    n/a
[RDT= 6.00] out<- 03:SMT-3R      28.90    3.923 No_date    6:18    72.54    n/a
[L/S/n= 100./ .700/.030]
{Vmax= 1.481:Dmax= 1.020}
*****
# DRAINAGE FROM CEMETERY LANDS D1a, D1b
*****
006:0077-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:D1a      1.90      .515 No_date    6:00    76.09    .711
[CN= 88.0: N= 3.00]
[Tp= .13:DT= 3.00]
006:0078-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      07:D1b      1.90      .578 No_date    6:00    72.54    .678
[CN= 86.0: N= 3.00]
[Tp= .09:DT= 3.00]
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b
*****
006:0079-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          02:D1a      1.90      .515 No_date    6:00    76.09    n/a
+ 03:SMT-3R      28.90    3.923 No_date    6:18    72.54    n/a
+ 07:D1b         1.90      .578 No_date    6:00    72.54    n/a
[DT= 3.00] SUM= 06:SMT3      32.70    4.289 No_date    6:12    72.75    n/a
*****
# CONFLUENCE SMT 1-3
*****
006:0080-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:SMT1     102.30   11.525 No_date    6:22    72.55    n/a
+ 04:SMT4         35.40    3.805 No_date    6:09    75.11    n/a
+ 06:SMT3         32.70    4.289 No_date    6:12    72.75    n/a
[DT= 2.00] SUM= 03:SMT1-3   170.40   19.103 No_date    6:18    73.12    n/a
*****
# TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D
*****
006:0081-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:SMT1     102.30   11.525 No_date    6:22    72.55    n/a
+ 04:SMT4         35.40    3.805 No_date    6:09    75.11    n/a
+ 06:SMT3         32.70    4.289 No_date    6:12    72.75    n/a
+ 05:SMT2         83.60    8.867 No_date    6:24    73.01    n/a
[DT= 2.00] SUM= 08:1201     254.00   27.734 No_date    6:20    73.09    n/a
006:0082-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 08:1201     254.00   27.734 No_date    6:20    73.09    n/a
* [RDT= 2.00] out<- 03:002202     254.00   27.015 No_date    6:26    73.09    n/a
[L/S/n= 475./1.050/.030]
{Vmax= 1.184:Dmax= .702}
006:0083-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      04:000202     21.60    3.673 No_date    6:12    76.26    .713
[CN= 86.8: N= 3.00]
[Tp= .30:DT= 6.00]
006:0084-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:002202     254.00   27.015 No_date    6:26    73.09    n/a
+ 04:000202     21.60    3.673 No_date    6:12    76.26    n/a

```

```

                                SWM.sum
[DT= 2.00] SUM= 02:001202  275.60  29.716 No_date  6:24  73.34  n/a
006:0085-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          03:000203  26.30   5.247 No_date  6:06  76.26  .713
[CN= 86.8: N= 3.00]
[Tp= .24:DT= 6.00]
006:0086-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD              03:000203  26.30   5.247 No_date  6:06  76.26  n/a
+ 02:001202  275.60  29.716 No_date  6:24  73.34  n/a
[DT= 2.00] SUM= 04:000003  301.90  32.906 No_date  6:20  73.59  n/a
006:0087-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD           04:000003  301.90  32.906 No_date  6:20  73.59  n/a
*****
# SUBCATCHMENT 204 AREA REVISED
# NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha
*****
006:0088-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD          02:000204  53.60   5.593 No_date  6:30  75.38  .705
[CN= 87.6: N= 3.00]
[Tp= .63:DT= 6.00]
006:0089-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD              02:000204  53.60   5.593 No_date  6:30  75.38  n/a
+ 04:000003  301.90  32.906 No_date  6:20  73.59  n/a
[DT= 2.00] SUM= 03:001204  355.50  38.245 No_date  6:22  73.86  n/a
*****
# ROUTE through channel 205 ELIMINATED, OUTSIDE OF STUDY AREA
*****
# SUBCATCHMENT 205 ELIMINATED, OUTSIDE OF STUDY AREA
*****
# ID REVISED TO ID=9, PREVIOUSLY ID=1
*****
006:0090-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD              09:001108  784.37  40.288 No_date  6:18  79.92  n/a
+ 03:001204  355.50  38.245 No_date  6:22  73.86  n/a
[DT= 2.00] SUM= 02:000008  1139.87  78.317 No_date  6:20  78.03  n/a
006:0091-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD           02:000008  1139.87  78.317 No_date  6:20  78.03  n/a
*****
006:0002-----
FINISH

```

 WARNINGS / ERRORS / NOTES

- 001:0008 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.
- 001:0011 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.
- 001:0013 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.
 *** WARNING: For areas with impervious ratios below
 20%, this routine may not be applicable.
- 001:0021 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.
- 001:0038 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.
- 001:0049 ROUTE CHANNEL ->
 *** WARNING: Requested routing DT > than inflow DT.
 Routing DT set to inflow hydrograph DT.

SWM.sum

001:0054 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

001:0060 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

001:0069 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

001:0071 ROUTE CHANNEL ->
 *** WARNING: Requested routing DT > than inflow DT.
 Routing DT set to inflow hydrograph DT.

001:0078 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

001:0082 ROUTE CHANNEL ->
 *** WARNING: Requested routing DT > than inflow DT.
 Routing DT set to inflow hydrograph DT.

002:0008 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

002:0011 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

002:0013 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.
 *** WARNING: For areas with impervious ratios below
 20%, this routine may not be applicable.

002:0021 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

002:0038 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

002:0049 ROUTE CHANNEL ->
 *** WARNING: Requested routing DT > than inflow DT.
 Routing DT set to inflow hydrograph DT.

002:0054 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

002:0060 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

002:0069 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

002:0071 ROUTE CHANNEL ->
 *** WARNING: Requested routing DT > than inflow DT.
 Routing DT set to inflow hydrograph DT.

002:0078 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

002:0082 ROUTE CHANNEL ->
 *** WARNING: Requested routing DT > than inflow DT.
 Routing DT set to inflow hydrograph DT.

003:0008 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

003:0011 CALIB NASHYD
 *** WARNING: Time step is too large for value of TP.
 R.V. may be ok. Peak flow could be off.

003:0013 CALIB STANDHYD
 *** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

SWM.sum

*** WARNING: For areas with impervious ratios below
20%, this routine may not be applicable.

003:0021 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

003:0038 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

003:0049 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

003:0054 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

003:0060 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

003:0069 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

003:0071 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

003:0078 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

003:0082 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

004:0008 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

004:0011 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

004:0013 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.
*** WARNING: For areas with impervious ratios below
20%, this routine may not be applicable.

004:0021 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

004:0038 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

004:0049 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

004:0054 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

004:0060 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

004:0069 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

004:0071 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

004:0078 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

004:0082 ROUTE CHANNEL ->

SWM.sum

*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

005:0008 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

005:0011 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

005:0013 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.
*** WARNING: For areas with impervious ratios below
20%, this routine may not be applicable.

005:0021 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

005:0038 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

005:0049 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

005:0054 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

005:0060 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

005:0069 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

005:0071 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

005:0078 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

005:0082 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

006:0008 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

006:0011 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

006:0013 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.
*** WARNING: For areas with impervious ratios below
20%, this routine may not be applicable.

006:0021 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

006:0038 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

006:0049 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

006:0054 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

006:0060 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!

SWM.sum

Use a smaller DT or a larger area.

006:0069 CALIB NASHYD

*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

006:0071 ROUTE CHANNEL ->

*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

006:0078 CALIB NASHYD

*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.

006:0082 ROUTE CHANNEL ->

*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.

Simulation ended on 2011-12-06 at 12:10:23

SWMR.dat

2 Metric units

```

*****
*# Project Name: [Holy Family Catholic Cemetery] Project Number: [111063]
*# Date : 08-16-2011
*# Modeller : [C. Silvestri]
*# Company : Philips Engineering Ltd
*# License # : 3569108
*****

```

```

START START=0.0 HRS METOUT=0 NSTORM=1 NRUN=1
HAZEL.STM

```

```

*
READ STORM "STORM.001"
*

```

```

* Subarea 103 - Entering Property
CALIB NASHYD ID= 1 NHYD=103 DT=5 min AREA=42.1 ha DWF=0.0 cms
CN=94 IA=0 mm N=3.0 Tp=0.399 hrs END=-1

```

```

* Route through channel 104
ROUTE CHANNEL ID=2 NHYD=2104 IDIN=1 DT=5.0 min
CHLGTH=440 m CHSLP=1 % FPSLP=1 %
VSN=104 NSEG=3
ROUGH DIST(m)
0.04 59
-0.03 60
0.04 89

```

DIST(m)	ELEV(m)
0.0	179.5
18.0	178.5
59.0	178.0
59.5	177.7
60.0	178.0
89.0	178.5

```

* Subarea 104 - Creek Block Upstream of Proposed 5 acre Pond
CALIB NASHYD ID= 3 NHYD=104 DT=5 min AREA= 24.1 ha DWF=0.0 cms
CN=94.0 IA=0 mm N=3.0 Tp=0.208 hrs END=-1

```

```

*
ADD HYD ID= 1 NHYD=1104 IDI= 3 IDII= 2
*

```

```

* Route through channel 105
ROUTE CHANNEL ID=2 NHYD=2105 IDIN=1 DT=5.0 min
CHLGTH=365 m CHSLP=0.4 % FPSLP=0.4 %
VSN=105 NSEG=3
ROUGH DIST(m)
0.04 52
-0.03 53
0.04 100

```

DIST(m)	ELEV(m)
0.0	178.0
28.0	177.0
52.0	176.9
52.5	176.6
53.0	176.9
80.0	177.0
100.0	177.5

```

* Subarea 105 - Creek Block Upstream of Proposed Pond 2nd 5 acre pond
CALIB NASHYD ID=3 NHYD=105 DT=5 min AREA= 19.2 ha DWF=0.0 cms
CN=95 IA=0 mm N=3.0 Tp=0.176 hrs END=-1

```

```

*
ADD HYD ID=1 NHYD=1105 IDI=3 IDII=2
*

```

SWMR.dat

ROUTE CHANNEL ID=2 NHYD=2106 IDIN=1 DT=5.0 min
 CHLGTH=385 m CHSLP=0.67 % FPSLP=0.67 %
 VSN=106 NSEG=3
 ROUGH DIST(m)
 0.04 77
 -0.03 78
 0.04 120

DIST(m)	ELEV(m)
0.0	176.0
20.0	175.5
32.0	175.0
58.0	174.5
77.0	174.5
77.5	174.2
78.0	174.5
102.0	175.0
120.0	175.5

*
 * Subarea 106 - Creek Block Upstream of Pond
 CALIB NASHYD ID= 3 NHYD=106 DT=5 min AREA= 15.3 ha DWF=0.0 cms
 CN=95 IA=0 mm N=3.0 Tp=0.168 hrs END=-1

*
 ADD HYD ID= 1 NHYD=1106 IDI= 3 IDII= 2

*
 * Subarea 107 - East drainage area for tributary
 CALIB STANDHYD ID= 3 NHYD=107 DT=5 min AREA= 15.27 ha
 XIMP=0.10 TIMP=0.17 DWF=0.0 cms LOSS=2 CN=93
 DPSP=5.0 mm SLPP=1.27 % LGP=717 MNP=0.250 SCP=0.0
 DPSI=1.57 mm SLPI=1.27 % LGI=100 MNI=0.017 SCI=0.0
 END=-1

*
 ADD HYD ID=2 NHYD=1107 IDI=1 IDII=3

*
 * Route Eastern Section of Tributary through Channel-108
 ROUTE CHANNEL ID=1 NHYD=2108 IDIN=2 DT=5.0 min
 CHLGTH=1300 m CHSLP=1.67 % FPSLP=1.67 %
 VSN=108 NSEG=3
 ROUGH DIST(m)
 0.04 65
 -0.03 66
 0.04 110

DIST(m)	ELEV(m)
0.0	172.0
42.0	167.5
51.0	160.0
65.0	159.0
65.5	158.7
66.0	159.0
88.0	165.0
110.0	170.0

*
 * Subarea 108
 CALIB NASHYD ID= 2 NHYD=108 DT=5 min AREA=33.5 ha DWF=0.0 cms
 CN=95 IA=0 mm N=3.0 Tp=0.295 hrs END=-1

*
 ADD HYD ID=3 NHYD=004 IDI=1 IDII=2
 PRINT HYD ID=3 NPCYC=-1

*
 * CALCULATE FLOWS ENTERING SITE FROM NORTHWEST
 * Subarea 101 -
 CALIB STANDHYD ID= 4 NHYD=101 DT=5 min AREA= 287.8 ha
 XIMP=0.20 TIMP=0.495 DWF=0.0 cms LOSS=2 CN=93
 DPSP=5.0 mm SLPP=0.625 % LGP=700 MNP=0.250 SCP=0.0

SWMR.dat

DPSI=1.57 mm SLPI=0.625 % LGI=3200 MNI=0.017 SCI=0.0
 END=-1

*
 *

*Route NHYD=101 through channel 102

ROUTE CHANNEL ID=5 NHYD=2101 IDIN=4 DT=5.0 min
 CHLGTH=700 m CHSLP=0.42 % FPSLP=0.42 %
 VSN=102 NSEG=3
 ROUGH DIST(m)
 0.04 110
 -0.03 111
 0.04 160

DIST(m)	ELEV(m)
0.0	182.5
90.0	180.0
110.0	179.8
110.5	179.5
111.0	179.8
130.0	180.0
160.0	182.5

*

* Subarea 102 -
 CALIB STANDHYD

ID= 4 NHYD=102 DT=5 min AREA= 272.9 ha
 XIMP=0.13 TIMP=0.275 DWF=0.0 cms LOSS=2 CN=93
 DPSP=5.0 mm SLPP=0.98 % LGP=1350 MNP=0.250 SCP=0.0
 DPSI=1.57 mm SLPI=0.98 % LGI=40 MNI=0.017 SCI=0.0
 END=-1

*

* Node 001

ADD HYD ID= 6 NHYD= 001 IDI=4 IDII=5
 PRINT HYD ID= 6 NPCYC=-1

*

*Route NHYD=001 through channel 109

ROUTE CHANNEL ID=4 NHYD=2109 IDIN=6 DT=5.0 min
 CHLGTH=1000 m CHSLP=0.54 % FPSLP=0.54 %
 VSN=109 NSEG=3
 ROUGH DIST(m)
 0.04 50
 -0.03 51
 0.04 88

DIST(m)	ELEV(m)
0.0	176.0
14.0	175.5
18.0	175.0
26.0	174.0
42.0	173.0
50.0	173.0
50.5	172.7
51.0	173.0
58.0	173.5
88.0	174.0

* Subarea 109

CALIB NASHYD ID= 5 NHYD=109 DT=5 min AREA= 35.1 ha DWF=0.0 cms
 CN=95 IA=0 mm N=3.0 Tp=0.318 hrs END=-1

*

ADD HYD ID= 6 NHYD=1109 IDI=4 IDII=5

*

*Route NHYD=1109 through Channel 110

ROUTE CHANNEL ID=4 NHYD=2110 IDIN=6 DT=5.0 min
 CHLGTH=900 m CHSLP=0.71 % FPSLP=0.71 %
 VSN=110 NSEG=3
 ROUGH DIST(m)
 0.04 61

SWMR.dat

-0.03 62
0.04 114

DIST(m)	ELEV(m)
0.0	175.0
10.0	172.5
18.0	170.0
20.0	168.0
61.0	167.5
61.5	167.2
62.0	167.5
80.0	170.0
98.0	172.5
114.0	175.5

*

* Subarea 110

CALIB NASHYD

ID= 5 NHYD=110 DT=5 min AREA= 21.8 ha DWF=0.0 cms
CN=95 IA=0 mm N=3.0 Tp=0.215 hrs END=-1

*

ADD HYD

ID= 6 NHYD= 1110 IDI=4 IDII=5

*

*Route NHYD=1110 through Channel 111

ROUTE CHANNEL

ID=4 NHYD=2111 IDIN=6 DT=5.0 min
CHLGTH=920 m CHSLP=1.25 % FPSLP=1.25 %
VSN=111 NSEG=3
ROUGH DIST(m)
0.04 56
-0.03 57
0.04 105

DIST(m)	ELEV(m)
0.0	172.0
16.0	170.0
44.0	159.0
56.0	159.0
56.5	158.7
57.0	159.0
84.0	170.0
105.0	175.0

*

* Subarea 111

CALIB NASHYD

ID= 1 NHYD=0111 DT=5 min AREA=17.3 ha DWF=0.0 cms
CN=94 IA=0mm N=3.0 Tp=0.235 hrs END=-1

* Node 002

ADD HYD

ID=2 NHYD= 002 IDI=1 IDII=4

PRINT HYD

ID=2 NPCYC=-1

*

*

** ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN

* At confluence of two main branches

ADD HYD ID=9 NHYD=1108 IDI=3 IDII=2

*

* Calculations for South-West section of site (3 subcatchments have been created for catchment 201)

** SUBCATCHMENT CONTAINING CEMETERY LANDS

** PROPOSED IMPERVIOUSNESS LESS THAN 20%

** THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURFACES

**

SWMR.dat

```

*****
*# DRAINAGE FROM 201A (EXTERNAL)
*****
*%-----|-----
CALIB NASHYD      ID=1  NHYD="201A"  DT=5 min  AREA=68.2 ha  DWF=0.0 cms
                  CN=94.0  IA=3 mm  N=3.0   Tp=0.47 hrs  END=-1
*%-----|-----
*#Route NHYD=201A through Channel SMT-2
ROUTE CHANNEL    ID=2  NHYD="SMT-2"  IDIN=1  DT=5.0 min
                  CHLGTH=450 m  CHSLP=0.75 %  FPSLP=0.75 %
                  VSN=CA1  NSEG=3
                  ROUGH DIST(m)
                    0.04  35
                    -0.03  45
                    0.04  90

                  DIST(m)  ELEV(m)
                    0.0    101.0
                    35.0   100.5
                    40.0   100.0
                    45.0   100.5
                    90.0   101.0
*%-----|-----
*****
*# DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d
*****
*%-----|-----
CALIB NASHYD      ID=1  NHYD="A1a"  DT=5 min  AREA=0.8 ha  DWF=0.0 cms
                  CN=94.19 IA=3 mm  N=3.0   Tp=0.27 hrs  END=-1
*%-----|-----
CALIB NASHYD      ID=3  NHYD="A1b"  DT=3 min  AREA=6.1 ha  DWF=0.0 cms
                  CN=94.01 IA=3 mm  N=3.0   Tp=0.07 hrs  END=-1
*%-----|-----
CALIB NASHYD      ID=4  NHYD="A1c"  DT=3 min  AREA=3.2 ha  DWF=0.0 cms
                  CN=94.14 IA=3 mm  N=3.0   Tp=0.14 hrs  END=-1
*%-----|-----
CALIB NASHYD      ID=6  NHYD="A1d"  DT=5 min  AREA=5.3 ha  DWF=0.0 cms
                  CN=94.15 IA=3 mm  N=3.0   Tp=0.21 hrs  END=-1
*%-----|-----
ROUTE RESERVOIR  IDout=[7],  NHYD=["A1d"],  IDin=[6],
                  RDT=[5](min),
                  TABLE of ( OUTFLOW-STORAGE ) values
                    (cms) - (ha-m)
                    [ 0.0 , 0.0 ]
                    [ 0.034, 0.028 ]
                    [ 0.103, 0.043 ]
                    [ 0.142, 0.059 ]
                    [ 0.198, 0.093 ]
                    [ 0.241, 0.129 ]
                    [ 0.278, 0.168 ]
                    [ 0.310, 0.209 ]
                    [ -1 , -1 ] (max twenty pts)
                  IDovf=[8], NHYDovf=["OVR"]
*%-----|-----
ADD HYD          IDsum=[6], NHYD=["A1dPND"], IDs to add=[7+8]
*%-----|-----
*****
*# TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d
*****
*%-----|-----
ADD HYD          IDsum=[5], NHYD=["SMT2"], IDs to add=[1+2+3+4+6]
*%-----|-----
*****
*# DRAINAGE FROM 201B (EXTERNAL)
*****

```

SWMR.dat

```

*%-----|-----
CALIB NASHYD      ID=1  NHYD="201B"  DT=5 min  AREA=13.4 ha  DWF=0.0 cms
                  CN=94.0  IA=3 mm   N=3.0    Tp=0.31 hrs  END=-1

*#*****
*# DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)
*#*****
*%-----|-----
CALIB NASHYD      ID=2  NHYD="B1a"  DT=3 min  AREA=4.6 ha  DWF=0.0 cms
                  CN=94.11 IA=3 mm   N=3.0    Tp=0.17 hrs  END=-1

*%-----|-----
ROUTE RESERVOIR   IDout=[4],  NHYD=["B1a"],  IDin=[2],
                  RDT=[5](min),
                  TABLE of ( OUTFLOW-STORAGE ) values
                                (cms) - (ha-m)
                                [ 0.0 , 0.0 ]
                                [ 0.034, 0.019 ]
                                [ 0.103, 0.029 ]
                                [ 0.142, 0.040 ]
                                [ 0.198, 0.062 ]
                                [ 0.241, 0.087 ]
                                [ 0.278, 0.114 ]
                                [ 0.310, 0.142 ]
                                [ 0.325, 0.158 ]
                                [ -1 , -1 ] (max twenty pts)
                  IDovf=[8],  NHYDovf=["OVR"]

*%-----|-----
ADD HYD           IDsum=[2],  NHYD=["B1aPND"],  IDs to add=[4+8]
*%-----|-----
ADD HYD           IDsum=[3],  NHYD=["SMT-4"],  IDs to add=[1+2]
*%-----|-----
*#Route NHYD=201B + B1a through Channel SMT-4
ROUTE CHANNEL     ID=1  NHYD="SMT-4R"  IDIN=3    DT=5.0 min
                  CHLGTH=600 m  CHSLP=0.85 %  FPSLP=0.85 %
                  VSN=CB1  NSEG=3
                  ROUGH DIST(m)
                    0.04  35
                    -0.03 45
                    0.04  90

                  DIST(m)  ELEV(m)
                    0.0    101.0
                    35.0   100.5
                    40.0   100.0
                    45.0   100.5
                    90.0   101.0

*%-----|-----
CALIB NASHYD      ID=3  NHYD="B1b"  DT=3 min  AREA=5.0 ha  DWF=0.0 cms
                  CN=94.02 IA=3 mm   N=3.0    Tp=0.17 hrs  END=-1

*%-----|-----
CALIB NASHYD      ID=4  NHYD="B1c"  DT=3 min  AREA=1.0 ha  DWF=0.0 cms
                  CN=94.19 IA=3 mm   N=3.0    Tp=0.10 hrs  END=-1

*%-----|-----
ADD HYD           IDsum=[2],  NHYD=["B1b/c"],  IDs to add=[3+4]
*%-----|-----
*#*****
*# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c
*#*****
*%-----|-----
ADD HYD           IDsum=[3],  NHYD=["B1East"],  IDs to add=[1+2]
*%-----|-----
*#*****
*# DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)
*#*****
*%-----|-----

```

CALIB STANDHYD

SWMR.dat
ID=[1], NHYD=["B1d"], DT=[3](min), AREA=[4.3](ha),
XIMP=[0.2535], TIMP=[0.2535], DWF=[0.0](cms), LOSS=[2],
SCS curve number CN=[94],
Pervious surfaces: IAper=[5](mm), SLPP=[1.00](%),
LGP=[30](m), MNP=[0.035], SCP=[0](min),
Impervious surfaces: IAimp=[0.5](mm), SLPI=[1.00](%),
LGI=[50](m), MNI=[0.013], SCI=[0](min),
END=-1

ROUTE RESERVOIR

IDout=[4], NHYD=["B1d"], IDin=[1],
RDT=[5](min),
TABLE of (OUTFLOW-STORAGE) values

(cms) - (ha-m)	
[0.0 , 0.0]	
[0.034 , 0.031]	
[0.103 , 0.048]	
[0.142 , 0.065]	
[0.198 , 0.101]	
[0.241 , 0.139]	
[0.278 , 0.180]	
[0.310 , 0.223]	
[-1 , -1]	

(max twenty pts)

IDovf=[8], NHYDovf=["OVR"]

ADD HYD

IDsum=[1], NHYD=["B1dPND"], IDs to add=[4+8]

CALIB NASHYD

ID=2 NHYD="B1f" DT=3 min AREA=3.5 ha DWF=0.0 cms
CN=94.15 IA=3 mm N=3.0 Tp=0.11 hrs END=-1

ROUTE RESERVOIR

IDout=[4], NHYD=["B1f"], IDin=[2],
RDT=[5](min),
TABLE of (OUTFLOW-STORAGE) values

(cms) - (ha-m)	
[0.0 , 0.0]	
[0.044 , 0.025]	
[0.076 , 0.038]	
[0.099 , 0.052]	
[0.132 , 0.081]	
[0.159 , 0.112]	
[0.182 , 0.145]	
[0.202 , 0.181]	
[0.212 , 0.199]	
[-1 , -1]	

(max twenty pts)

IDovf=[8], NHYDovf=["OVR"]

ADD HYD

IDsum=[2], NHYD=["B1fPND"], IDs to add=[4+8]

CALIB STANDHYD

ID=[7], NHYD=["B1e"], DT=[3](min), AREA=[3.6](ha),
XIMP=[0.2694], TIMP=[0.2694], DWF=[0.0](cms), LOSS=[2],
SCS curve number CN=[94],
Pervious surfaces: IAper=[5](mm), SLPP=[1.00](%),
LGP=[30](m), MNP=[0.035], SCP=[0](min),
Impervious surfaces: IAimp=[0.5](mm), SLPI=[1.00](%),
LGI=[50](m), MNI=[0.013], SCI=[0](min),
END=-1

ROUTE RESERVOIR

IDout=[6], NHYD=["B1e"], IDin=[7],
RDT=[5](min),
TABLE of (OUTFLOW-STORAGE) values

(cms) - (ha-m)	
[0.0 , 0.0]	
[0.034 , 0.041]	
[0.103 , 0.062]	
[0.142 , 0.085]	
[0.198 , 0.133]	

```

SWMR.dat
[ 0.241, 0.184]
[ 0.278, 0.240]
[ 0.310, 0.299]
[ -1, -1]

```

(max twenty pts)

IDovf=[8], NHYDovf=["OVR"]

```

*%-----|-----
ADD HYD   | IDsum=[7], NHYD=["B1ePND"], IDs to add=[6+8]
*%-----|-----
ADD HYD   | IDsum=[2], NHYD=["B1d/e/f"], IDs to add=[1+2+7]
*%-----|-----

```

```

*#*****
*# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
*#*****

```

```

*%-----|-----
ADD HYD   | IDsum=[4], NHYD=["SMT4"], IDs to add=[2+3]
*%-----|-----

```

```

*#*****
*# DRAINAGE FROM 201C (EXTERNAL)
*#*****
CALIB NASHYD   ID=1 NHYD="201C" DT=5 min AREA=91.0 ha DWF=0.0 cms
                CN=94.0 IA=3 mm N=3.0 Tp=0.50 hrs END=-1

```

```

*# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
*#*****

```

```

*%-----|-----
CALIB NASHYD   ID=2 NHYD="C1a" DT=5 min AREA=7.0 ha DWF=0.0 cms
                CN=94.11 IA=3 mm N=3.0 Tp=0.21 hrs END=-1

```

```

*%-----|-----
ROUTE RESERVOIR IDout=[6], NHYD=["C1a"], IDin=[2],
                RDT=[5](min),

```

TABLE of (OUTFLOW-STORAGE) values

```

                (cms) - (ha-m)
[ 0.0, 0.0]
[ 0.034, 0.021]
[ 0.103, 0.032]
[ 0.142, 0.043]
[ 0.198, 0.067]
[ 0.241, 0.093]
[ 0.278, 0.120]
[ 0.310, 0.150]
[ 0.325, 0.165]
[ -1, -1]

```

(max twenty pts)

IDovf=[8], NHYDovf=["OVR"]

```

*%-----|-----
ADD HYD   | IDsum=[2], NHYD=["C1aPND"], IDs to add=[6+8]
*%-----|-----

```

```

CALIB NASHYD   ID=3 NHYD="C1b" DT=2 min AREA=0.5 ha DWF=0.0 cms
                CN=94.06 IA=3 mm N=3.0 Tp=0.04 hrs END=-1

```

```

*#*****
*# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
*#*****

```

```

*%-----|-----
ADD HYD   | IDsum=[2], NHYD=["EX+MC"], IDs to add=[1+2+3]
*%-----|-----

```

```

*#*****
*# Route NHYD=201c through Channel SMT-1
*#*****
ROUTE CHANNEL   ID=1 NHYD="SMT-1" IDIN=2 DT=5.0 min
                CHLGTH=275 m CHSLP=0.50 % FPSLP=0.50 %
                VSN=CC1 NSEG=3
                ROUGH DIST(m)
                0.04 35
                -0.03 45
                0.04 90

```

SWMR.dat

DIST(m)	ELEV(m)
0.0	101.0
35.0	100.5
40.0	100.0
45.0	100.5
90.0	101.0

```

*%-----|-----
CALIB NASHYD      ID=7 NHYD="C2" DT=3 min AREA=3.8 ha DWF=0.0 cms
                  CN=94.02 IA=3 mm N=3.0 Tp=0.17 hrs END=-1
*%-----|-----
*#*****|-----
*# TOTAL DRAINAGE FROM SUBCATCHMENTS
*# EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2
*#*****|-----
ADD HYD           IDsum=[1], NHYD=["SMT1"], IDs to add=[1+7]
*%-----|-----
*#*****|-----
*# CONFLUENCE SMT 1-4
*#*****|-----
*%-----|-----
ADD HYD           IDsum=[2], NHYD=["SMT1-4"], IDs to add=[4+1]
*%-----|-----
*#*****|-----
*# DRAINAGE FROM 201D (EXTERNAL)
*#*****|-----
CALIB NASHYD      ID=2 NHYD="201D" DT=5 min AREA=28.9 ha DWF=0.0 cms
                  CN=94.0 IA=3 mm N=3.0 Tp=0.41 hrs END=-1
*%-----|-----

*#*****|-----
*# SUBCATCHMENT 201D ROUTED
*# THROUGH Channel SMT-3
*#*****|-----
*%-----|-----
ROUTE CHANNEL     ID=3 NHYD="SMT-3" IDIN=2 DT=5.0 min
                  CHLGTH=100 m CHSLP=0.70 % FPSLP=0.70 %
                  VSN=CD1 NSEG=3
                  ROUGH DIST(m)
                   0.04 10
                   -0.03 15
                   0.04 20

                  DIST(m)  ELEV(m)
                   0.0    178.0
                   26.0   177.6
                   30.0   176.0
                   34.0   177.57
                   50.0   178.0
*%-----|-----
*#*****|-----
*# DRAINAGE FROM CEMETERY LANDS D1a, D1b
*#*****|-----
*%-----|-----
CALIB NASHYD      ID=2, NHYD=["D1a"], DT=3 min, AREA=1.9 ha, DWF=0.0 cms
                  CN=94.22, IA=3 mm, N=3.0, Tp=0.13 hrs, END=-1
*%-----|-----
CALIB NASHYD      ID=7, NHYD=["D1b"], DT=3 min, AREA=1.9 ha, DWF=0.0 cms
                  CN=94.00, IA=3 mm, N=3.0, Tp=0.09 hrs, END=-1
*%-----|-----
*#*****|-----
*# TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b
*#*****|-----
*%-----|-----
ADD HYD           IDsum=[6], NHYD=["STM3"], IDs to add=[2+3+7]
    
```

SWMR.dat

```

*%-----|-----
*#*****
*# CONFLUENCE SMT 1-3
*#*****
*%-----|-----
ADD HYD          IDsum=[3], NHYD=["SMT1-3"], IDs to add=[1+4+6]
*%-----|-----
*#*****
*# TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D
*#*****
ADD HYD          ID=[8]  NHYD=["1201"]  IDs to add=[1+4+5+6]
*%-----|-----
*
*
*Route NHYD=201 through Channel 202
ROUTE CHANNEL   ID=3  NHYD=2202  IDIN=8  DT=5.0 min
                CHLGTH=475 m  CHSLP=1.05 %  FPSLP=1.05 %
                VSN=202  NSEG=3
                ROUGH DIST(m)
                0.04  55
                -0.03  56
                0.04  105

                DIST(m)  ELEV(m)
                0.0      180.0
                15.0     175.0
                55.0     174.9
                55.5     174.6
                56.0     174.9
                70.0     175.0
                105.0    180.0

*
* Subarea 202
CALIB NASHYD    ID= 4  NHYD=202  DT=5 min  AREA=21.6 ha  DWF=0.0 cms
                CN=95  IA=0 mm  N=3.0  Tp=0.303 hrs  END=-1

*
ADD HYD         ID=2  NHYD=1202  IDI=3  IDII=4
*
* Subarea 203
CALIB NASHYD    ID= 3  NHYD=203  DT=5 min  AREA=26.3 ha  DWF=0.0 cms
                CN=95  IA=0mm  N=3.0  Tp=0.240 hrs  END=-1

*
* Node 003 - exit from site
ADD HYD         ID= 4  NHYD=003  IDI=3  IDII=2
PRINT HYD      ID= 4  NPCYC=-1
*
*#*****
*# SUBCATCHMENT 204 AREA REVISED
*# NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha
*#*****
*
*Subarea 204 - off site
CALIB NASHYD    ID= 2  NHYD=204  DT=5 min  AREA=53.6 ha  DWF=0.0 cms
                CN=95  IA=0 mm  N=3.0  Tp=0.626 hrs  END=-1

*
ADD HYD         ID= 3  NHYD= 1204  IDI= 2  IDII= 4
*
*#*****
*# ROUTE through Channel 205 ELIMINATED,  OUTSIDE OF STUDY AREA
*#*****
*
*#*****
*# SUBCATCHMENT 205 ELIMINTATED,  OUTSIDE OF STUDY AREA
*#*****
*

```


SWMR.dat

```
* Confluence of tributaries off site
*****
*# ID REVISED TO ID=9, PREVIOUSLY ID=1
*****
ADD HYD          ID=2  NHYD=008  IDI=9  IDII=3
PRINT HYD       ID=2  NPCYC=-1
*****
```

FINISH

SWMR.sum

SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM O O 9 9 9 9
SSSSS W W W M M M H H H H Y M M M O O ## 9 9 9 9 Ver. 4.02
S W W M M H H Y M M O O 9999 9999 July 1999
SSSSS W W M M H H Y M M 000 9 9 9 9 # 3569108
StormWater Management Hydrologic Model 999 999 =====

***** SWMHYMO-99 Ver/4.02 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 727-5199 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****

+++++++ Licensed user: Philips Engineering Ltd ++++++++
+++++++ Burlington SERIAL#:3569108 ++++++++
+++++++

***** ++++++ PROGRAM ARRAY DIMENSIONS ++++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 15000 *****
***** Max. number of flow points : 15000 *****

*** DESCRIPTION SUMMARY TABLE HEADERS (units depend on METOUT in START) ***
*** ----- ***
*** ID: Hydrograph Identification numbers, (1-10). ***
*** NHYD: Hydrograph reference numbers, (6 digits or characters). ***
*** AREA: Drainage area associated with hydrograph, (ac.) or (ha.). ***
*** QPEAK: Peak flow of simulated hydrograph, (ft^3/s) or (m^3/s). ***
*** TpeakDate_hh:mm is the date and time of the peak flow. ***
*** R.V.: Runoff Volume of simulated hydrograph, (in) or (mm). ***
*** R.C.: Runoff Coefficient of simulated hydrograph, (ratio). ***
*** *: see WARNING or NOTE message printed at end of run. ***
*** **: see ERROR message printed at end of run. ***

***** SUMMARY OUTPUT *****

* DATE: 2011-12-06 TIME: 12:48:29 RUN COUNTER: 000140 *

* Input filename: G:\work\105128\water\SWMHYMO\2011NO~1\REG\SWMR.dat *
* Output filename: G:\work\105128\water\SWMHYMO\2011NO~1\REG\SWMR.out *
* Summary filename: G:\work\105128\water\SWMHYMO\2011NO~1\REG\SWMR.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *

SWMR.sum

```
*****
# Project Name: [Holy Family Catholic Cemetery] Project Number: [111063]
# Date : 08-16-2011
# Modeller : [C. Silvestri]
# Company : Philips Engineering Ltd
# License # : 3569108
*****
```

RUN:COMMAND#

```
001:0001-----
START
[TZERO = .00 hrs on 0]
[METOUT= 2 (1=imperial, 2=metric output)]
[NSTORM= 1 ]
[NRUN = 1 ]

001:0002-----
READ STORM
Filename = STORM.001
Comment = Regional storm event (Hurricane Hazel)
[SDT=60.00:SDUR= 12.00:PTOT= 212.00]

001:0003-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 01:000103 42.10 5.719 No_date 10:05 196.94 .929
[CN= 94.0: N= 3.00]
[Tp= .40:DT= 5.00]

001:0004-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:000103 42.10 5.719 No_date 10:05 196.94 n/a
[RDT= 5.00] out<- 02:002104 42.10 5.626 No_date 10:15 196.94 n/a
[L/S/n= 440./1.000/.030]
{Vmax= .789:Dmax= .610}

001:0005-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 03:000104 24.10 3.506 No_date 10:00 196.94 .929
[CN= 94.0: N= 3.00]
[Tp= .21:DT= 5.00]

001:0006-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000104 24.10 3.506 No_date 10:00 196.94 n/a
+ 02:002104 42.10 5.626 No_date 10:15 196.94 n/a
[DT= 5.00] SUM= 01:001104 66.20 8.880 No_date 10:05 196.94 n/a

001:0007-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:001104 66.20 8.880 No_date 10:05 196.94 n/a
[RDT= 5.00] out<- 02:002105 66.20 8.712 No_date 10:10 196.94 n/a
[L/S/n= 365./ .400/.030]
{Vmax= .596:Dmax= .605}

001:0008-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 03:000105 19.20 2.806 No_date 10:00 199.42 .941
[CN= 95.0: N= 3.00]
[Tp= .18:DT= 5.00]

001:0009-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000105 19.20 2.806 No_date 10:00 199.42 n/a
+ 02:002105 66.20 8.712 No_date 10:10 196.94 n/a
[DT= 5.00] SUM= 01:001105 85.40 11.273 No_date 10:05 197.50 n/a

001:0010-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 01:001105 85.40 11.273 No_date 10:05 197.50 n/a
[RDT= 5.00] out<- 02:002106 85.40 11.137 No_date 10:10 197.50 n/a
[L/S/n= 385./ .670/.030]
{Vmax= .830:Dmax= .655}

001:0011-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 03:000106 15.30 2.237 No_date 10:00 199.42 .941
[CN= 95.0: N= 3.00]
[Tp= .17:DT= 5.00]

001:0012-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 03:000106 15.30 2.237 No_date 10:00 199.42 n/a
+ 02:002106 85.40 11.137 No_date 10:10 197.50 n/a
[DT= 5.00] SUM= 01:001106 100.70 13.116 No_date 10:05 197.79 n/a

001:0013-----ID:NHYD-----AREA-----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 03:000107 15.27 1.602 No_date 11:00 193.07 .911
```

SWMR.sum

```

[XIMP=.10:TIMP=.17]
[LOSS= 2 :CN= 93.0]
[Pervious area: IAper= 5.00:SLPP=1.27:LGP= 717.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI=1.27:LGI= 100.:MNI=.017:SCI= .0]
001:0014-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:001106   100.70   13.116 No_date   10:05   197.79  n/a
                + 03:000107    15.27    1.602 No_date   11:00   193.07  n/a
[DT= 5.00] SUM= 02:001107   115.97   14.432 No_date   10:10   197.17  n/a
001:0015-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 02:001107   115.97   14.432 No_date   10:10   197.17  n/a
[RDT= 5.00] out<- 01:002108   115.97   14.097 No_date   10:20   197.17  n/a
[L/s/n= 1300./1.670/.030]
{Vmax= 1.934:Dmax= 1.048}
001:0016-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   02:000108    33.50    4.791 No_date   10:00   199.42  .941
[CN= 95.0: N= 3.00]
[Tp= .29:DT= 5.00]
001:0017-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:002108   115.97   14.097 No_date   10:20   197.17  n/a
                + 02:000108    33.50    4.791 No_date   10:00   199.42  n/a
[DT= 5.00] SUM= 03:000004   149.47   18.476 No_date   10:15   197.67  n/a
001:0018-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD       03:000004   149.47   18.476 No_date   10:15   197.67  n/a
001:0019-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB STANDHYD 04:000101   287.80   26.354 No_date   11:15   200.03  .944
[XIMP=.20:TIMP=.50]
[LOSS= 2 :CN= 93.0]
[Pervious area: IAper= 5.00:SLPP= .63:LGP= 700.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI= .63:LGI=3200.:MNI=.017:SCI= .0]
001:0020-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 04:000101   287.80   26.354 No_date   11:15   200.03  n/a
[RDT= 5.00] out<- 05:002101   287.80   26.125 No_date   11:25   200.03  n/a
[L/s/n= 700./ .420/.030]
{Vmax= .955:Dmax= .954}
001:0021-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 04:000102   272.90   24.298 No_date   11:00   195.30  .921
[XIMP=.13:TIMP=.28]
[LOSS= 2 :CN= 93.0]
[Pervious area: IAper= 5.00:SLPP= .98:LGP=1350.:MNP=.250:SCP= .0]
[Impervious area: IAimp= 1.57:SLPI= .98:LGI= 40.:MNI=.017:SCI= .0]
001:0022-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          04:000102   272.90   24.298 No_date   11:00   195.30  n/a
                + 05:002101   287.80   26.125 No_date   11:25   200.03  n/a
[DT= 5.00] SUM= 06:000001   560.70   49.278 No_date   11:00   197.73  n/a
001:0023-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD       06:000001   560.70   49.278 No_date   11:00   197.73  n/a
001:0024-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 06:000001   560.70   49.278 No_date   11:00   197.73  n/a
* [RDT= 5.00] out<- 04:002109   560.70   48.639 No_date   11:35   197.73  n/a
[L/s/n= 1000./ .540/.030]
{Vmax= 1.225:Dmax= 1.295}
001:0025-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD   05:000109    35.10    4.969 No_date   10:00   199.42  .941
[CN= 95.0: N= 3.00]
[Tp= .32:DT= 5.00]
001:0026-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          04:002109   560.70   48.639 No_date   11:35   197.73  n/a
                + 05:000109    35.10    4.969 No_date   10:00   199.42  n/a
[DT= 5.00] SUM= 06:001109   595.80   50.677 No_date   11:20   197.83  n/a
001:0027-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 06:001109   595.80   50.677 No_date   11:20   197.83  n/a
[RDT= 5.00] out<- 04:002110   595.80   50.591 No_date   11:30   197.83  n/a
[L/s/n= 900./ .710/.030]
{Vmax= 1.529:Dmax= 1.203}
001:0028-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-

```

ID	Description	ID:NHYD	AREA	QPEAK	TpeakDate_hh:mm	R.V.	R.C.
	CALIB NASHYD	05:000110	21.80	3.178	No_date 10:00	199.42	.941
	[CN= 95.0: N= 3.00]						
	[Tp= .22:DT= 5.00]						
001:0029	ADD HYD	04:002110	595.80	50.591	No_date 11:30	197.83	n/a
	+ 05:000110	21.80	3.178	No_date 10:00	199.42	n/a	
	[DT= 5.00] SUM= 06:001110	617.60	51.769	No_date 11:15	197.88	n/a	
001:0030	ROUTE CHANNEL ->	06:001110	617.60	51.769	No_date 11:15	197.88	n/a
	[RDT= 5.00] out<- 04:002111	617.60	51.727	No_date 11:20	197.88	n/a	
	[L/S/n= 920./1.250/.030]						
	{Vmax= 2.629:Dmax= 1.406}						
001:0031	CALIB NASHYD	01:000111	17.30	2.508	No_date 10:00	196.94	.929
	[CN= 94.0: N= 3.00]						
	[Tp= .23:DT= 5.00]						
001:0032	ADD HYD	01:000111	17.30	2.508	No_date 10:00	196.94	n/a
	+ 04:002111	617.60	51.727	No_date 11:20	197.88	n/a	
	[DT= 5.00] SUM= 02:000002	634.90	52.989	No_date 11:15	197.86	n/a	
001:0033	PRINT HYD	02:000002	634.90	52.989	No_date 11:15	197.86	n/a

# ID revised to ID=9, PREVIOUSLY ID=1 WAS BEING OVER-WRITEN							
001:0034	ADD HYD	03:000004	149.47	18.476	No_date 10:15	197.67	n/a
	+ 02:000002	634.90	52.989	No_date 11:15	197.86	n/a	
	[DT= 5.00] SUM= 09:001108	784.37	68.678	No_date 11:05	197.82	n/a	

# SUBCATCHMENT CONTAINING CEMETERY LANDS							

# PROPOSED IMPERVIOUSNESS LESS THAN 20%							
# THEREFORE, CN VALUE HAS BEEN MODIFIED TO ACCOUNT FOR PROPOSED IMPERVIOUS SURF							
#							

# DRAINAGE FROM 201A (EXTERNAL)							

001:0035	CALIB NASHYD	01:201A	68.20	8.910	No_date 10:10	193.95	.915
	[CN= 94.0: N= 3.00]						
	[Tp= .47:DT= 5.00]						
#Route NHYD=201A through Channel SMT-2							
001:0036	ROUTE CHANNEL ->	01:201A	68.20	8.910	No_date 10:10	193.95	n/a
	[RDT= 5.00] out<- 02:SMT-2	68.20	8.827	No_date 10:20	193.95	n/a	
	[L/S/n= 450./ .750/.030]						
	{Vmax= 1.184:Dmax= .694}						

# DRAINAGE FROM CEMETERY LANDS A1a, A1b, A1c, A1d							

001:0037	CALIB NASHYD	01:A1a	.80	.115	No_date 10:00	194.42	.917
	[CN= 94.2: N= 3.00]						
	[Tp= .27:DT= 5.00]						
001:0038	* CALIB NASHYD	03:A1b	6.10	.890	No_date 10:00	193.98	.915
	[CN= 94.0: N= 3.00]						
	[Tp= .07:DT= 3.00]						
001:0039	CALIB NASHYD	04:A1c	3.20	.467	No_date 10:00	194.30	.917
	[CN= 94.1: N= 3.00]						
	[Tp= .14:DT= 3.00]						
001:0040	CALIB NASHYD	06:A1d	5.30	.771	No_date 10:00	194.33	.917

SWMR.sum

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[CN= 94.2: N= 3.00]
[TP= .21:DT= 5.00]
001:0041-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 06:A1d      5.30      .771 No_date  10:00  194.33  n/a
[RD= 5.00] out<- 07:A1d      4.56      .310 No_date   9:55  194.33  n/a
overflow <= 08:OVR      .74      .460 No_date  10:00  194.33  n/a
{MxStoUsed=.2085E+00, TotOvfVo]=.1447E+00, N-ovf= 2, TotDurovf= 1.hrs}
001:0042-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          07:A1d      4.56      .310 No_date   9:55  194.33  n/a
+ 08:OVR          .74      .460 No_date  10:00  194.33  n/a
[DT= 5.00] SUM= 06:A1dPND  5.30      .770 No_date  10:00  194.33  n/a
#*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201A + A1a + A1b + A1c + A1d
#*****
001:0043-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:A1a      .80      .115 No_date  10:00  194.42  n/a
+ 02:SMT-2       68.20     8.827 No_date  10:20  193.95  n/a
+ 03:A1b         6.10      .890 No_date  10:00  193.98  n/a
+ 04:A1c         3.20      .467 No_date  10:00  194.30  n/a
+ 06:A1dPND      5.30      .770 No_date  10:00  194.33  n/a
[DT= 3.00] SUM= 05:SMT2   83.60    10.587 No_date  10:15  194.07  n/a
#*****
# DRAINAGE FROM 201B (EXTERNAL)
#*****
001:0044-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD    01:201B    13.40     1.897 No_date  10:00  193.95  .915
[CN= 94.0: N= 3.00]
[TP= .31:DT= 5.00]
#*****
# DRAINAGE FROM CEMETERY LANDS B1a, B1b, B1c (B-Series, East Drainage)
#*****
001:0045-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD    02:B1a      4.60      .671 No_date  10:00  194.23  .916
[CN= 94.1: N= 3.00]
[TP= .17:DT= 3.00]
001:0046-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1a      4.60      .671 No_date  10:00  194.23  n/a
[RD= 3.00] out<- 04:B1a      4.17      .325 No_date  10:00  194.23  n/a
overflow <= 08:OVR      .43      .345 No_date  10:00  194.23  n/a
{MxStoUsed=.1577E+00, TotOvfVo]=.8385E-01, N-ovf= 1, TotDurovf= 1.hrs}
001:0047-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          04:B1a      4.17      .325 No_date  10:00  194.23  n/a
+ 08:OVR          .43      .345 No_date  10:00  194.23  n/a
[DT= 3.00] SUM= 02:B1aPND  4.60      .670 No_date  10:00  194.23  n/a
001:0048-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          01:201B    13.40     1.897 No_date  10:00  193.95  n/a
+ 02:B1aPND      4.60      .670 No_date  10:00  194.23  n/a
[DT= 3.00] SUM= 03:SMT-4   18.00     2.568 No_date  10:00  194.02  n/a
#Route NHYD=201B + B1a through Channel SMT-4
001:0049-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 03:SMT-4    18.00     2.568 No_date  10:00  194.02  n/a
* [RD= 3.00] out<- 01:SMT-4R  18.00     2.442 No_date  10:09  194.02  n/a
[L/S/n= 600./ .850/.030]
{Vmax= 1.162:Dmax= .468}
001:0050-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD    03:B1b      5.00      .729 No_date  10:00  194.00  .915
[CN= 94.0: N= 3.00]
[TP= .17:DT= 3.00]
001:0051-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD    04:B1c      1.00      .146 No_date  10:00  194.42  .917
[CN= 94.2: N= 3.00]
[TP= .10:DT= 3.00]
001:0052-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:B1b      5.00      .729 No_date  10:00  194.00  n/a
+ 04:B1c          1.00      .146 No_date  10:00  194.42  n/a

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SWMR.sum
[DT= 3.00] SUM= 02:B1b/c 6.00 .875 No_date 10:00 194.07 n/a
#*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B + B1a + B1b + B1c
#*****
001:0053-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:SMT-4R 18.00 2.442 No_date 10:09 194.02 n/a
+ 02:B1b/c 6.00 .875 No_date 10:00 194.07 n/a
[DT= 3.00] SUM= 03:B1East 24.00 3.237 No_date 10:06 194.04 n/a
#*****
# DRAINAGE FROM CEMETERY LANDS B1d, B1e, B1f (B-series, West Drainage)
#*****
001:0054-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 01:B1d 4.30 .629 No_date 10:00 196.92 .929
[XIMP=.25:TIMP=.25]
[LOSS= 2 :CN= 94.0]
[Pervious area: IAper= 5.00:SLPP=1.00:LGP= 30.:MNP=.035:SCP= .0]
[Impervious area: IAimp= .50:SLPI=1.00:LGI= 50.:MNI=.013:SCI= .0]
001:0055-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 01:B1d 4.30 .629 No_date 10:00 196.92 n/a
[RDT= 3.00] out<- 04:B1d 4.09 .310 No_date 10:15 196.92 n/a
overflow <= 08:OVR .21 .157 No_date 10:15 196.92 n/a
{MxStoUsed=.2231E+00, TotOvfVol=.4185E-01, N-ovf= 1, TotDurovf= 1.hrs}
001:0056-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 04:B1d 4.09 .310 No_date 10:15 196.92 n/a
+ 08:OVR .21 .157 No_date 10:15 196.92 n/a
[DT= 3.00] SUM= 01:B1dPND 4.30 .467 No_date 10:15 196.92 n/a
001:0057-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD 02:B1f 3.50 .511 No_date 10:00 194.33 .917
[CN= 94.2: N= 3.00]
[Tp= .11:DT= 3.00]
001:0058-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:B1f 3.50 .511 No_date 10:00 194.33 n/a
[RDT= 3.00] out<- 04:B1f 3.22 .212 No_date 10:09 194.33 n/a
overflow <= 08:OVR .28 .226 No_date 10:09 194.33 n/a
{MxStoUsed=.1987E+00, TotOvfVol=.5475E-01, N-ovf= 2, TotDurovf= 1.hrs}
001:0059-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 04:B1f 3.22 .212 No_date 10:09 194.33 n/a
+ 08:OVR .28 .226 No_date 10:09 194.33 n/a
[DT= 3.00] SUM= 02:B1fPND 3.50 .438 No_date 10:09 194.33 n/a
001:0060-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB STANDHYD 07:B1e 3.60 .526 No_date 10:00 197.23 .930
[XIMP=.27:TIMP=.27]
[LOSS= 2 :CN= 94.0]
[Pervious area: IAper= 5.00:SLPP=1.00:LGP= 30.:MNP=.035:SCP= .0]
[Impervious area: IAimp= .50:SLPI=1.00:LGI= 50.:MNI=.013:SCI= .0]
001:0061-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 07:B1e 3.60 .526 No_date 10:00 197.23 n/a
[RDT= 3.00] out<- 06:B1e 3.60 .277 No_date 11:03 197.23 n/a
overflow <= 08:OVR .00 .000 No_date 0:00 .00 n/a
{MxStoUsed=.2379E+00, TotOvfVol=.0000E+00, N-ovf= 0, TotDurovf= 0.hrs}
001:0062-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 06:B1e 3.60 .277 No_date 11:03 197.23 n/a
+ 08:OVR .00 .000 No_date 0:00 .00 n/a
[DT= 3.00] SUM= 07:B1ePND 3.60 .277 No_date 11:03 197.23 n/a
001:0063-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 01:B1dPND 4.30 .467 No_date 10:15 196.92 n/a
+ 02:B1d/e/ 3.50 .438 No_date 10:09 194.33 n/a
+ 07:B1ePND 3.60 .277 No_date 11:03 197.23 n/a
[DT= 3.00] SUM= 02:B1d/e/ 11.40 1.115 No_date 10:15 196.22 n/a
#*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201B+B1a+B1b+B1c+B1d+B1e+B1f
#*****
001:0064-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD 02:B1d/e/ 11.40 1.115 No_date 10:15 196.22 n/a
+ 03:B1East 24.00 3.237 No_date 10:06 194.04 n/a

```

```

                                SWMR.sum
                                35.40   4.237 No_date   10:15  194.74  n/a
[DT= 3.00] SUM= 04:SMT4
*****
# DRAINAGE FROM 201C (EXTERNAL)
*****
001:0065-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      01:201C      91.00   11.714 No_date   10:15  193.95  .915
  [CN= 94.0: N= 3.00]
  [Tp= .50:DT= 5.00]
*****
# DRAINAGE FROM CEMETERY LANDS C1a, C1b, C2
*****
001:0066-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:C1a       7.00    1.018 No_date   10:00  194.23  .916
  [CN= 94.1: N= 3.00]
  [Tp= .21:DT= 5.00]
001:0067-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE RESERVOIR -> 02:C1a       7.00    1.018 No_date   10:00  194.23  n/a
  [RDT= 5.00] out<- 06:C1a       5.25    .325 No_date   9:30   194.23  n/a
    overflow <= 08:OVR          1.75    .692 No_date   10:00  194.23  n/a
  {MxStoUsed=.1642E+00, TotOvfVol=.3391E+00, N-ovf= 2, TotDurOvf= 2.hrs}
001:0068-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           06:C1a       5.25    .325 No_date   9:30   194.23  n/a
  + 08:OVR          1.75    .692 No_date   10:00  194.23  n/a
  [DT= 5.00] SUM= 02:C1aPND       7.00    1.017 No_date   10:00  194.23  n/a
001:0069-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      03:C1b       .50     .073 No_date   10:00  194.10  .916
  [CN= 94.1: N= 3.00]
  [Tp= .04:DT= 2.00]
*****
# DISCHARGE FROM EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS
*****
001:0070-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:201C      91.00   11.714 No_date   10:15  193.95  n/a
  + 02:EX+MC        7.00    1.017 No_date   10:00  194.23  n/a
  + 03:C1b          .50     .073 No_date   10:00  194.10  n/a
  [DT= 2.00] SUM= 02:EX+MC       98.50   12.666 No_date   10:14  193.98  n/a
*****
# Route NHYD=201C through channel SMT-1
*****
001:0071-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL -> 02:EX+MC       98.50   12.666 No_date   10:14  193.98  n/a
* [RDT= 2.00] out<- 01:SMT-1     98.50   12.602 No_date   10:18  193.98  n/a
  [L/s/n= 275./ .500/.030]
  {Vmax= .968:Dmax= .805}
001:0072-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      07:C2       3.80    .554 No_date   10:00  194.00  .915
  [CN= 94.0: N= 3.00]
  [Tp= .17:DT= 3.00]
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS
# EXTERNAL LANDS (WEST) + MILTON CEMETERY LANDS + C2
*****
001:0073-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:SMT1      98.50   12.602 No_date   10:18  193.98  n/a
  + 07:C2           3.80    .554 No_date   10:00  194.00  n/a
  [DT= 2.00] SUM= 01:SMT1      102.30   13.045 No_date   10:16  193.98  n/a
*****
# CONFLUENCE SMT 1-4
*****
001:0074-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           04:SMT4       35.40    4.237 No_date   10:15  194.74  n/a
  + 01:SMT1        102.30   13.045 No_date   10:16  193.98  n/a
  [DT= 2.00] SUM= 02:SMT1-4     137.70   17.256 No_date   10:16  194.17  n/a
*****
# DRAINAGE FROM 201D (EXTERNAL)

```


SWMR.sum

```

*****
001:0075-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:201D      28.90      3.899 No_date  10:10  193.95 .915
  [CN= 94.0: N= 3.00]
  [Tp= .41:DT= 5.00]
*****
# SUBCATCHMENT 201D ROUTED
# THROUGH Channel SMT-3
*****
001:0076-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 02:201D      28.90      3.899 No_date  10:10  193.95 n/a
  [RDT= 5.00] out<- 03:SMT-3  28.90      3.904 No_date  10:10  193.95 n/a
  [L/s/n= 100./ .700/.030]
  {Vmax= 1.480:Dmax= 1.020}
*****
# DRAINAGE FROM CEMETERY LANDS D1a, D1b
*****
001:0077-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      02:D1a        1.90        .277 No_date  10:00  194.50 .917
  [CN= 94.2: N= 3.00]
  [Tp= .13:DT= 3.00]
001:0078-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
* CALIB NASHYD      07:D1b        1.90        .277 No_date  10:00  193.95 .915
  [CN= 94.0: N= 3.00]
  [Tp= .09:DT= 3.00]
*****
# TOTAL DRAINAGE FROM SUBCATCHMENTS 201D+D1a+D1b
*****
001:0079-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           02:D1a        1.90        .277 No_date  10:00  194.50 n/a
                  + 03:SMT-3      28.90      3.904 No_date  10:10  193.95 n/a
                  + 07:D1b        1.90        .277 No_date  10:00  193.95 n/a
  [DT= 3.00] SUM= 06:STM3      32.70      4.386 No_date  10:03  193.99 n/a
*****
# CONFLUENCE SMT 1-3
*****
001:0080-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:SMT1      102.30     13.045 No_date  10:16  193.98 n/a
                  + 04:SMT4       35.40      4.237 No_date  10:15  194.74 n/a
                  + 06:STM3       32.70      4.386 No_date  10:03  193.99 n/a
  [DT= 2.00] SUM= 03:SMT1-3   170.40     21.519 No_date  10:16  194.13 n/a
*****
# TOTAL DRAINAGE FROM SUBJECT LANDS + EXT.SUBCATCHMENTS 201A/B/C/D
*****
001:0081-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           01:SMT1      102.30     13.045 No_date  10:16  193.98 n/a
                  + 04:SMT4       35.40      4.237 No_date  10:15  194.74 n/a
                  + 05:SMT2       83.60     10.587 No_date  10:15  194.07 n/a
                  + 06:STM3       32.70      4.386 No_date  10:03  193.99 n/a
  [DT= 2.00] SUM= 08:1201     254.00     32.100 No_date  10:16  194.12 n/a
001:0082-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ROUTE CHANNEL  -> 08:1201     254.00     32.100 No_date  10:16  194.12 n/a
* [RDT= 2.00] out<- 03:002202  254.00     31.916 No_date  10:20  194.12 n/a
  [L/s/n= 475./1.050/.030]
  {Vmax= 1.247:Dmax= .735}
001:0083-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      04:000202     21.60      3.079 No_date  10:00  199.42 .941
  [CN= 95.0: N= 3.00]
  [Tp= .30:DT= 5.00]
001:0084-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD           03:002202     254.00     31.916 No_date  10:20  194.12 n/a
                  + 04:000202     21.60      3.079 No_date  10:00  199.42 n/a
  [DT= 2.00] SUM= 02:001202     275.60     34.698 No_date  10:18  194.53 n/a
001:0085-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD      03:000203     26.30      3.821 No_date  10:00  199.42 .941

```

SWMR.sum

```

[CN= 95.0: N= 3.00]
[TP= .24:DT= 5.00]
001:0086-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          03:000203    26.30    3.821 No_date  10:00  199.42  n/a
                + 02:001202    275.60   34.698 No_date  10:18  194.53  n/a
[DT= 2.00] SUM= 04:000003    301.90   37.995 No_date  10:16  194.96  n/a
001:0087-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD       04:000003    301.90   37.995 No_date  10:16  194.96  n/a
*****
# SUBCATCHMENT 204 AREA REVISED
# NEW AREA = 70.0 ha, PREVIOUSLY = 52.3 ha
*****
001:0088-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
CALIB NASHYD    02:000204    53.60    6.507 No_date  10:30  199.42  .941
[CN= 95.0: N= 3.00]
[TP= .63:DT= 5.00]
001:0089-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          02:000204    53.60    6.507 No_date  10:30  199.42  n/a
                + 04:000003    301.90   37.995 No_date  10:16  194.96  n/a
[DT= 2.00] SUM= 03:001204    355.50   44.391 No_date  10:18  195.63  n/a
*****
# ROUTE through Channel] 205 ELIMINATED, OUTSIDE OF STUDY AREA
# *****
# *****
# SUBCATCHMENT 205 ELIMINTATED, OUTSIDE OF STUDY AREA
# *****
# *****
# ID REVISED TO ID=9, PREVIOUSLY ID=1
# *****
001:0090-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
ADD HYD          09:001108    784.37   68.678 No_date  11:05  197.82  n/a
                + 03:001204    355.50   44.391 No_date  10:18  195.63  n/a
[DT= 2.00] SUM= 02:000008    1139.87  107.826 No_date  11:00  197.14  n/a
001:0091-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
PRINT HYD       02:000008    1139.87  107.826 No_date  11:00  197.14  n/a
*****
001:0092-----ID:NHYD-----AREA----QPEAK-TpeakDate_hh:mm----R.V.-R.C.-
FINISH

```

WARNINGS / ERRORS / NOTES

```

001:0013 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
                Use a smaller DT or a larger area.
*** WARNING: For areas with impervious ratios below
                20%, this routine may not be applicable.
001:0021 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
                Use a smaller DT or a larger area.
001:0024 ROUTE CHANNEL ->
*** WARNING: TRAVEL TIME TABLE was exceeded
001:0038 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
                R.V. may be ok. Peak flow could be off.
001:0049 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
                Routing DT set to inflow hydrograph DT.
001:0054 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
                Use a smaller DT or a larger area.
001:0060 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
                Use a smaller DT or a larger area.
001:0069 CALIB NASHYD

```

SWMR.sum

*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.
001:0071 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.
001:0078 CALIB NASHYD
*** WARNING: Time step is too large for value of TP.
R.V. may be ok. Peak flow could be off.
001:0082 ROUTE CHANNEL ->
*** WARNING: Requested routing DT > than inflow DT.
Routing DT set to inflow hydrograph DT.
simulation ended on 2011-12-06 at 12:48:30

APPENDIX C

SWMHYMO INPUT/OUTPUT INFORMATION

```

2 Metric units
*#-----|
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : JUNE 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT
*#-----|
*#
*#
*#
START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
MILSCS12.002
*
READ STORM STORM_FILENAME "STORM.001"
*
*#-----|
*#
*# PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*# -----
*#
*# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC
*#
CALIB NASHYD ID=[1], NHYD=["101"], DT=[1]min, AREA=[4.1](ha),
DWP=[0](cms), CN/C=[86], IA=[5.00](mm),
N=[3], TP=[0.28]hrs,
RAINFALL=[ , , , ](mm/hr), END=-1
*#-----|
*#
*# POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*# -----
*#
*# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4
*#
CALIB STANDHYD ID=[1], NHYD=["201"], DT=[1](min), AREA=[4.1](ha),
XIMP=[0.36], TIMP=[0.36], DWP=[0](cms), LOSS=[2],
SCS curve number CN=[86],
Pervious surfaces: IAPER=[5.00](mm), SLPP=[2.0](%),
LGP=[5.0](m), MNP=[0.250], SCP=[0](min)
Impervious surfaces: IAIMP=[1.0](mm), SLPI=[1.0](%),
LGI=[15](m), MNI=[0.015], SCI=[0](min),
RAINFALL=[ , , , ](mm/hr), END=-1
*#-----|
*#
*# ROUTE CATCHMENT 201 THROUGH DDUAL STAGE ORIFICE DEVICE
*# -----
*# POST DEVELOPEMENT FLOWS FROM CATCHMENT 201
*#-----|
*#
ROUTE RESERVOIR IDout=[2], NHYD=["201-SWM"], IDin=[1],
RDT=[1](min),
TABLE of ( OUTFLOW-STORAGE ) values
(cms) - (ha-m)
0.0033 0
0.0216 0.01520
0.0512 0.03100
0.0854 0.04750
0.1169 0.06460
0.1424 0.08240
0.1650 0.10090
0.1841 0.12000
0.2014 0.14000
0.2174 0.16060
0.2322 0.18200
0.2393 0.19300
0.2985 0.20410
0.5311 0.22700
-1 -1 (max twenty pts)
*#-----|
*#
*# IDovf=[3], NHYDovf=["OPL-ORP"]
*#-----|
START START=0.0 HRS METOUT=0 NSTORM=1 NRUN=[005]
MILSCS12.005
*
START START=0.0 HRS METOUT=0 NSTORM=1 NRUN=[010]
MILSCS12.010
*
START START=0.0 HRS METOUT=0 NSTORM=1 NRUN=[025]
MILSCS12.025
*
START START=0.0 HRS METOUT=0 NSTORM=1 NRUN=[050]
MILSCS12.050
*
START START=0.0 HRS METOUT=0 NSTORM=1 NRUN=[100]
MILSCS12.100
*
FINISH

```

```

SSSSS W W M M H H Y Y M M OOO          999 999 =====
S      W W W MM MM H H Y Y MM MM O O     9 9 9 9
SSSSS W W W M M M H H H H Y M M O O ##   9999 9999 Ver 4.05
S      W W M M H H Y M M O O              9999 9999 Sept 2011
SSSSS W W M M H H Y M M OOO              9 9 9 9 =====
StormWater Management Hydrologic Model    999 999 =====

```

```

***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhym@jfsa.Com *****

```

```

+++++++ Licensed user: S. Llewellyn & Associates Ltd ++++++
+++++++ Burlington SERIAL#:3902680 ++++++

```

```

+++++ PROGRAM ARRAY DIMENSIONS ++++++
Maximum value for ID numbers : 10
Max. number of rainfall points: 105408
Max. number of flow points : 105408

```

***** DETAILED OUTPUT *****

```

* DATE: 2022-06-28 TIME: 17:43:18 RUN COUNTER: 000743 *
* Input filename: T:\PROJECTS\13084\SWM\SWMHYMO\13084.dat *
* Output filename: T:\PROJECTS\13084\SWM\SWMHYMO\13084.out *
* Summary filename: T:\PROJECTS\13084\SWM\SWMHYMO\13084.sum *
* User comments:
* 1:
* 2:
* 3:

```

```

001:0001-----
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : JUNE 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT
** END OF RUN : 1

```

```

| START | Project dir.: T:\PROJECTS\13084\SWM\SWMHYMO\
| TZERO = .00 hrs on 0
| METOUT= 2 (output = METRIC)
| NRUN = 002
| NSTORM= 1
| # 1=MILSCS12.002

```

```

002:0002-----
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : JUNE 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT

```

```

002:0002-----
| READ STORM | Filename: TOWN OF MILTON 12 HOUR 2 YEAR SCS STORM
| Ptotal= 42.82 mm | Comments: TOWN OF MILTON 12 HOUR 2 YEAR SCS STORM

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.20	.850	3.20	1.690	6.20	10.360	9.20	1.690
.40	.850	3.40	1.690	6.40	6.130	9.40	1.690
.60	.850	3.60	1.690	6.60	4.440	9.60	1.690
.80	.850	3.80	1.690	6.80	4.230	9.80	1.690
1.00	.850	4.00	1.690	7.00	2.960	10.00	1.690
1.20	.850	4.20	2.960	7.20	2.540	10.20	.850
1.40	.850	4.40	2.960	7.40	2.540	10.40	.850
1.60	.850	4.60	2.960	7.60	2.540	10.60	.850
1.80	.850	4.80	2.960	7.80	2.540	10.80	.850
2.00	.850	5.00	2.960	8.00	2.540	11.00	.850
2.20	1.690	5.20	3.810	8.20	1.690	11.20	.850
2.40	1.690	5.40	5.500	8.40	1.690	11.40	.850
2.60	1.690	5.60	12.690	8.60	1.690	11.60	.850
2.80	1.690	5.80	27.710	8.80	1.690	11.80	.850
3.00	1.690	6.00	57.950	9.00	1.690	12.00	.850

```

002:0003-----
*#

```

```

*#*****|
*# PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#*****|
*# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC

```

```

| CALIB NASHYD | Area (ha)= 4.10 Curve Number (CN)=86.00
| 01:101 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .280
Unit Hyd Qpeak (cms)= .559
PEAK FLOW (cms)= .175 (i)
TIME TO PEAK (hrs)= 6.200
RUNOFF VOLUME (mm)= 18.064
TOTAL RAINFALL (mm)= 42.816
RUNOFF COEFFICIENT = .422
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

002:0004-----
*#*****|
*# POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#*****|
*# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4

```

```

| CALIB STANDHYD | Area (ha)= 4.10
| 01:201 DT= 1.00 | Total Imp(%)= 36.00 Dir. Conn.(%)= 36.00
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 1.48 2.62
Dep. Storage (mm)= 1.00 5.00
Average Slope (%)= 1.00 2.00
Length (m)= 15.00 5.00
Mannings n = .015 .250
Max.eff.Inten.(mm/hr)= 57.95 33.73
over (min) 1.00 4.00
Storage Coeff. (min)= 1.11 (ii) 4.24 (ii)
Unit Hyd. Tpeak (min)= 1.00 4.00
Unit Hyd. peak (cms)= 1.01 .27

```

```

*#*****|
*# PEAK FLOW (cms)= .24 .21 .452 (iii)
*# TIME TO PEAK (hrs)= 6.00 6.00 6.000
*# RUNOFF VOLUME (mm)= 41.82 18.06 26.615
*# TOTAL RAINFALL (mm)= 42.82 42.82 42.816
*# RUNOFF COEFFICIENT = .98 .42 .622
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 86.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

002:0005-----
*#
*# ROUTE CATCHMENT 201 THROUGH DDUAL STAGE ORIFICE DEVICE
*#*****|
*# POST DEVELOPEMENT FLOWS FROM CATCHMENT 201
*#*****|
*#

```

```

| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>01: (201 ) |
| OUT<02: (201-SW) |
===== OUTFLOW STORAGE TABLE =====
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
*** WARNING: First OUTFLOW value in table should be ZERO.
.003 .0000E+00 | .184 .1200E+00
.022 .1520E-01 | .201 .1400E+00
.051 .3100E-01 | .217 .1606E+00
.085 .4750E-01 | .232 .1820E+00
.117 .6460E-01 | .239 .1930E+00
.142 .8240E-01 | .299 .2041E+00
.165 .1009E+00 | .531 .2270E+00

```

```

ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >01: (201 ) 4.10 .452 6.000 26.615
OUTFLOW<02: (201-SW) 4.10 .090 6.217 26.617
OVERFLOW<03: (OFL-OR) .00 .000 .000 .000
TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00
PEAK FLOW REDUCTION [Qout/Qin](%)= 19.959
TIME SHIFT OF PEAK FLOW (min)= 13.00
MAXIMUM STORAGE USED (ha.m.)=.5009E-01

```

```

002:0006-----
*#
** END OF RUN : 4

```

```

| START | Project dir.: T:\PROJECTS\13084\SWM\SWMHYMO\
| TZERO = .00 hrs on 0
| METOUT= 2 (output = METRIC)
| NRUN = 005
| NSTORM= 1
| # 1=MILSCS12.005

```

```

005:0002-----
*#-----
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : JUNE 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT
*#-----
*#-----
*#-----

```

```

005:0002-----
*#-----
*# READ STORM          Filename: TOWN OF MILTON 12 HOUR 5 YEAR SCS STORM
*# Ptotal= 59.90 mm   Comments: TOWN OF MILTON 12 HOUR 5 YEAR SCS STORM
*#-----
*# TIME RAIN          TIME RAIN          TIME RAIN          TIME RAIN
*# hrs mm/hr         hrs mm/hr         hrs mm/hr         hrs mm/hr
*# .20 1.180         3.20 2.370         6.20 14.500       9.20 2.370
*# .40 1.180         3.40 2.370         6.40 8.580        9.40 2.370
*# .60 1.180         3.60 2.370         6.60 6.220        9.60 2.370
*# .80 1.180         3.80 2.370         6.80 5.920        9.80 2.370
*# 1.00 1.180        4.00 2.370        7.00 4.140        10.00 2.370
*# 1.20 1.180        4.20 4.140        7.20 3.550        10.20 1.180
*# 1.40 1.180        4.40 4.140        7.40 3.550        10.40 1.180
*# 1.60 1.180        4.60 4.140        7.60 3.550        10.60 1.180
*# 1.80 1.180        4.80 4.140        7.80 3.550        10.80 1.180
*# 2.00 1.180        5.00 4.140        8.00 3.550        11.00 1.180
*# 2.20 2.370        5.20 5.330        8.20 2.370        11.20 1.180
*# 2.40 2.370        5.40 7.700        8.40 2.370        11.40 1.180
*# 2.60 2.370        5.60 17.760       8.60 2.370        11.60 1.180
*# 2.80 2.370        5.80 38.780       8.80 2.370        11.80 1.180
*# 3.00 2.370        6.00 81.100       9.00 2.370        12.00 1.180

```

```

005:0003-----
*#-----
*# PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#-----
*#-----
*# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC)
*#-----

```

```

*# CALIB NASHYD          Area (ha)= 4.10 Curve Number (CN)=86.00
*# 01:101 DT= 1.00     Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
*# U.H. Tp(hrs)= .280
*#-----
*# Unit Hyd Qpeak (cms)= .559
*# PEAK FLOW (cms)= .308 (i)
*# TIME TO PEAK (hrs)= 6.183
*# RUNOFF VOLUME (mm)= 31.312
*# TOTAL RAINFALL (mm)= 59.897
*# RUNOFF COEFFICIENT = .523
*# (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

005:0004-----
*#-----
*# POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#-----
*#-----
*# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4
*#-----

```

```

*# CALIB STANDHYD          Area (ha)= 4.10
*# 01:201 DT= 1.00     Total Imp(%)= 36.00 Dir. Conn.(%)= 36.00
*#-----
*# IMPERVIOUS          PERVIOUS (i)
*# Surface Area (ha)= 1.48 2.62
*# Dep. Storage (mm)= 1.00 5.00
*# Average Slope (%)= 1.00 2.00
*# Length (m)= 15.00 5.00
*# Mannings n = .015 .250
*# Max. eff. Inten.(mm/hr)= 81.10 56.43
*# over (min)= 1.00 4.00
*# Storage Coeff. (min)= .97 (ii) 3.52 (ii)
*# Unit Hyd. Tpeak (min)= 1.00 4.00
*# Unit Hyd. peak (cms)= 1.09 .31
*#-----
*# PEAK FLOW (cms)= .33 .38 *TOTALS*
*# TIME TO PEAK (hrs)= 6.00 6.00 6.000
*# RUNOFF VOLUME (mm)= 58.90 31.31 41.242
*# TOTAL RAINFALL (mm)= 59.90 59.90 59.897
*# RUNOFF COEFFICIENT = .98 .52 .689
*# (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
*# CN* = 86.0 Ia = Dep. Storage (Above)
*# (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
*# THAN THE STORAGE COEFFICIENT.
*# (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

005:0005-----
*#-----
*# ROUTE CATCHMENT 201 THROUGH DDUAL STAGE ORIPICE DEVICE
*#-----
*# POST DEVELOPEMENT FLOWS FROM CATCHMENT 201
*#-----
*#-----

```

```

*# ROUTE RESERVOIR          Requested routing time step = 1.0 min.
*# IN:01:(201 )
*# OUT:02:(201-SW)
*#-----
*# OUTFLOW STORAGE TABLE
*# OUTFLOW STORAGE OUTFLOW STORAGE
*# (cms) (ha.m.) (cms) (ha.m.)
*# *** WARNING: First OUTFLOW value in table should be ZERO.
*# .003 .0000E+00 .184 .1200E+00
*# .022 .1520E-01 .201 .1400E+00

```

```

.051 .3100E-01 .217 .1606E+00
.085 .4750E-01 .232 .1820E+00
.117 .6460E-01 .239 .1930E+00
.142 .8240E-01 .299 .2041E+00
.165 .1009E+00 .531 .2270E+00
*#-----
*# ROUTING RESULTS          AREA QPEAK TPEAK R.V.
*# (ha) (cms) (hrs) (mm)
*# INFLOW >01: (201 ) 4.10 .710 6.000 41.242
*# OUTFLOW<02: (201-SW) 4.10 .138 6.217 41.243
*# OVERFLOW<03: (OFL-OR) .00 .000 .000 .000
*#-----
*# TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
*# CUMULATIVE TIME OF OVERFLOWS (hours)= .00
*# PERCENTAGE OF TIME OVERFLOWING (%)= .00

```

```

*#-----
*# PEAK FLOW REDUCTION (Qout/Qin)= 19.486
*# TIME SHIFT OF PEAK FLOW (min)= 13.00
*# MAXIMUM STORAGE USED (ha.m.)=.7958E-01

```

```

005:0006-----
*#-----
005:0002-----
*#-----
*# ** END OF RUN : 9

```

```

*# START Project dir.: T:\PROJECTS\13084\SWM\SWMHYMO\
*# Rainfall dir.: T:\PROJECTS\13084\SWM\SWMHYMO\
*# TZERO = .00 hrs on 0
*# METOUT= 2 (output = METRIC)
*# NRUN = 010
*# NSTORM= 1
*# # 1=MILSCS12.010

```

```

010:0002-----
*#-----
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : JUNE 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT
*#-----
*#-----

```

```

*# READ STORM          Filename: TOWN OF MILTON 12 HOUR 10 YEAR SCS STORM
*# Ptotal= 71.35 mm   Comments: TOWN OF MILTON 12 HOUR 10 YEAR SCS STORM
*#-----
*# TIME RAIN          TIME RAIN          TIME RAIN          TIME RAIN
*# hrs mm/hr         hrs mm/hr         hrs mm/hr         hrs mm/hr
*# .20 1.410         3.20 2.820         6.20 17.270       9.20 2.820
*# .40 1.410         3.40 2.820         6.40 10.220       9.40 2.820
*# .60 1.410         3.60 2.820         6.60 7.400        9.60 2.820
*# .80 1.410         3.80 2.820         6.80 7.050        9.80 2.820
*# 1.00 1.410        4.00 2.820        7.00 4.940        10.00 2.820
*# 1.20 1.410        4.20 4.940        7.20 4.230        10.20 1.410
*# 1.40 1.410        4.40 4.940        7.40 4.230        10.40 1.410
*# 1.60 1.410        4.60 4.940        7.60 4.230        10.60 1.410
*# 1.80 1.410        4.80 4.940        7.80 4.230        10.80 1.410
*# 2.00 1.410        5.00 4.940        8.00 4.230        11.00 1.410
*# 2.20 2.820        5.20 6.350        8.20 2.820        11.20 1.410
*# 2.40 2.820        5.40 9.170        8.40 2.820        11.40 1.410
*# 2.60 2.820        5.60 21.150       8.60 2.820        11.60 1.410
*# 2.80 2.820        5.80 46.180       8.80 2.820        11.80 1.410
*# 3.00 2.820        6.00 96.590       9.00 2.820        12.00 1.410

```

```

010:0003-----
*#-----
*# PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#-----
*#-----
*# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC)
*#-----

```

```

*# CALIB NASHYD          Area (ha)= 4.10 Curve Number (CN)=86.00
*# 01:101 DT= 1.00     Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
*# U.H. Tp(hrs)= .280
*#-----
*# Unit Hyd Qpeak (cms)= .559
*# PEAK FLOW (cms)= .403 (i)
*# TIME TO PEAK (hrs)= 6.183
*# RUNOFF VOLUME (mm)= 40.880
*# TOTAL RAINFALL (mm)= 71.354
*# RUNOFF COEFFICIENT = .573
*# (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

010:0004-----
*#-----
*# POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#-----
*#-----
*# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4
*#-----

```

```

*# CALIB STANDHYD          Area (ha)= 4.10

```

| 01:201 DT= 1.00 | Total Imp(%)= 36.00 Dir. Conn.(%)= 36.00

Table with columns: IMPERVIOUS, PERVIOUS (i), and *TOTALS*. Rows include Surface Area, Dep. Storage, Average Slope, Length, Mannings n, Max. eff. Inten., Storage Coeff., Unit Hyd. Tpeak, Unit Hyd. peak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, and RUNOFF COEFFICIENT.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 86.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0005
*#
*# ROUTE CATCHMENT 201 THROUGH DDUAL STAGE ORIFICE DEVICE
*#
*# POST DEVELOPEMENT FLOWS FROM CATCHMENT 201
*#

ROUTE RESERVOIR Requested routing time step = 1.0 min.
Table with columns: OUTFLOW STORAGE, OUTFLOW STORAGE. Rows include values for (cms) and (ha.m.) with a warning about zero values.

ROUTING RESULTS
Table with columns: AREA, QPEAK, TPEAK, R.V. Rows include INFLOW >01: (201), OUTFLOW <02: (201-SW), and OVERFLOW <03: (OFL-OR).

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours) = .00
PERCENTAGE OF TIME OVERFLOWING (%) = .00

PEAK FLOW REDUCTION [Qout/Qin](%) = 18.444
TIME SHIFT OF PEAK FLOW (min) = 13.00
MAXIMUM STORAGE USED (ha.m.) = .1011E+00

010:0006
*#

010:0002
*#

010:0002
*#

** END OF RUN : 24

START Project dir.: T:\PROJECTS\13084\SWM\SWMHYMO\
Rainfall dir.: T:\PROJECTS\13084\SWM\SWMHYMO\
TZERO = .00 hrs on
METOUT= 2 (output = METRIC)
NRUN = 025
NSTORM= 1
1=MILSCS12.025

025:0002
*#
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : JUNE 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT
*#

025:0002
*#
*# READ STORM Ptotal= 85.71 mm
*# Filename: TOWN OF MILTON 12 HOUR 25 YEAR SCS STORM
*# Comments: TOWN OF MILTON 12 HOUR 25 YEAR SCS STORM

Table with columns: TIME, RAIN. Rows include values for hrs mm/hr and TIME RAIN for various durations.

Table with columns: IMPERVIOUS, PERVIOUS (i). Rows include values for Surface Area, Dep. Storage, Average Slope, Length, Mannings n, Max. eff. Inten., Storage Coeff., Unit Hyd. Tpeak, Unit Hyd. peak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, and RUNOFF COEFFICIENT.

025:0003
*#
*# PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#
*# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC)
*#

CALIB NASHYD Area (ha)= 4.10 Curve Number (CN)=86.0
01:101 DT= 1.00 Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .280

Unit Hyd Qpeak (cms)= .559
PEAK FLOW (cms)= .526 (i)
TIME TO PEAK (hrs)= 6.183
RUNOFF VOLUME (mm)= 53.365
TOTAL RAINFALL (mm)= 85.706
RUNOFF COEFFICIENT = .623

- (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0004
*#
*# POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#
*# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4
*#

CALIB STANDHYD Area (ha)= 4.10
01:201 DT= 1.00 Total Imp(%)= 36.00 Dir. Conn.(%)= 36.00

Table with columns: IMPERVIOUS, PERVIOUS (i). Rows include Surface Area, Dep. Storage, Average Slope, Length, Mannings n, Max. eff. Inten., Storage Coeff., Unit Hyd. Tpeak, Unit Hyd. peak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, and RUNOFF COEFFICIENT.

PEAK FLOW (cms)= .48 .65 *TOTALS* 1.124 (iii)
TIME TO PEAK (hrs)= 6.00 6.00 6.000
RUNOFF VOLUME (mm)= 84.71 53.36 64.648
TOTAL RAINFALL (mm)= 85.71 85.71 85.706
RUNOFF COEFFICIENT = .99 .62 .754

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN* = 86.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0005
*#
*# ROUTE CATCHMENT 201 THROUGH DDUAL STAGE ORIFICE DEVICE
*#
*# POST DEVELOPEMENT FLOWS FROM CATCHMENT 201
*#

ROUTE RESERVOIR Requested routing time step = 1.0 min.
Table with columns: OUTFLOW STORAGE, OUTFLOW STORAGE. Rows include values for (cms) and (ha.m.) with a warning about zero values.

ROUTING RESULTS
Table with columns: AREA, QPEAK, TPEAK, R.V. Rows include INFLOW >01: (201), OUTFLOW <02: (201-SW), and OVERFLOW <03: (OFL-OR).

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours) = .00
PERCENTAGE OF TIME OVERFLOWING (%) = .00

PEAK FLOW REDUCTION [Qout/Qin](%) = 17.107
TIME SHIFT OF PEAK FLOW (min) = 13.00
MAXIMUM STORAGE USED (ha.m.) = .1294E+00

025:0006
*#

025:0002
*#

025:0002
*#


```

*
025:0002
*
** END OF RUN : 49
*****
| START | Project dir.: T:\PROJECTS\13084\SWM\SWMHYM\
| Rainfall dir.: T:\PROJECTS\13084\SWM\SWMHYM\
TZERO = .00 hrs on
METOUT= 2 (output = METRIC)
NRUN = 050
NSTORM= 1
# 1=MILSCS12.050

```

```

050:0002
*
Project Name: HOLY FAMILY CATHOLIC CEMETERY
2523 LOWER BASE LINE, MILTON, ONTARIO
JOB NUMBER : 13084
Date : MARCH 2021
Revised : JUNE 2022
Company : S. LLEWELLYN & ASSOCIATES LIMITED
File : 13084.DAT

```

```

050:0002
*
READ STORM | Filename: TOWN OF MILTON 12 HOUR 50 YEAR SCS STORM
Ptotal= 96.33 mm | Comments: TOWN OF MILTON 12 HOUR 50 YEAR SCS STORM

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.20	1.900	3.20	3.810	6.20	23.320	9.20	3.810
.40	1.900	3.40	3.810	6.40	13.800	9.40	3.810
.60	1.900	3.60	3.810	6.60	10.000	9.60	3.810
.80	1.900	3.80	3.810	6.80	9.520	9.80	3.810
1.00	1.900	4.00	3.810	7.00	6.660	10.00	3.810
1.20	1.900	4.20	6.660	7.20	5.710	10.20	1.900
1.40	1.900	4.40	6.660	7.40	5.710	10.40	1.900
1.60	1.900	4.60	6.660	7.60	5.710	10.60	1.900
1.80	1.900	4.80	6.660	7.80	5.710	10.80	1.900
2.00	1.900	5.00	6.660	8.00	5.710	11.00	1.900
2.20	3.810	5.20	8.570	8.20	3.810	11.20	1.900
2.40	3.810	5.40	12.380	8.40	3.810	11.40	1.900
2.60	3.810	5.60	28.560	8.60	3.810	11.60	1.900
2.80	3.810	5.80	62.360	8.80	3.810	11.80	1.900
3.00	3.810	6.00	130.420	9.00	3.810	12.00	1.900

```

050:0003
*
PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*****
# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC)
*
CALIB NASHYD | Area (ha)= 4.10 | Curve Number (CN)=86.00
01:101 DT= 1.00 | Ia (mm)= 5.000 | # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .280
Unit Hyd Qpeak (cms)= .559
PEAK FLOW (cms)= .619 (i)
TIME TO PEAK (hrs)= 6.183
RUNOFF VOLUME (mm)= 62.866
TOTAL RAINFALL (mm)= 96.328
RUNOFF COEFFICIENT = .653
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

050:0004
*
POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*****
# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4
*
CALIB STANDHYD | Area (ha)= 4.10
01:201 DT= 1.00 | Total Imp(%)= 36.00 | Dir. Conn.(%)= 36.00

```

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)	1.48	2.62
Dep. Storage (mm)	1.00	5.00
Average Slope (%)	1.00	2.00
Length (m)	15.00	5.00
Mannings n	.015	.250
Max. eff. Inten. (mm/hr)	130.42	107.93
over (min)	1.00	3.00
Storage Coeff. (min)	.80 (ii)	2.77 (ii)
Unit Hyd. Tpeak (min)	1.00	3.00
Unit Hyd. peak (cms)	1.21	.40

```

*TOTALS*
PEAK FLOW (cms)= .53 | .76 | 1.293 (iii)
TIME TO PEAK (hrs)= 6.00 | 6.00 | 6.000
RUNOFF VOLUME (mm)= 95.33 | 62.86 | 74.552
TOTAL RAINFALL (mm)= 96.33 | 96.33 | 96.328
RUNOFF COEFFICIENT = .99 | .65 | .774
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 86.0 Ia = Dep. Storage (Above)

```

```

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0005
*
ROUTE CATCHMENT 201 THROUGH DDUAL STAGE ORIFICE DEVICE
*
*****
# POST DEVELOPMENT FLOWS FROM CATCHMENT 201
#
ROUTE RESERVOIR | Requested routing time step = 1.0 min.
IN>01:(201 )
OUT<02:(201-SW)
*****
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
*** WARNING: First OUTFLOW value in table should be ZERO.
.003 .0000E+00 | .184 .1200E+00
.022 .1520E-01 | .201 .1400E+00
.051 .3100E-01 | .217 .1606E+00
.085 .4750E-01 | .232 .1820E+00
.117 .6460E-01 | .239 .1930E+00
.142 .8240E-01 | .299 .2041E+00
.165 .1009E+00 | .531 .2270E+00
ROUTING RESULTS | AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >01: (201 ) 4.10 1.293 6.000 74.552
OUTFLOW<02: (201-SW) 4.10 .210 6.217 74.552
OVERFLOW<03: (OFL-OR) .00 .000 .000 .000
TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00
PEAK FLOW REDUCTION [Qout/Qin](%)= 16.235
TIME SHIFT OF PEAK FLOW (min)= 13.00
MAXIMUM STORAGE USED (ha.m.)=.1510E+00

```

```

050:0006
*
050:0002
*
050:0002
*
050:0002
*
050:0002
*
** END OF RUN : 99

```

```

| START | Project dir.: T:\PROJECTS\13084\SWM\SWMHYM\
| Rainfall dir.: T:\PROJECTS\13084\SWM\SWMHYM\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 100
NSTORM= 1
# 1=MILSCS12.100
100:0002
*
Project Name: HOLY FAMILY CATHOLIC CEMETERY
2523 LOWER BASE LINE, MILTON, ONTARIO
JOB NUMBER : 13084
Date : MARCH 2021
Revised : JUNE 2022
Company : S. LLEWELLYN & ASSOCIATES LIMITED
File : 13084.DAT

```

```

100:0002
*
READ STORM | Filename: TOWN OF MILTON 12 HOUR 100 YEAR SCS STOR
Ptotal= 106.96 mm | Comments: TOWN OF MILTON 12 HOUR 100 YEAR SCS STOR

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.20	2.110	3.20	4.230	6.20	25.900	9.20	4.230
.40	2.110	3.40	4.230	6.40	15.330	9.40	4.230
.60	2.110	3.60	4.230	6.60	11.100	9.60	4.230
.80	2.110	3.80	4.230	6.80	10.570	9.80	4.230
1.00	2.110	4.00	4.230	7.00	7.400	10.00	4.230
1.20	2.110	4.20	7.400	7.20	6.340	10.20	2.110
1.40	2.110	4.40	7.400	7.40	6.340	10.40	2.110
1.60	2.110	4.60	7.400	7.60	6.340	10.60	2.110
1.80	2.110	4.80	7.400	7.80	6.340	10.80	2.110
2.00	2.110	5.00	7.400	8.00	6.340	11.00	2.110
2.20	4.230	5.20	9.510	8.20	4.230	11.20	2.110
2.40	4.230	5.40	13.740	8.40	4.230	11.40	2.110
2.60	4.230	5.60	31.710	8.60	4.230	11.60	2.110
2.80	4.230	5.80	69.230	8.80	4.230	11.80	2.110
3.00	4.230	6.00	144.810	9.00	4.230	12.00	2.110

```

100:0003
*
PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*****

```

```

*****
*# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC
*
| CALIB NASHYD | Area (ha)= 4.10 Curve Number (CN)=86.00
| 01:101 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .280

```

```

Unit Hyd Qpeak (cms)= .559

PEAK FLOW (cms)= .713 (i)
TIME TO PEAK (hrs)= 6.167
RUNOFF VOLUME (mm)= 72.542
TOTAL RAINFALL (mm)= 106.961
RUNOFF COEFFICIENT = .678

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
100:0004-----
*#
*# POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#
*#
*#
*# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4
*

```

```

| CALIB STANDHYD | Area (ha)= 4.10
| 01:201 DT= 1.00 | Total Imp(%)= 36.00 Dir. Conn.(%)= 36.00
|-----|

```

```

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 1.48 2.62
Dep. Storage (mm)= 1.00 5.00
Average Slope (%)= 1.00 2.00
Length (m)= 15.00 5.00
Mannings n = .015 .250

Max. eff. Inten. (mm/hr)= 144.81 123.00
over (min) 1.00 3.00
Storage Coeff. (min)= .77 (ii) 2.63 (ii)
Unit Hyd. Tpeak (min)= 1.00 3.00
Unit Hyd. peak (cms)= 1.24 .41

PEAK FLOW (cms)= .59 .87 *TOTALS*
TIME TO PEAK (hrs)= 6.00 6.00 1.463 (iii)
RUNOFF VOLUME (mm)= 105.96 72.54 84.573
TOTAL RAINFALL (mm)= 106.96 106.96 106.961
RUNOFF COEFFICIENT = .99 .68 .791

```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 86.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
100:0005-----
*#
*# ROUTE CATCHMENT 201 THROUGH DDUAL STAGE ORIPICE DEVICE
*#
*# POST DEVELOPEMENT FLOWS FROM CATCHMENT 201
*#

```

```

| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>01:(201 ) |
| OUT<02:(201-SW) |

```

```

***** OUTFLOW STORAGE TABLE *****
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
*** WARNING: First OUTFLOW value in table should be ZERO.
.003 .0000E+00 | .184 .1200E+00
.022 .1520E-01 | .201 .1400E+00
.051 .3100E-01 | .217 .1606E+00
.085 .4750E-01 | .232 .1820E+00
.117 .6460E-01 | .239 .1930E+00
.142 .8240E-01 | .299 .2041E+00
.165 .1009E+00 | .531 .2270E+00

```

```

ROUTING RESULTS AREA QPEAK TPEAK R.V.
----- (ha) (cms) (hrs) (mm)
INFLOW >01: (201 ) 4.10 1.463 6.000 84.573
OUTFLOW<02: (201-SW) 4.10 .226 6.233 84.574
OVERFLOW<03: (OFL-OR) .00 .000 .000 .000

```

```

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

```

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 15.450
TIME SHIFT OF PEAK FLOW (min)= 14.00
MAXIMUM STORAGE USED (ha.m.)=.1732E+00

```

```

-----
100:0006-----
*
-----
100:0002-----
*
-----
100:0002-----
*
-----
100:0002-----
*
-----
100:0002-----
*
-----
100:0002-----
*
-----
100:0002-----
*

```

FINISH

```

*****
WARNINGS / ERRORS / NOTES
-----
002:0005 ROUTE RESERVOIR
*** WARNING: First OUTFLOW value in table should be ZERO.

```

```

*** WARNING: First OUTFLOW value in table should be ZERO.
*** WARNING: First OUTFLOW value in table should be ZERO.
*** WARNING: First OUTFLOW value in table should be ZERO.
*** WARNING: First OUTFLOW value in table should be ZERO.
*** WARNING: First OUTFLOW value in table should be ZERO.
Simulation ended on 2022-06-28 at 17:43:21

```

```

2 Metric units
*#-----|
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : June 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT
*#-----|
*#
*#
*#
START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
HAZEL.STM
*
READ STORM STORM_FILENAME "STORM.001"
*
*#-----|
*#
*# PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*# -----
*#
*# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC
*#
CALIB NASHYD ID=[1], NHYD=["101"], DT=[1]min, AREA=[4.1]ha,
DWP=[0]cms, CN/C=[94], IA=[5.00]mm,
N=[3], TP=[0.28]hrs,
RAINFALL=[ , , , ](mm/hr), END=-1
*#-----|
*#
*# POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*# -----
*#
*# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4
*#
CALIB STANDHYD ID=[1], NHYD=["201"], DT=[1]min, AREA=[4.1]ha,
XIMP=[0.36], TIMP=[0.36], DWP=[0]cms, LOSS=[2],
SCS curve number CN=[94],
Pervious surfaces: IAPer=[5.00]mm, SLPP=[2.0]%,
LGP=[5.0]m, MNP=[0.250], SCP=[0]min
Impervious surfaces: IAImp=[1.0]mm, SLPI=[1.0]%,
LGI=[15]m, MNI=[0.015], SCI=[0]min,
RAINFALL=[ , , , ](mm/hr), END=-1
*#-----|
*#
*# ROUTE CATCHMENT 201 THROUGH DUAL STAGE ORIFICE
*# -----
*# POST DEVELOPEMENT FLOWS FROM CATCHMENT 201
*#-----|
*#
ROUTE RESERVOIR IDout=[2], NHYD=["201-SWM"], IDin=[1],
RDT=[1]min,
TABLE of ( OUTFLOW-STORAGE ) values
(cms) - (ha-m)
0.0033 0
0.0216 0.01520
0.0512 0.03100
0.0854 0.04750
0.1169 0.06460
0.1424 0.08240
0.1650 0.10090
0.1841 0.12000
0.2014 0.14000
0.2174 0.16060
0.2322 0.18200
0.2393 0.19300
0.2985 0.20410
0.5311 0.22700
-1 -1 (max twenty pts)
IDovf=[3], NHYDovf=["OPL-ORP"]
*#-----|
ADD HYD IDsum=[4], NHYD=[201+ORP], IDs to add=[2, 3]
*#-----|
*
FINISH

```

```

SSSSS W W M M H H Y Y M M OOO 999 999 =====
S W W W MM MM H H Y Y M M O O 9 9 9 9
SSSSS W W M M M H H H H Y M M O O ## 9 9 9 9 Ver 4.05
S W W M M H H Y M M O O 9999 9999 Sept 2011
SSSSS W W M M H H Y M M OOO 9 9 9 9 =====
StormWater Management Hydrologic Model 999 999 =====

```

```

***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhym@jfsa.Com *****

```

```

+++++++ Licensed user: S. Llewellyn & Associates Ltd ++++++
+++++++ Burlington SERIAL#:3902680 ++++++

```

```

+++++ PROGRAM ARRAY DIMENSIONS +++++
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****

```

```

***** DETAILED OUTPUT *****
* DATE: 2022-06-28 TIME: 18:00:31 RUN COUNTER: 000744 *
* Input filename: T:\PROJECTS\13084\SWM\SWMHYMO\13084HAZ.dat *
* Output filename: T:\PROJECTS\13084\SWM\SWMHYMO\13084HAZ.out *
* Summary filename: T:\PROJECTS\13084\SWM\SWMHYMO\13084HAZ.sum *
* User comments:
* 1:
* 2:
* 3:

```

```

001:0001-----
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : June 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT
*#
*#
** END OF RUN : 1

```

```

| START | Project dir.: T:\PROJECTS\13084\SWM\SWMHYMO\
| | Rainfall dir.: T:\PROJECTS\13084\SWM\SWMHYMO\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 002
NSTORM= 1
# 1=HAZEL.STM

```

```

002:0002-----
*# Project Name: HOLY FAMILY CATHOLIC CEMETERY
*# 2523 LOWER BASE LINE, MILTON, ONTARIO
*# JOB NUMBER : 13084
*# Date : MARCH 2021
*# Revised : June 2022
*# Company : S. LLEWELLYN & ASSOCIATES LIMITED
*# File : 13084.DAT
*#
*#

```

```

002:0002-----
| READ STORM | Filename: Regional storm event (Hurricane Hazel)
| Ptotal= 212.00 mm | Comments: Regional storm event (Hurricane Hazel)

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
1.00	6.360	4.00	12.720	7.00	23.320	10.00	53.000
2.00	4.240	5.00	16.960	8.00	12.720	11.00	38.160
3.00	6.360	6.00	12.720	9.00	12.720	12.00	12.720

```

002:0003-----
*#
*# PRE-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#
*#
*# CATCHMENT 101 - PRE DEVELOPMENT DISCHARGE TO EXISTING WATERCOURSE (HYDROLOGIC)

```

```

| CALIB NASHYD | Area (ha)= 4.10 Curve Number (CN)=94.00
| 01:101 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
| | U.H. Tp(hrs)= .280

```

```

Unit Hyd Qpeak (cms)= .559
PEAK FLOW (cms)= .587 (i)
TIME TO PEAK (hrs)= 10.050
RUNOFF VOLUME (mm)= 191.965
TOTAL RAINFALL (mm)= 212.000
RUNOFF COEFFICIENT = .905
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

002:0004-----
*# POST-DEVELOPMENT CONDITIONS HYDROLOGIC MODELING
*#
*# CATCHMENT 201 - CONTROLLED DISCHARGE TO WATERCOURSE SMT-4

```

CALIB STANDHYD	Area (ha)	Total Imp(%)	Dir. Conn.(%)
01:201 DT= 1.00	4.10	36.00	36.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)	1.48	2.62
Dep. Storage (mm)	1.00	5.00
Average Slope (%)	1.00	2.00
Length (m)	15.00	5.00
Mannings n	.015	.250

Max. eff. Inten. (mm/hr)	53.00	52.52
over (min)	1.00	4.00
Storage Coeff. (min)	1.15 (ii)	3.77 (ii)
Unit Hyd. Tpeak (min)	1.00	4.00
Unit Hyd. peak (cms)	.99	.29

PEAK FLOW (cms)	.22	.38	*TOTALS*
TIME TO PEAK (hrs)	9.32	10.00	10.000
RUNOFF VOLUME (mm)	211.00	191.96	198.818
TOTAL RAINFALL (mm)	212.00	212.00	212.000
RUNOFF COEFFICIENT	1.00	.91	.938

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 94.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0005-----
*# ROUTE CATCHMENT 201 THROUGH DUAL STAGE ORIFICE
*# POST DEVELOPMENT FLOWS FROM CATCHMENT 201

```

```

| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>01: (201 ) |
| OUT<02: (201-SW) |

```

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.003	.0000E+00	.184	.1200E+00
.022	.1520E-01	.201	.1400E+00
.051	.3100E-01	.217	.1606E+00
.085	.4750E-01	.232	.1820E+00
.117	.6460E-01	.239	.1930E+00
.142	.8240E-01	.299	.2041E+00
.165	.1009E+00	.531	.2270E+00

ROUTING RESULTS	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW >01: (201)	4.10	.600	10.000	198.818
OUTFLOW<02: (201-SW)	4.10	.454	10.133	198.820
OVERFLOW<03: (OPL-OR)	.00	.000	.000	.000

```

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

```

PEAK FLOW REDUCTION [Qout/Qin](%)	75.600
TIME SHIFT OF PEAK FLOW (min)	8.00
MAXIMUM STORAGE USED (ha.m.)	.2194E+00

```

002:0006-----
| ADD HYD ( 201) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| | (ha) (cms) (hrs) (mm) (cms)
ID1 02:201-SWM 4.10 .454 10.13 198.82 .000
+ID2 03:OPL-ORF .00 .000 .00 .00 .000
SUM 04: 201 4.10 .454 10.13 198.82 .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

002:0007-----
*# FINISH
*# WARNINGS / ERRORS / NOTES
002:0005 ROUTE RESERVOIR
*** WARNING: First OUTFLOW value in table should be ZERO.
Simulation ended on 2022-06-28 at 18:00:31

```

APPENDIX D

QUALITY CONTROL INFORMATION



Hydroworks Sizing Summary

Holy Family Cemetery Crematorium

03-31-2021

Recommended Size: HS 10

A HydroStorm HS 10 is recommended to provide 80 % annual TSS removal based on a drainage area of 1.69 (ha) with an imperviousness of 30.3 % and Hamilton RBG, Ontario rainfall for the ETV Canada particle size distribution.

The recommended HydroStorm HS 10 treats 96 % of the annual runoff and provides 85 % annual TSS removal for the Hamilton RBG rainfall records and ETV Canada particle size distribution.

The HydroStorm has a headloss coefficient (K) of 1.04. Since a peak flow was not specified, headloss was calculated using the full pipe flow of .1 (m³/s) for the given 300 (mm) pipe diameter at 1% slope. The headloss was calculated to be 99 (mm) based on a flow depth of 300 (mm) (full pipe flow).

This summary report provides the main parameters that were used for sizing. These parameters are shown on the summary tables and graphs provided in this report.

If you have any questions regarding this sizing summary please do not hesitate to contact Hydroworks at 888-290-7900 or email us at support@hydroworks.com.

The sizing program is for sizing purposes only and does not address any site specific parameters such as hydraulic gradeline, tailwater submergence, groundwater, soils bearing capacity, etc. Headloss calculations are not a hydraulic gradeline calculation since this requires a starting water level and an analysis of the entire system downstream of the HydroStorm . Design liability is only valid for lawsuits brought within the United States where Hydroworks has its corporate headquarters.

TSS Removal Sizing Summary

Hydroworks Hydrodynamic Separator Sizing Program - HydroStorm

File Product Units View Help

General | Dimensions | Rainfall | Site | TSS PSD | TSS Loading | Quantity Storage | By-Pass | Custom | CAD | Other

Site Parameters: Area (ha) 1.69, Imperviousness (%) 30.3

Units: U.S., Metric

Rainfall Station: Hamilton RBG, Ontario, 2004 to 2013, Rainfall Timestep = 15 min.

Project Title (2 lines): Holy Family Cemetery Crematorium

Inlet Pipe: Diam. (mm) 300, Slope (%) 1, Peak Design Flow (m3/s)

Stokes Cheng Lab Results-Linear Lab Results-Exponential

Annual TSS Removal Results					Particle Size Distribution		
Model #	Qlow (m3/s)	Qtot (m3/s)	Flow Capture (%)	TSS Removal (%)	Size (um)	%	SG
HS 4	.03	.1	90 %	60 %	2	5	2.65
HS 5	.05	.1	94 %	67 %	5	5	2.65
HS 6	.07	.1	95 %	73 %	8	10	2.65
Unavailable	.09	.1	95 %	76 %	20	15	2.65
HS 8	.1	.1	96 %	79 %	50	10	2.65
Unavailable	.1	.1	96 %	82 %	75	5	2.65
HS 10	.1	.1	96 %	85 %	100	10	2.65
HS 12	.1	.1	96 %	89 %	150	15	2.65
					250	15	2.65
					500	5	2.65

Note: Results vary significantly based on particle size distribution

Simulate

TSS Particle Size Distribution

Hydroworks Hydrodynamic Separator Sizing Program - HydroStorm

File Product Units View Help

General | Dimensions | Rainfall | Site | TSS PSD | TSS Loading | Quantity Storage | By-Pass | Custom | CAD | Other

TSS Particle Size Distribution

Size (um)	%	SG
2	5	2.65
5	5	2.65
8	10	2.65
20	15	2.65
50	10	2.65
75	5	2.65
100	10	2.65
150	15	2.65
250	15	2.65
500	5	2.65
1000	5	2.65
*		

Notes:

- To change data just click a cell and type in the new value(s)
- To add a row just go to the bottom of the table and start typing.
- To delete a row, select the row by clicking on the first pointer column, then press delete
- To sort the table click on one of the column headings

TSS Distributions

ETV Canada

OK110

Toronto

Ontario (1994)

Calgary Forebay

F95 Sand

NURP (1983)

Kitchener

User Defined

Clear

TSS Removal Required (%) 80

Water Temp (C) 20

You must select a particle size distribution for TSS to simulate TSS removal

Dimensions And Capacities

Hydroworks Hydrodynamic Separator Sizing Program - HydroStorm

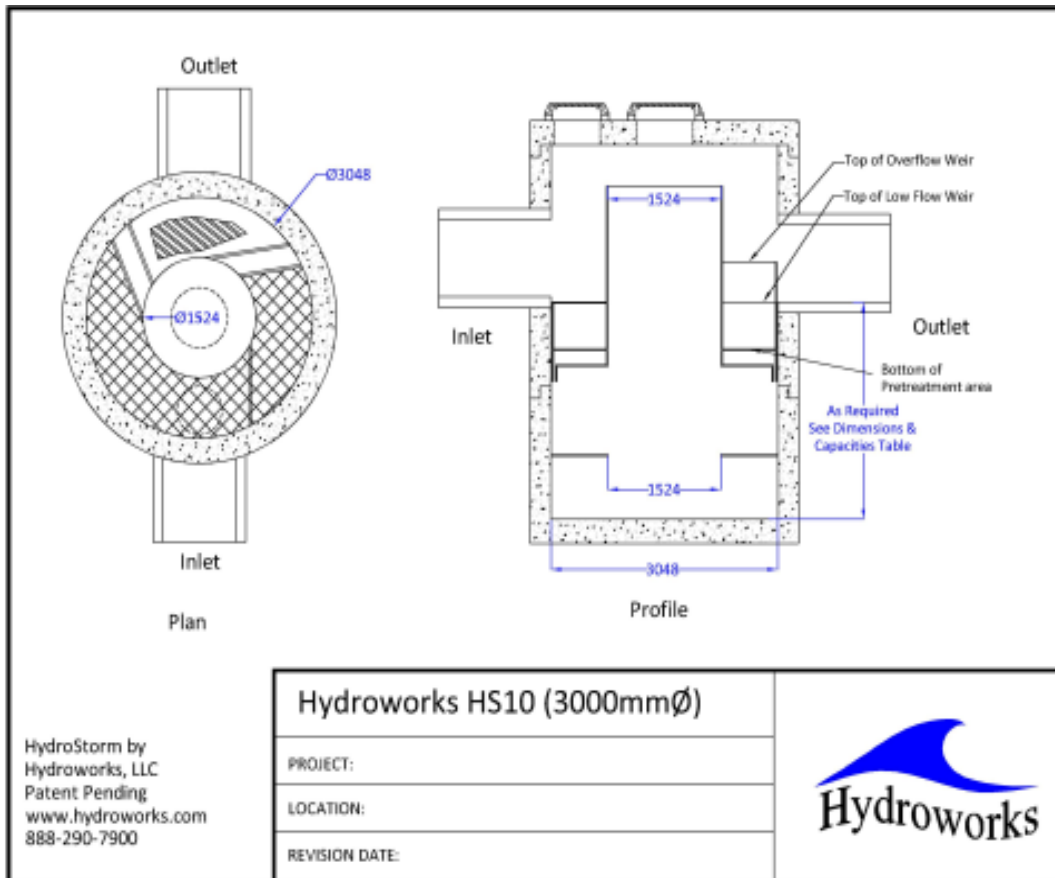
File Product Units View Help

General Dimensions Rainfall Site TSS PSD TSS Loading Quantity Storage By-Pass Custom CAD Other

Dimensions and Capacities					
Model	Diam. (m)	Depth (m)	Float. Vol. (L)	Sediment Vol. (m3)	Total Vol. (m3)
HS 4	1.22	1.22	381	0.9	1.4
HS 5	1.52	1.52	642	1.8	2.8
HS 6	1.83	1.83	1041	3.2	4.8
HS 7	2.13	1.98	1575	4.6	7.1
HS 8	2.44	2.13	2354	6.3	10
HS 9	2.74	2.44	3242	9.3	14.4
HS 10	3.05	2.74	4327	13.2	20
HS 12	3.66	3.35	7164	23.8	35.2

Depth = Depth from outlet invert to inside bottom of tank

Generic HS 10 CAD Drawing



TSS Buildup And Washoff

Hydroworks Hydrodynamic Separator Sizing Program - HydroStorm

File Product Units View Help

General | Dimensions | Rainfall | Site | TSS PSD | TSS Loading | Quantity Storage | By-Pass | Custom | CAD | Other

TSS Buildup

Power Linear
 Exponential
 Michaelis-Menton
 No Buildup Required

TSS Washoff

Power-Exponential
 Rating Curve (no upper limit)
 Rating Curve (limited to buildup)
 Event Mean Concentration

Street Sweeping

Efficiency (%)
 Start Month
 Stop Month
 Frequency (days)
 Available Fraction

Soil Erosion

Add Erosion to TSS

TSS Buildup Parameters

Limit (kg/ha)
 Coeff (kg/ha)
 Exponent

TSS Washoff Parameters

Coefficient
 Exponent

TSS Buildup

Based on Area
 Based on Curb Length

Upstream Quantity Storage

Hydroworks Hydrodynamic Separator Sizing Program - HydroStorm

File Product Units View Help

General | Dimensions | Rainfall | Site | TSS PSD | TSS Loading | Quantity Storage | By-Pass | Custom | CAD | Other

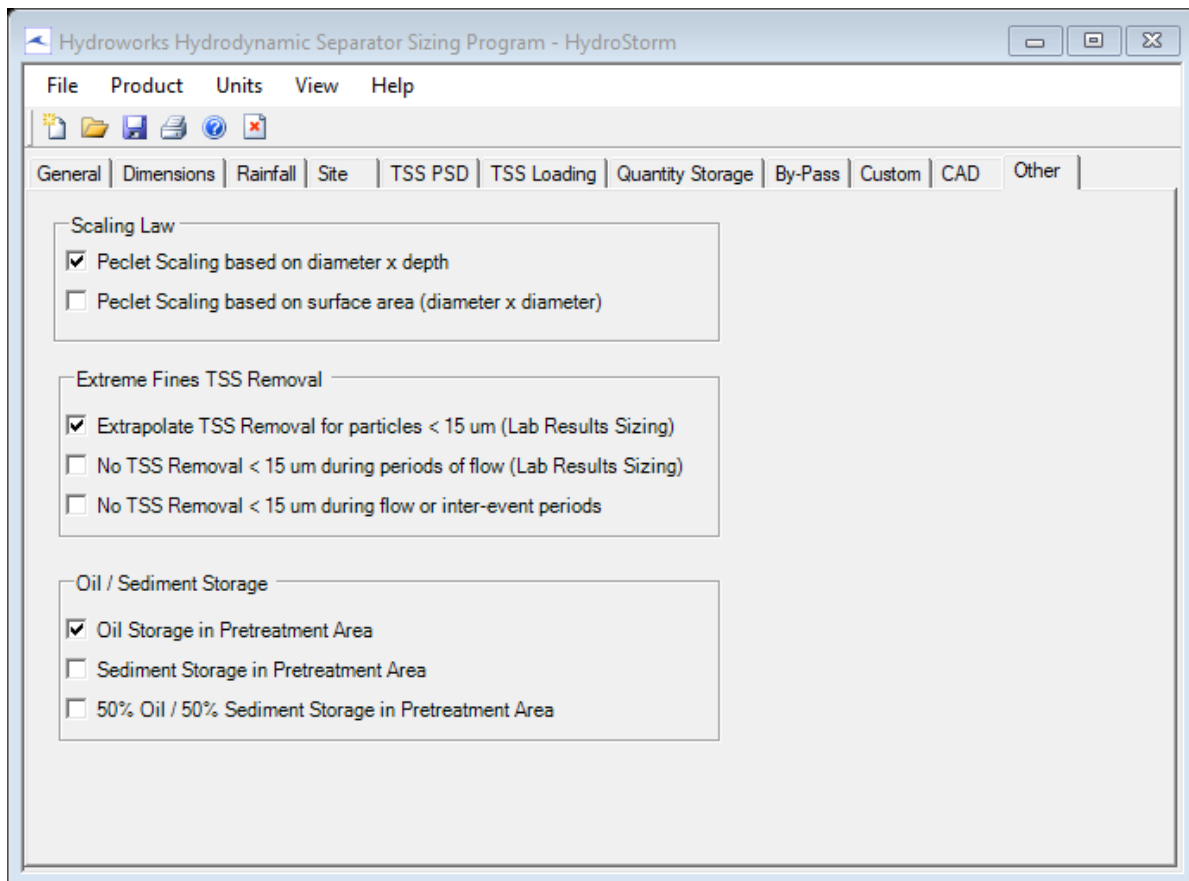
Quantity Control Storage

	Storage (m3)	Discharge (m3/s)
▶	0	0
*		

Notes:

1. To change data just click a cell and type in the new value (s)
2. To add a row just go to the bottom of the table and start typing.
3. To delete a row, select the row by clicking on the first pointer column, then press delete
4. To sort the table click on one of the column headings

Other Parameters



Hydroworks Sizing Program - Version 4.9
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VERIFICATION STATEMENT

GLOBE Performance Solutions

Verifies the performance of

Hydroworks® HydroStorm (HS) Hydrodynamic Separator

Developed by Hydroworks, LLC
Clark, NJ, USA

In accordance with

ISO 14034:2016

Environmental management — Environmental technology verification (ETV)



John D. Wiebe, PhD
Executive Chairman
GLOBE Performance Solutions

May 15, 2018
Vancouver, BC, Canada



Verification Body
GLOBE Performance Solutions
404 – 999 Canada Place | Vancouver, B.C | Canada |V6C 3E2

Technology description and application

The Hydroworks® HydroStorm (HS) Hydrodynamic Separator is a concrete cylindrical device with an annular pre-treatment channel, an inner chamber, and lower collection sump. A schematic of the HS 4 test unit is shown in Figure 1. The pre-treatment channel extends below the outlet pipe invert and contains three intermediate low-flow weirs (flush with the outlet invert), and two downstream higher bypass weirs that extend above the outlet invert. The higher weirs bypass high flows to prevent oil and solids from being scoured out of the separator.

As water enters the unit through one or more inlets, coarser solids immediately start to settle below a horizontal grate extending from the inlet to two sets of lower weirs near the outlet pipe. The grating is positioned over the pre-treatment channel to help displace the inflow turbulence and protect the captured sediment from scour. Openings are located on the horizontal plate upstream of each weir to allow the flow to be conveyed into the inner chamber and lower sump. The weirs are positioned to create a counter clockwise rotation of water in the inner chamber to minimize turbulence and maximize settling. After water spirals down the inner chamber to the main settling chamber towards the floor of the separator where it deposits suspended sediments, it flows upwards between the wall of the unit and the outer edge of the disk extended from the inner chamber and through an arced opening at the bottom of the pre-treatment disk, downstream of the bypass weirs, where it is conveyed into the outlet pipe. An annular secondary horizontal plate with 32% of open-perforations is located within the lower sump to protect the collected sediment from scour. Oil and light liquids enter the inner chamber through the holes, reaching the bottom of the pre-treatment area and rises to the top of the water level where they are trapped.

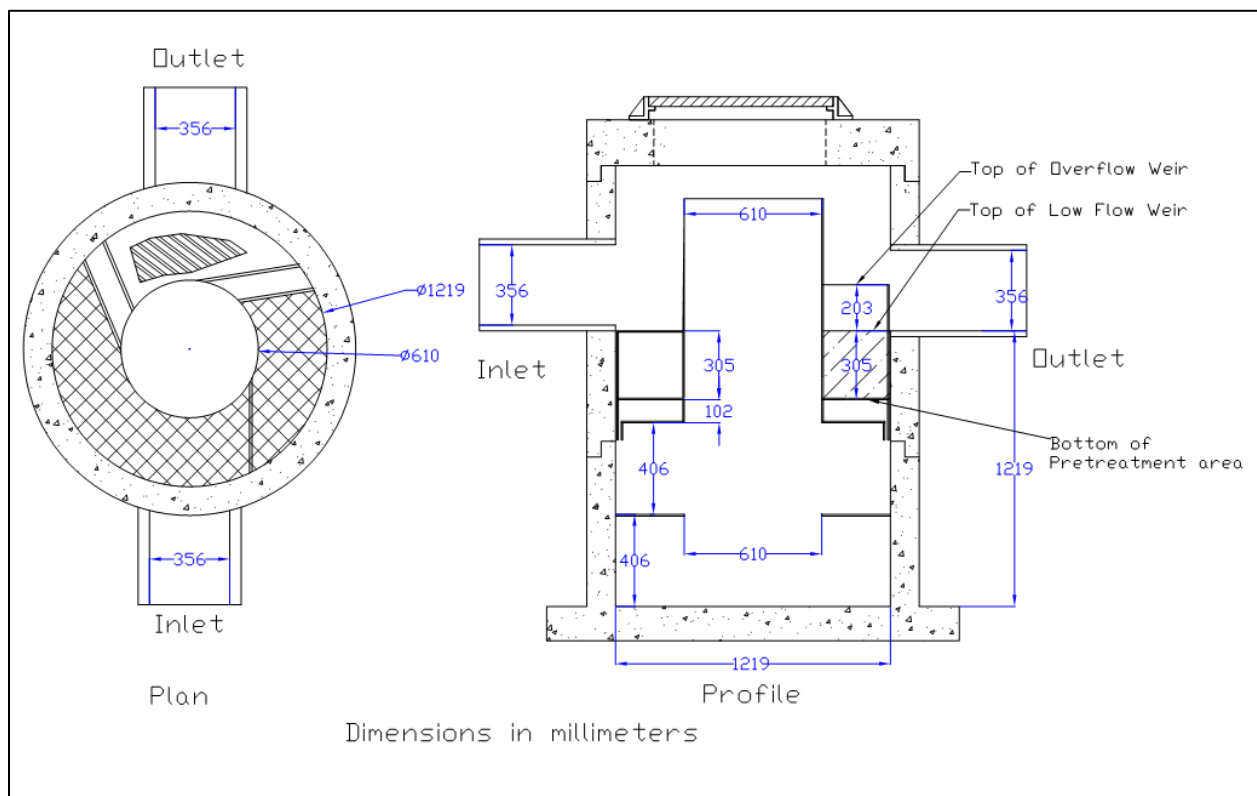


Figure 1: Schematic of the Hydroworks® HS4 Hydrodynamic Separator treatment unit tested as part of this verification.

Performance conditions

The data and results published in this Technology Fact Sheet were obtained from the testing program conducted on the Hydroworks® HS4 Hydrodynamic Separator, in accordance with the *Procedure for Laboratory Testing of Oil-Grit Separators (Version 3.0, June 2014)*. The Procedure was prepared by the Toronto and Region Conservation Authority (TRCA) for the Canadian Environmental Technology Verification Program. A copy of the Procedure may be accessed on the Canadian ETV website at www.etvcanada.ca.

Performance claim(s)

Capture test¹:

During the capture test, the Hydroworks® HS Hydrodynamic Separator, with a false floor set to 50% of the manufacturer's recommended maximum sediment storage depth and a constant influent test sediment concentration of 200 mg/L, removes 69, 64, 60, 56, 46, 41, and 36 percent of influent sediment by mass at surface loading rates of 40, 80, 200, 400, 600, 1000, and 1400 L/min/m², respectively.

Scour test¹:

During the scour test, the Hydroworks® HS Hydrodynamic Separator, with 10.2 cm (4 inches) of test sediment pre-loaded onto a false floor reaching 50% of the manufacturer's recommended maximum sediment sump storage depth and sediment loaded onto the pre-treatment channel emulating depositional pattern of the 40 L/min/m² capture test, generate corrected effluent concentrations of 22.4, 28.5, 20.0, 19.1, and 24.4 mg/L at 5-minute duration surface loading rates of 200, 800, 1400, 2000, and 2600 L/min/m², respectively.

Light liquid re-entrainment test¹:

During the light liquid re-entrainment test, the Hydroworks® HS Hydrodynamic Separator with surrogate low-density polyethylene beads preloaded within the inner chamber, representing a floating light liquid volume equal to a depth of 50.8 mm over the sedimentation area, retains 100, 99.9, 95.4, 95.7, and 97.5 percent of loaded beads by mass during the 5-minute duration surface loading rates of 200, 800, 1400, 2000, and 2600 L/min/m², respectively.

Performance results

The test sediment consisted of ground silica (1 – 1000 micron) with a specific gravity of 2.65, uniformly mixed to meet the particle size distribution specified in the testing procedure. The *Procedure for Laboratory Testing of Oil Grit Separators* requires that the three sample average of the test sediment particle size distribution (PSD) meet the specified PSD percent less than values within a boundary threshold of 6%. The comparison of the average test sediment PSD to the CETV specified PSD in Figure 2 indicates that the test sediment used for the capture and scour tests met this condition.

¹ The claim can be applied to other units smaller or larger than the tested unit as long as the untested units meet the scaling rule specified in the Procedure for Laboratory of Testing of Oil Grit Separators (Version 3.0, June 2014)

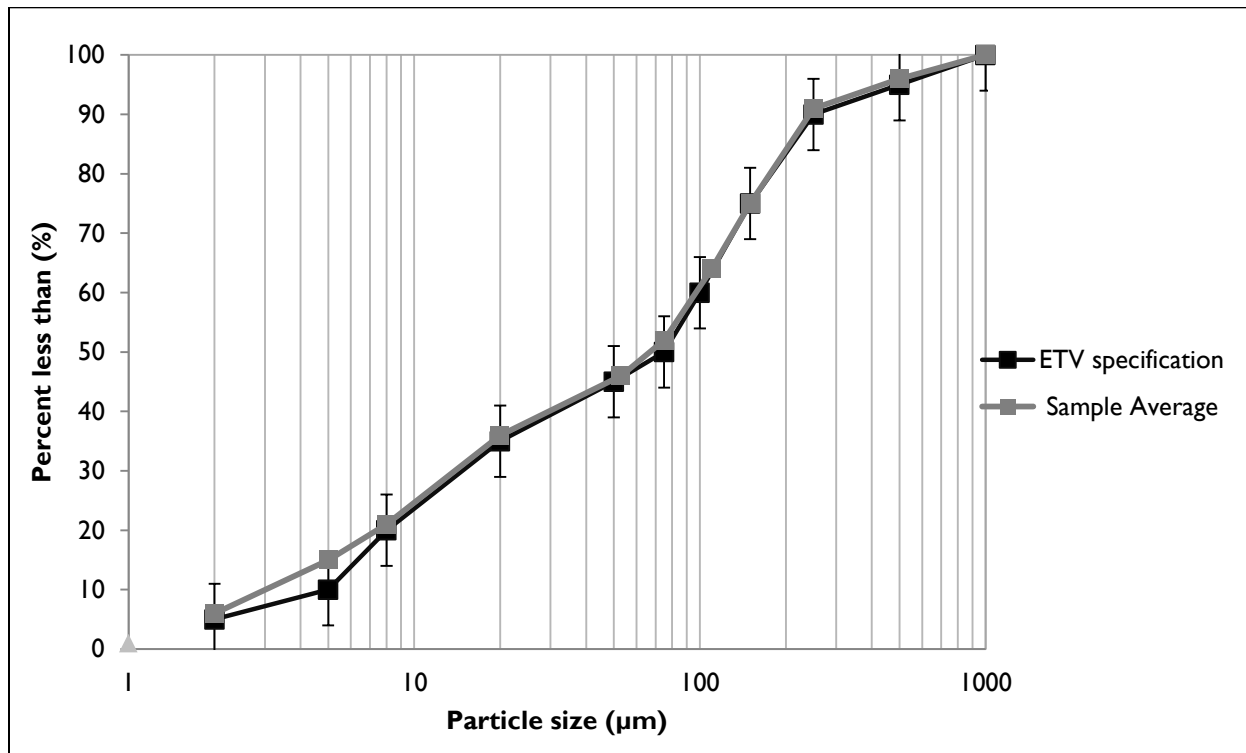


Figure 2. The three sample average particle size distribution (PSD) of the test sediment used for the capture and scour test compared to the specified PSD.

The capacity of the device to retain sediment was determined at seven surface loading rates using the modified mass balance method. This method involved measuring the mass and particle size distribution of the injected and retained sediment for each test run. Performance was evaluated with a false floor at 0.15 m from the bottom, simulating the technology filled to 50% of the manufacturer’s recommended maximum sediment storage depth. The test was carried out with clean water that maintained a sediment concentration below 20 mg/L. Based on these conditions, removal efficiencies for individual particle size classes and for the test sediment as a whole were determined for each of the tested surface loading rates (Table 1).

In some instances, the removal efficiencies were above 100% for certain particle size fractions. These discrepancies are not unique to any one test laboratory and may be attributed to errors relating to the blending of sediment, collection of representative samples for laboratory submission, and laboratory analysis of PSD. Due to these errors, caution should be exercised in applying the removal efficiencies by particle size fraction for the purposes of sizing the tested device (see [Bulletin # CETV 2016-11-0001](#)). The results for “all particle sizes by mass balance” (see Table 1 and 2) are based on measurements of the total injected and retained sediment mass, and are therefore not subject to blending, sampling or PSD analysis errors.

Table I. Removal efficiencies (%) of the HS4 unit at specified surface loading rates.

Particle size fraction (µm)	Surface loading rate (L/min/m ²)						
	40	80	200	400	600	1000	1400
>500	73	100*	98	67	100*	100*	26
250 - 500	100	100*	92	64	100*	98	48
150 - 250	100*	75	89	72	89	60	69
105 - 150	94	100*	100*	100*	78	99	91
75 - 105	96	76	79	95	68	54	46
53 - 75	87	100*	100*	100*	56	69	65
20 - 53	71	54	46	44	19	14	10
8 - 20	38	23	15	8	2	2	2
5 - 8	13	6	1	1	0	0	0
<5	8	0	0	0	0	0	0
All particle sizes by mass balance	68.6	64.0	60.0	56.1	46.1	41.2	35.7

*Removal efficiencies were calculated to be above 100%. Calculated values ranged between 103 and 194% (average 128%). See text and [Bulletin # CETV 2016-11-0001](#) for more information.

Figure 3 compares the particle size distribution (PSD) of the three sample average of the test sediment to the PSD of the sediment retained by the HS4 unit at each of the tested surface loading rates. As expected, the capture efficiency for fine particles in the unit was generally found to decrease as surface loading rates increased.

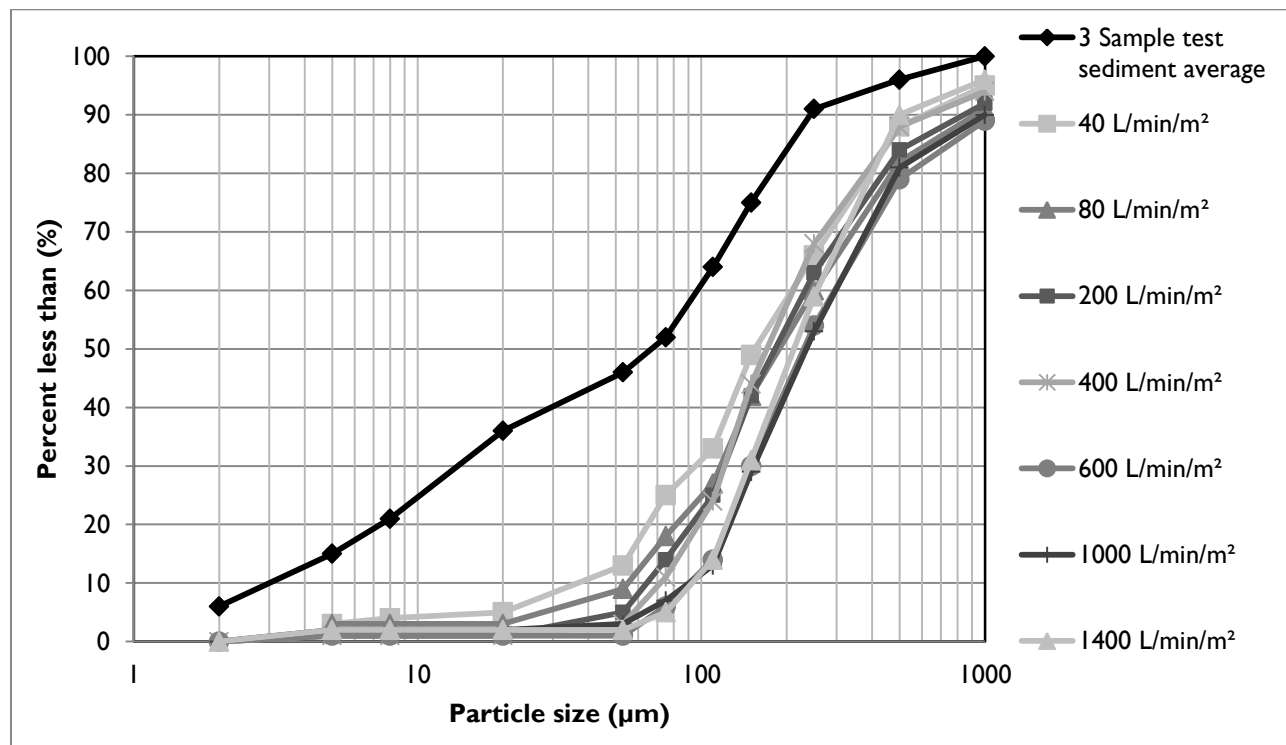


Figure 3. Particle size distribution of sediment retained in the HS4 unit in relation to the injected test sediment average.

For the sediment scour and re-suspension test, two tests were conducted. The first test was conducted with the secondary plate used in the capture tests. The second used a perforated secondary plate. Since sediment during the capture tests was found to settle in the pre-treatment channel, and in roughly the same quantities on the secondary plate and collection sump, all three of these surfaces were preloaded with sediment during the first test. The pre-treatment channel only captures coarse sediment. Therefore, this area was pre-loaded with sediment having a PSD similar to the PSD of the sediment that settled in this area during the 40 L/min/m² SLR sediment capture test. The pre-loaded sediment in the pre-treatment channel was shaped and leveled to correspond with sedimentation patterns and depths observed by the laboratory technician during the 40 L/min/m² SLR capture test. It should be noted that the actual sediment preloaded in this area was finer than the PSD of sediment captured in the same area during the 40 L/min/m² SLR capture test, particularly for particle sizes less than the median size. Both the sump and secondary plate were pre-loaded with the 1-1000 µm sediment mix to a depth of 10.2 cm. The preloaded sediment in the lower sump was placed on a false floor to mimic a device filled to 50% of the manufacturer's maximum recommended sediment storage depth.

After pre-loading the sediment, clean water was run through the device at five SLRs over a 25 minute period. At each SLR, five effluent samples were collected over a four minute interval (one per minute) with the first sample collected at the beginning of each flow rate, and the last collected just prior to the one minute transition to the next flow rate or end of the test. Effluent samples were analyzed for Suspended Sediment Concentration (SSC) and PSD by methods prescribed in the *Procedure*. The effluent samples were subsequently adjusted based on the background concentration of the influent water and the smallest 5% of particles captured during the 40 L/min/m² sediment capture test (7 µm), as per the method described in [Bulletin # CETV 2016-09-0001](#).

Measurements of sediment depths in the sump after the first test showed that most of the sediment from the secondary plate was carried into the lower sump. During this process, the fine sediment was likely re-suspended and carried out of the unit with the flow. The average adjusted effluent suspended sediment concentrations for each SLR ranged from 11.3 mg/L at the 200 L/min/m² SLR to 196.7 mg/L at the 1400 L/min/m² SLR. Effluent SSCs declined after the 1400 L/min/m² SLR because the unit begins to bypass flow at this rate. It should be noted that this was a very conservative test as sediment was preloaded in three areas, rather than in the lower sump alone, and the preloaded sediment on the pre-treatment channel and secondary plate had a finer PSD than the sediment found to settle in these areas during the lowest SLR capture test.

The second sediment scour test was conducted on an identical unit but with a 32% open-area perforated secondary plate of the same size and orientation as the solid plate used in the first test. The perforated plate was intended to allow most of the sediment to settle in the lower sump, while still protecting against sediment scour, and not affecting the capacity of the unit to capture sediment. A second capture test was run at the 600 L/min/m² SLR to confirm that the perforated plate would have the same flow characteristics and removal efficiencies as the solid plate. Results of this comparison presented in Table 2 show that removal efficiencies were not affected and that the collection sump was receiving the majority of sediment transported into the lower chamber. Based on the observed sediment deposition zones, the second repeat test with the perforated plate had sediment preloaded in the pre-treatment channel and the lower collection sump only (i.e. the major deposition zones). The collection sump was preloaded with 10.2 cm of the 1- 1000 µm test sediment mix, as in the first test, and the pre-treatment channel was preloaded in much the same way as the first test, but with a sediment PSD that more closely mimicked the PSD of sediment observed to settle in this area during the 40 L/min/m² sediment capture test.

Table 2: Injected mass captured at the 600 L/min/m² SLR for two different configurations of the secondary plate

Secondary Plate type	Target Surface Loading Rate (L/min/m ²)	Tested Flow Rate (L/min)	Removal Efficiency (%)	Pre-treatment Channel (%)	Secondary Plate (%)	Outlet Dispersion Plate (%)	Collection Sump (%)
Solid Plate	600	736.2	46.1	24.7	8.5	3.1	9.9
Perforated Plate	600	740.9	45.9	25.8	2.7	3.0	14.5

Results of the second test are presented in Table 3. Background concentrations were maintained below 10.5 mg/L. The average adjusted effluent suspended sediment concentrations ranged from 19.1 to 28.5 mg/L. Since the commercially available unit will have a perforated secondary plate, these concentrations are the appropriate values to consider for approvals. The verifier acknowledges that the sediment capture removal efficiencies were not all tested with the perforated plate (see variance notes below), but that the repeat test results at the 600 L/min/m² SLR and a statement from the independent test laboratory were sufficient to provide reasonable confidence that the added perforations in the secondary plate would have negligible influence on sediment removal efficiencies.

Table 3. Scour test adjusted effluent sediment concentrations

Run	Surface loading rate (L/min/m ²)	Run time (min)	Background sample concentration (mg/L) ^a	Average adjusted effluent suspended sediment concentration (mg/L) ^b
1	200	5	3.6	22.4
2	800	5	8.9	28.5
3	1400	5	7.6	20.0
4	2000	5	10.4	19.1
5	2600	5	6.0	24.4

^a Background concentrations shown here are approximate values based on graphical interpolation

^b The adjusted effluent suspended sediment concentration represents the actual measured effluent concentration minus the background concentration. For more information see [Bulletin # CETV 2016-09-0001](#). Adjusted concentrations were only calculated for the average of the five samples collected per surface loading rate.

The results of the light liquid re-entrainment test used to evaluate the unit’s capacity to prevent re-entrainment of light liquids are reported in Table 4. The test involved preloading 58.3 L (corresponding to a 5 cm depth over the collection sump area of 1.17m²) of surrogate low-density polyethylene beads (Dow Chemical Dowlex™ 2517) within the inner chamber and running clean water through the device continuously at five surface loading rates (200, 800, 1400, 2000, and 2600 L/min/m²). Each flow rate was maintained for 5 minutes with approximately 1 minute transition time between flow rates (30 minutes total). The effluent flow was screened to capture all re-entrained pellets throughout the test. Results showed maximum re-entrainment of 4.6% at 1400 L/min/m², which is the highest SLR without bypass. Re-entrainment decreased at subsequent SLRs as bypass volumes increased.

Table 4. Light liquid re-entrainment test results for the HS4

Surface Loading Rate (L/min/m ²)	Time Stamp (min)	Amount of Beads Re-entrained			
		Mass (g)	Volume (L)	% of Pre-loaded Mass Re-entrained	% of Pre-loaded Mass Retained
200	1:00 – 6:00	0	0	0.00	100
800	7:00 – 12:00	49	0.1	0.1	99.9
1400	13:00 – 18:00	1523	2.7	4.6	95.4
2000	19:00 – 24:00	1445	2.5	4.3	95.7
2600	25:00 – 30:00	847	1.5	2.5	97.5
Interim Collection Net		39	0.1	0.1	99.9
Total Re-entrained		3902	6.8	11.7	--
Total Retained		29,497	51.5	--	88.3
Total Loaded		33,399	58.3	--	--

Variations from testing Procedure

The following deviations from the *Procedure for Laboratory Testing of Oil-Grit Separators* (Version 3.0, June 2014) have been noted:

1. The Procedure stipulates that the tested device “must be a full scale, commercially available device with the same configuration and components that would be typical for an actual installation.” As noted above, the sediment capture tests were conducted with a solid secondary plate. The solid secondary plate was later modified to a 32% open area perforated plate to reduce sediment settling on the plate, while continuing to provide scour prevention. As described above, the scour test was repeated with the perforated secondary plate, but the sediment capture test was only repeated at the 600 L/min/m² SLR (i.e. one of seven tested SLRs). Removal efficiency results for the repeat test showed very close correspondence with the earlier test using the solid plate and much of the sediment that previously settled on the secondary plate was deposited in the lower collection sump (see Table 2). The independent laboratory provided the following statement regarding the potential for the added perforations to affect sediment removal efficiencies: “Taking into account the close proximity of the plate to the collection sump, as well as our knowledge of sediment transport, it is expected that the deposited sediment would have settled in the lower sump, with no impact on removal efficiency, if the plate was removed.” While the verifier acknowledges that stronger evidence would have been provided by additional repeat testing at a lower and higher SLR, the close correlation between the original and repeat test, combined with the statement from the lab were sufficient to provide reasonable confidence that adding the perforations would not likely have changed the capture test results significantly.
2. The repeat test at the 600 L/min/m² SLR had background concentrations exceeding the 20 mg/L threshold during the last half of the test. The exceedances occurred in 4 of the 8 samples collected, reaching a maximum of 28.4 mg/L. The experimental apparatus is a closed loop system. Therefore, the sediment in the background samples consists of fine particles not captured by the device, and would therefore not likely bias the mass balance results.

3. It was necessary to change flow meters during the sediment scour and light liquid re-entrainment test, as the required flows exceeded the minimum and/or maximum range of any single meter. When the flow capacity of the selected meter was reached, the flow was shut down over a period of approximately 10 seconds and all flow data saved. The next data acquisition file was executed and flow increased at a rate that corresponded to reaching each previous target flow after a period of 1-minute. This procedure was approved by CETV prior to testing, in recognition that most particles susceptible to scour at low flows would not be in the sump at higher flows. Similarly, re-entrainment of the oil beads was not expected to be significantly affected by the flow meter change.
4. As part of the capture test, evaluation of the 40 and 80 L/min/m² surface loading rate was split into 3 and 2 parts, respectively, due to the long duration needed to feed the required minimum of 11.3 kg of test sediment into the unit. At the end of the first and second parts of the test, the flow rates were gradually shutdown to prevent capture of particles that would have been washed out under normal circumstances. The amended procedure was reviewed and approved by the verifier prior to testing.

Verification

The verification was completed by the Verification Expert, Toronto and Region Conservation Authority, contracted by GLOBE Performance Solutions, using the International Standard **ISO 14034:2016 Environmental management – Environmental technology verification (ETV)**. Data and information provided by Hydroworks, LLC to support the performance claim included the following: Performance test report prepared by Alden Research Laboratory, Inc., and dated February 2018. This report is based on testing completed in accordance with the *Procedure for Laboratory Testing of Oil-Grit Separators* (Version 3.0, June 2014).

What is ISO 14034:2016 Environmental management – Environmental technology verification (ETV)?

ISO 14034:2016 specifies principles, procedures and requirements for environmental technology verification (ETV), and was developed and published by the *International Organization for Standardization (ISO)*. The objective of ETV is to provide credible, reliable and independent verification of the performance of environmental technologies. An environmental technology is a technology that either results in an environmental added value or measures parameters that indicate an environmental impact. Such technologies have an increasingly important role in addressing environmental challenges and achieving sustainable development.

**For more information on the Hydroworks®
HS Hydrodynamic Separator please contact:**

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Limitation of verification

GLOBE Performance Solutions and the Verification Expert provide the verification services solely on the basis of the information supplied by the applicant or vendor and assume no liability thereafter. The responsibility for the information supplied remains solely with the applicant or vendor and the liability for the purchase, installation, and operation (whether consequential or otherwise) is not transferred to any other party as a result of the verification.



Hydroworks® HydroStorm

Operations & Maintenance Manual

Version 1.0

Please call Hydroworks at 888-290-7900 or email us at support@hydroworks.com if you have any questions regarding the Inspection Checklist. Please fax a copy of the completed checklist to Hydroworks at 888-783-7271 for our records.

Introduction

The HydroStorm is a state of the art hydrodynamic separator. Hydrodynamic separators remove solids, debris and lighter than water (oil, trash, floating debris) pollutants from stormwater. Hydrodynamic separators and other water quality measures are mandated by regulatory agencies (Town/City, State, Federal Government) to protect storm water quality from pollution generated by urban development (traffic, people) as part of new development permitting requirements.

As storm water treatment structures fill up with pollutants they become less and less effective in removing new pollution. Therefore, it is important that storm water treatment structures be maintained on a regular basis to ensure that they are operating at optimum performance. The HydroStorm is no different in this regard and this manual has been assembled to provide the owner/operator with the necessary information to inspect and coordinate maintenance of their HydroStorm.

Hydroworks® HydroStorm Operation

The Hydroworks HydroStorm (HS) separator is a unique hydrodynamic by-pass separator. It incorporates a protected submerged pretreatment zone to collect larger solids, a treatment tank to remove finer solids, and a dual set of weirs to create a high flow bypass. High flows are conveyed directly to the outlet and do not enter the treatment area, however, the submerged pretreatment area still allows removal of coarse solids during high flows.

Under normal or low flows, water enters an inlet area with a horizontal grate. The area underneath the grate is submerged with openings to the main treatment area of the separator. Coarse solids fall through the grate and are either trapped in the pretreatment area or conveyed into the main treatment area depending on the flow rate. Fines are transported into the main treatment area. Openings and weirs in the pretreatment area allow entry of water and solids into the main treatment area and cause water to rotate in the main treatment area creating a vortex motion. Water in the main treatment area is forced to rise along the walls of the separator to discharge from the treatment area to the downstream pipe.

The vortex motion forces solids and floatables to the middle of the inner chamber. Floatables are trapped since the inlet to the treatment area is submerged. The design maximizes the retention of settled solids since solids are forced to the center of the inner chamber by the vortex motion of water while water must flow up the walls of the separator to discharge into the downstream pipe.

A set of high flow weirs near the outlet pipe create a high flow bypass over both the pretreatment area and main treatment chamber. The rate of flow into the treatment area is regulated by the number and size of openings into the treatment chamber and the height of by-pass weirs. High flows flow over the weirs directly to the outlet pipe preventing the scour and resuspension of any fines collected in the treatment chamber.



A central access tube is located in the structure to provide access for cleaning. The arrangement of the inlet area and bypass weirs near the outlet pipe facilitate the use of multiple inlet pipes.

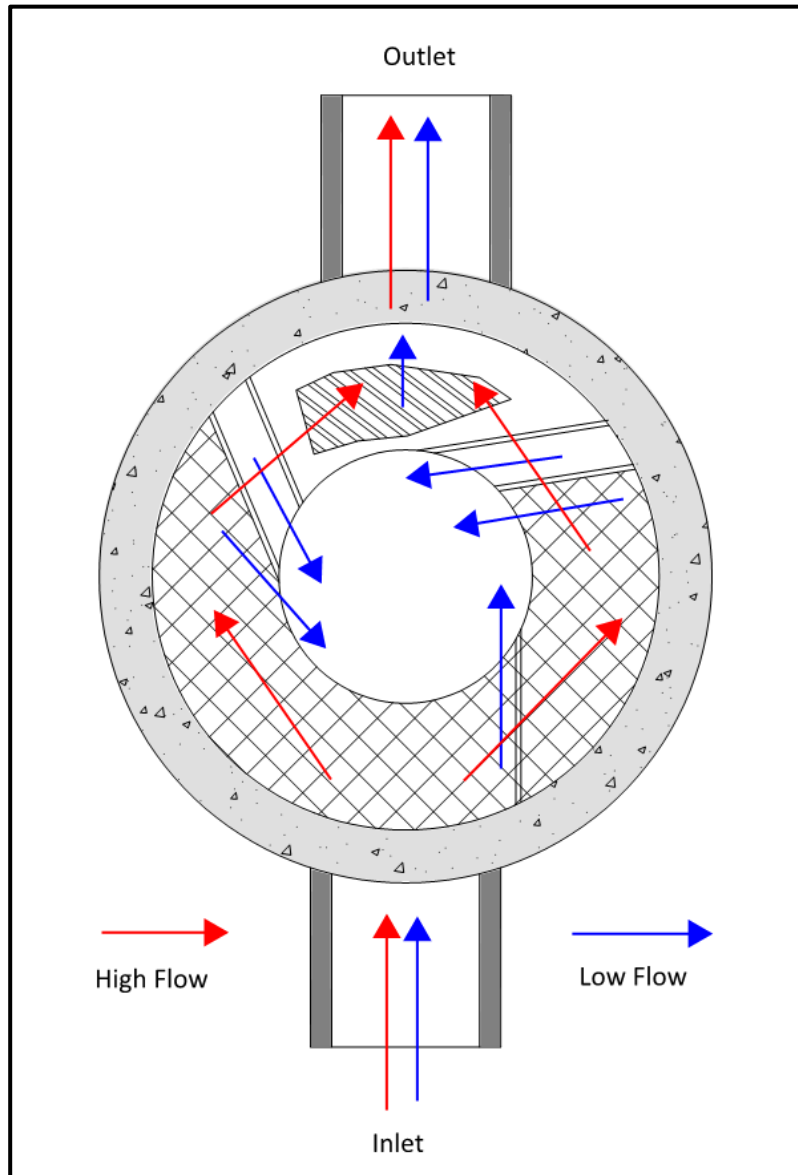


Figure 1. Hydroworks HydroStorm Operation – Plan View

Figure 2 is a profile view of the HydroStorm separator showing the flow patterns for low and high flows.

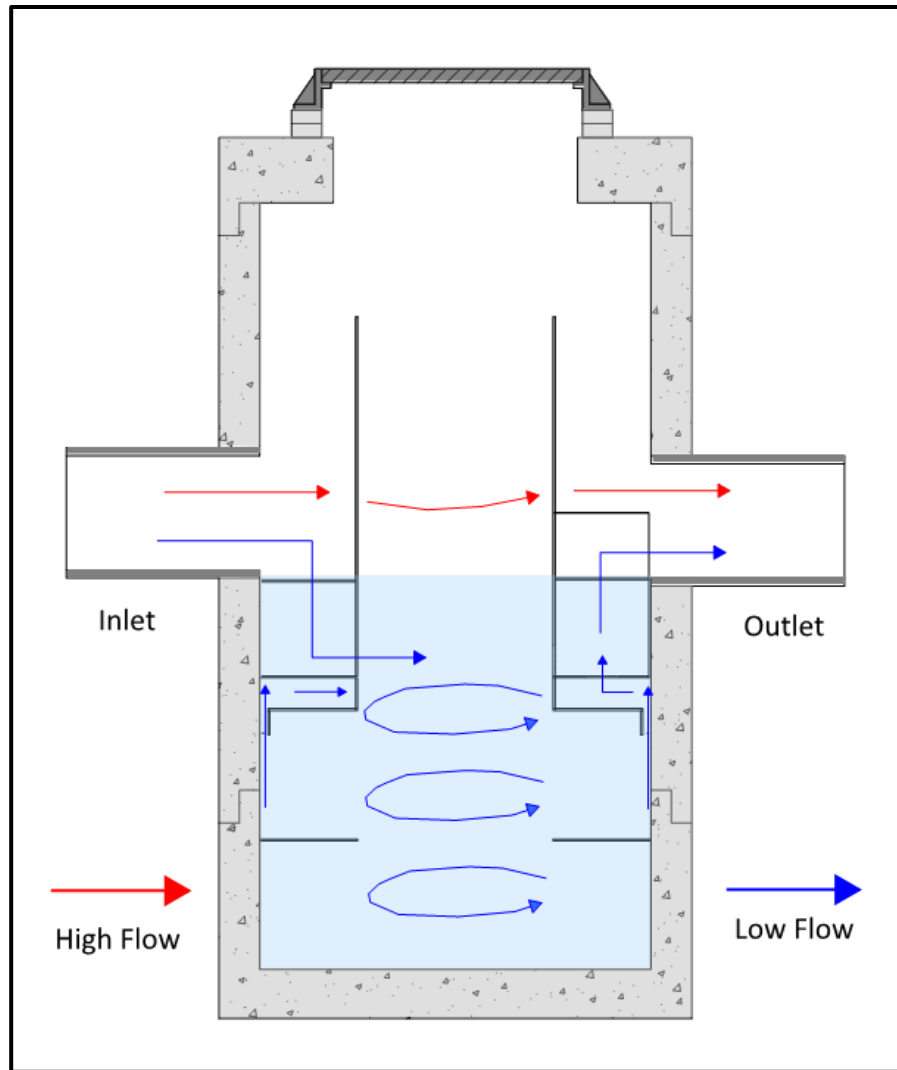


Figure 2. Hydroworks HydroStorm Operation – Profile View

The HS 4i is an inlet version of the HS 4 separator. There is a catch-basin grate on top of the HS 4i. A funnel sits underneath the grate on the frame and directs the water to the inlet side of the separator to ensure all low flows are properly treated. The whole funnel is removed for inspection and cleaning.

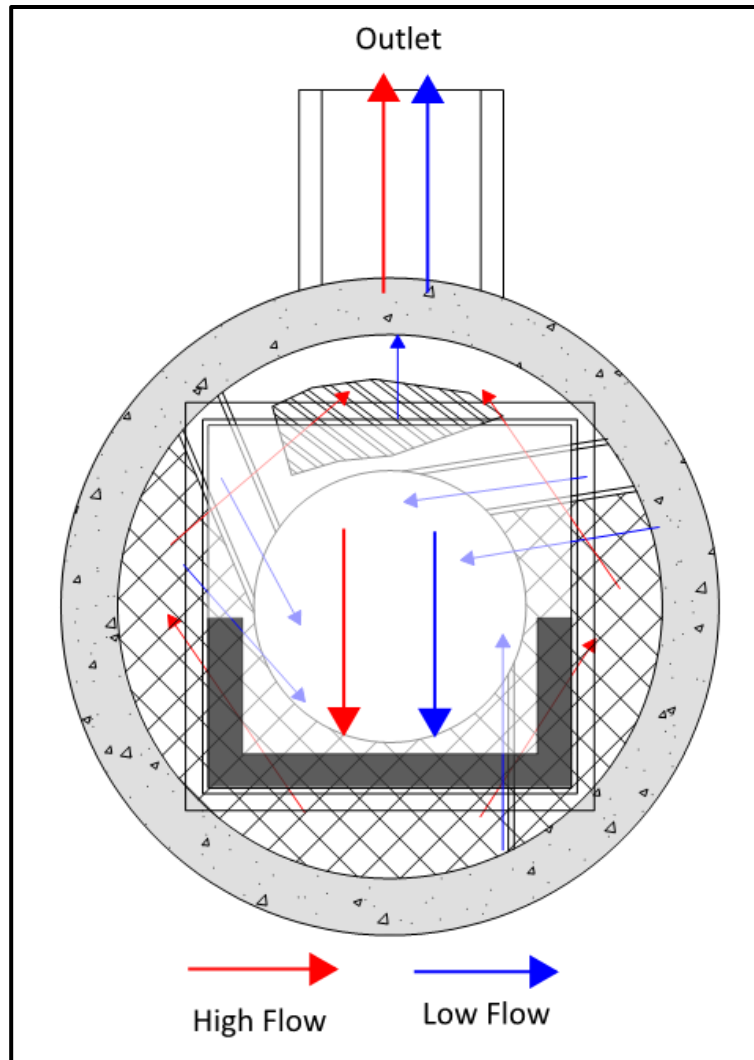


Figure 3. Hydroworks HS 4i Funnel

Inspection

Procedure

Floatables

A visual inspection can be conducted for floatables by removing the covers and looking down into the center access tube of the separator. Separators with an inlet grate (HS 4i or custom separator) will have a plastic funnel located under the grate that must be removed from the frame prior to inspection or maintenance. If you are missing a funnel please contact Hydroworks at the numbers provided at the end of this document.

TSS/Sediment

Inspection for TSS build-up can be conducted using a Sludge Judge®, Core Pro®, AccuSludge® or equivalent sampling device that allows the measurement of the depth of TSS/sediment in the unit. These devices typically have a ball valve at the bottom of the tube that allows water and TSS to flow into the tube when lowering the tube into the unit. Once the unit touches the bottom of the device, it is quickly pulled upward such that the water and TSS in the tube forces the ball valve closed allowing the user to see a full core of water/TSS in the unit. The unit should be inspected for TSS through each of the access covers. Several readings (2 or 3) should be made at each access cover to ensure that an accurate TSS depth measurement is recorded.

Frequency

Construction Period

The HydroStorm separator should be inspected every four weeks and after every large storm (over 0.5" (12.5 mm) of rain) during the construction period.

Post-Construction Period

The Hydroworks HydroStorm separator should be inspected during the first year of operation for normal stabilized sites (grassed or paved areas). If the unit is subject to oil spills or runoff from unstabilized (storage piles, exposed soils) areas the HydroStorm separator should be inspected more frequently (4 times per year). The initial annual inspection will indicate the required future frequency of inspection and maintenance if the unit was maintained after the construction period.

Reporting

Reports should be prepared as part of each inspection and include the following information:

1. Date of inspection
2. GPS coordinates of Hydroworks unit
3. Time since last rainfall
4. Date of last inspection
5. Installation deficiencies (missing parts, incorrect installation of parts)
6. Structural deficiencies (concrete cracks, broken parts)
7. Operational deficiencies (leaks, blockages)
8. Presence of oil sheen or depth of oil layer
9. Estimate of depth/volume of floatables (trash, leaves) captured
10. Sediment depth measured
11. Recommendations for any repairs and/or maintenance for the unit
12. Estimation of time before maintenance is required if not required at time of inspection



A sample inspection checklist is provided at the end of this manual.

Maintenance

Procedure

The Hydroworks HydroStorm unit is typically maintained using a vacuum truck. There are numerous companies that can maintain the HydroStorm separator. Maintenance with a vacuum truck involves removing all of the water and sediment together. The water is then separated from the sediment on the truck or at the disposal facility.

A central access opening (24" or greater) is provided to the gain access to the lower treatment tank of the unit. This is the primary location to maintain by vacuum truck. The pretreatment area can also be vacuumed and/or flushed into the lower treatment tank of the separator for cleaning via the central access once the water level is lowered below the pretreatment floor.

In instances where a vacuum truck is not available other maintenance methods (i.e. clamshell bucket) can be used, but they will be less effective. If a clamshell bucket is used the water must be decanted prior to cleaning since the sediment is under water and typically fine in nature. Disposal of the water will depend on local requirements. Disposal options for the decanted water may include:

1. Discharge into a nearby sanitary sewer manhole
2. Discharge into a nearby LID practice (grassed swale, bioretention)
3. Discharge through a filter bag into a downstream storm drain connection

The local municipality should be consulted for the allowable disposal options for both water and sediments prior to any maintenance operation. Once the water is decanted the sediment can be removed with the clamshell bucket.

Disposal of the contents of the separator depend on local requirements. Maintenance of a Hydroworks HydroStorm unit will typically take 1 to 2 hours based on a vacuum truck and longer for other cleaning methods (i.e. clamshell bucket).



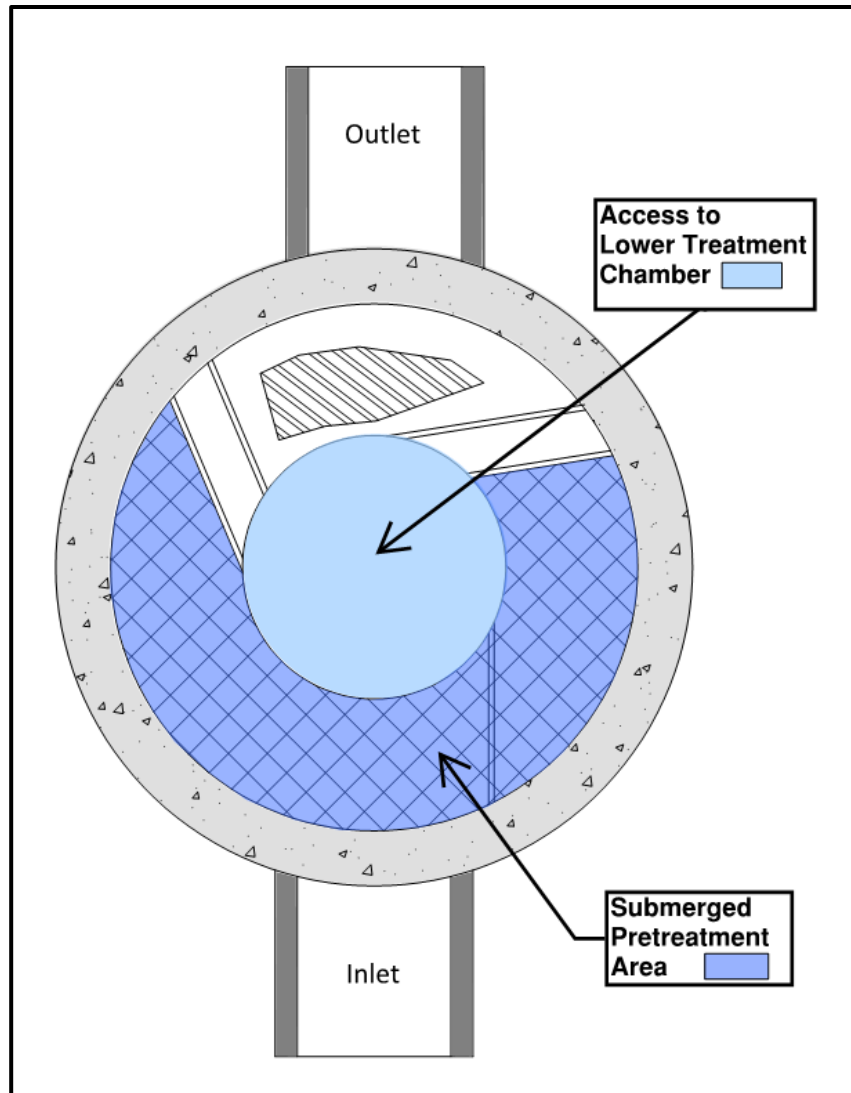


Figure 3. Maintenance Access

Frequency

Construction Period

A HydroStorm separator can fill with construction sediment quickly during the construction period. The HydroStorm must be maintained during the construction period when the depth of TSS/sediment reaches 24" (600 mm). It must also be maintained during the construction period if there is an appreciable depth of oil in the unit (more than a sheen) or if floatables other than oil cover over 50% of the area of the separator

The HydroStorm separator should be maintained at the end of the construction period, prior to operation for the post-construction period.

Post-Construction Period

The HydroStorm was independently tested by Alden Research Laboratory in 2017. A HydroStorm HS 4 was tested for scour with a 50% sediment depth of 0.5 ft. Therefore, maintenance for sediment accumulation is required if the depth of sediment is 1 ft or greater in separators with standard water (sump) depths (Table 1).

There will be designs with increased sediment storage based on specifications or site-specific criteria. A measurement of the total water depth in the separator through the central access tube should be taken and compared to water depth given in Table 1. The standard water depth from Table 1 should be subtracted from the measured water depth and the resulting extra depth should be added to the 1 ft to determine the site-specific sediment maintenance depth for that separator.

For example, if the measured water depth in the HS-7 is 7 feet, then the sediment maintenance depth for that HS-7 is 2 ft ($= 1 + 7 - 6$) and the separator does not need to be cleaned for sediment accumulation until the measure sediment depth is 2 ft.

The HydroStorm separator must also be maintained if there is an appreciable depth of oil in the unit (more than a sheen) or if floatables other than oil cover over 50% of the water surface of the separator.

Table 1 Standard Dimensions for Hydroworks HydroStorm Models

Model	Diameter (ft)	Total Water Depth (ft)	Sediment Maintenance Depth for Table 1 Total Water Depth(ft)
HS-3	3	3	1
HS-4	4	4	1
HS-5	5	4	1
HS-6	6	4	1
HS-7	7	6	1
HS-8	8	7	1
HS-9	9	7.5	1
HS-10	10	8	1
HS-11	11	9	1
HS-12	12	9.5	1



HYDROSTORM INSPECTION SHEET

Date
Date of Last Inspection _____

Site
City _____
State _____
Owner _____

GPS Coordinates _____

Date of last rainfall _____

Site Characteristics	Yes	No
Soil erosion evident	<input type="checkbox"/>	<input type="checkbox"/>
Exposed material storage on site	<input type="checkbox"/>	<input type="checkbox"/>
Large exposure to leaf litter (lots of trees)	<input type="checkbox"/>	<input type="checkbox"/>
High traffic (vehicle) area	<input type="checkbox"/>	<input type="checkbox"/>

HydroStorm	Yes	No
Obstructions in the inlet or outlet	<input type="checkbox"/> *	<input type="checkbox"/>
Missing internal components	<input type="checkbox"/> **	<input type="checkbox"/>
Improperly installed inlet or outlet pipes	<input type="checkbox"/> ***	<input type="checkbox"/>
Internal component damage (cracked, broken, loose pieces)	<input type="checkbox"/> **	<input type="checkbox"/>
Floating debris in the separator (oil, leaves, trash)	<input type="checkbox"/>	<input type="checkbox"/>
Large debris visible in the separator	<input type="checkbox"/> *	<input type="checkbox"/>
Concrete cracks/deficiencies	<input type="checkbox"/> ***	<input type="checkbox"/>
Exposed rebar	<input type="checkbox"/> **	<input type="checkbox"/>
Water seepage (water level not at outlet pipe invert)	<input type="checkbox"/> ***	<input type="checkbox"/>
Water level depth below outlet pipe invert _____"		

Routine Measurements			
Floating debris depth	<input type="checkbox"/> < 0.5" (13mm)	<input type="checkbox"/> >0.5" 13mm)	<input type="checkbox"/> *
Floating debris coverage	<input type="checkbox"/> < 50% of surface area	<input type="checkbox"/> > 50% surface area	<input type="checkbox"/> *
Sludge depth	<input type="checkbox"/> < 12" (300mm)	<input type="checkbox"/> > 12" (300mm)	<input type="checkbox"/> *

* Maintenance required
 ** Repairs required
 *** Further investigation is required





Hydroworks® HydroStorm

One Year Limited Warranty

Hydroworks, LLC warrants, to the purchaser and subsequent owner(s) during the warranty period subject to the terms and conditions hereof, the Hydroworks HydroStorm to be free from defects in material and workmanship under normal use and service, when properly installed, used, inspected and maintained in accordance with Hydroworks written instructions, for the period of the warranty. The standard warranty period is 1 year.

The warranty period begins once the separator has been manufactured and is available for delivery. Any components determined to be defective, either by failure or by inspection, in material and workmanship will be repaired, replaced or remanufactured at Hydroworks' option provided, however, that by doing so Hydroworks, LLC will not be obligated to replace an entire insert or concrete section, or the complete unit. This warranty does not cover shipping charges, damages, labor, any costs incurred to obtain access to the unit, any costs to repair/replace any surface treatment/cover after repair/replacement, or other charges that may occur due to product failure, repair or replacement.

This warranty does not apply to any material that has been disassembled or modified without prior approval of Hydroworks, LLC, that has been subjected to misuse, misapplication, neglect, alteration, accident or act of God, or that has not been installed, inspected, operated or maintained in accordance with Hydroworks, LLC instructions and is in lieu of all other warranties expressed or implied. Hydroworks, LLC does not authorize any representative or other person to expand or otherwise modify this limited warranty.

The owner shall provide Hydroworks, LLC with written notice of any alleged defect in material or workmanship including a detailed description of the alleged defect upon discovery of the defect. Hydroworks, LLC should be contacted at 136 Central Ave., Clark, NJ 07066 or any other address as supplied by Hydroworks, LLC. (888-290-7900).

This limited warranty is exclusive. There are no other warranties, express or implied, or merchantability or fitness for a particular purpose and none shall be created whether under the uniform commercial code, custom or usage in the industry or the course of dealings between the parties. Hydroworks, LLC will replace any goods that are defective under this warranty as the sole and exclusive remedy for breach of this warranty.

Subject to the foregoing, all conditions, warranties, terms, undertakings or liabilities (including liability as to negligence), expressed or implied, and howsoever arising, as to the condition, suitability, fitness, safety, or title to the Hydroworks HydroStorm are hereby negated and excluded and Hydroworks, LLC gives and makes no such representation, warranty or undertaking except as expressly set forth herein. Under no circumstances shall Hydroworks, LLC be liable to the Purchaser or to any third party for product liability claims; claims arising from the design, shipment, or installation of the HydroStorm, or the cost of other goods or services related to the purchase and installation of the HydroStorm. For this Limited Warranty to apply, the HydroStorm must be installed in accordance with all site conditions required by state and local codes; all other applicable laws; and Hydroworks' written installation instructions.

Hydroworks, LLC expressly disclaims liability for special, consequential or incidental damages (even if it has been advised of the possibility of the same) or breach of expressed or implied warranty. Hydroworks, LLC shall not be liable for penalties or liquidated damages, including loss of production and profits; labor and materials; overhead costs; or other loss or expense incurred by the purchaser or any third party. Specifically excluded from limited warranty coverage are damages to the HydroStorm arising from ordinary wear and tear; alteration, accident, misuse, abuse or neglect; improper maintenance, failure of the product due to improper installation of the concrete sections or improper sizing; or any other event not caused by Hydroworks, LLC. This limited warranty represents Hydroworks' sole liability to the purchaser for claims related to the HydroStorm, whether the claim is based upon contract, tort, or other legal basis.

APPENDIX E

FLOODPLAIN ANALYSIS MEMO



S. LLEWELLYN & ASSOCIATES LIMITED
CONSULTING ENGINEERS

TECHNICAL MEMORANDUM

To:	Matthew Lauzon, Planning and Regulations Analyst Conservation Halton	From:	Steven DeGrow Steven Frankovich
		Date:	July 6, 2022
Project:	Holy Family Catholic Cemetery 2523 Lower Base line Milton, ON	Pages:	4 + Appendix
		Job #:	13084
Re:	Floodplain Analysis for the proposed crossing culvert crossing of Sixteen Mile Creek Tributary		

Introduction

S. Llewellyn & Associates Limited has been retained by The Catholic Cemeteries of the Dioceses of Hamilton to provide consulting engineering services for the proposed Phase 2 portion of the Holy Family Catholic Cemetery development at the corner of Regional Road No. 25 and Lower Baseline Road in the Town of Milton (see Figure 1.0 for location plan). The property is traversed by a tributary of Sixteen Mile Creek that flows in a northeastern direction (see Figure 1.0 for location plan). Furthermore, the northeastern quadrant of the property has been redeveloped and converted from agricultural to cemetery lands with an associated asphalt roadway system. The remaining undeveloped portion of the site currently remains agricultural lands.

The proposed Phase 2 portion of the development consists of constructing one (1) single storey building for use as a crematorium facility. Additionally, there will be an associated asphalt parking lot with concrete curbing/sidewalks, landscaped areas, and an asphalt roadway that will connect to the existing cemetery roadway system. In order to connect the roadway system, it will be required to cross SMT-1 which is a tributary of the Sixteen Mile Creek. This technical memorandum will provide detailed information on the proposed watercourse crossing that has been designed to provide safe ingress/egress.

Background

The following information was used in the preparation of this memo:

- Ref. 1: Topographic surveys from Mackay, Mackay & Peters Limited. (December 01, 2014)
- Ref. 2: Stormwater Management Report for the proposed Cemetery Developments At Regional Road No. 25 And Lower Baseline Road In The Town of (AMEC Environment & Infrastructure, February 2012)



Ref. 3: Conservation Halton Planning & Permits Map-arcgis.com



Figure 1 – Location Plan

Hydraulic Modeling Information

Hydraulic analysis of the watercourse was performed using the HEC-RAS program developed by the U.S. Army Corp. of Engineers. The current HEC-RAS model for the tributaries of Sixteen Mile Creek which traverse the site was originally prepared by AMEC Environmental & Infrastructure.

Existing HEC-RAS Model

The HEC-RAS hydraulic model provided to S. Llewellyn & Associates was analyzed as provided to establish the existing condition water surface elevations (WSEL) for the 5-year to Regional storm events. See Appendix A for the output listing of the existing conditions. The existing condition WSEL's are also noted in Table 1.

The existing model consisted of nineteen (19) cross sections along SMT-1 with seven (7) downstream of the existing box culvert crossing Regional Road 25 and twelve upstream. Furthermore, there are six (6) cross sections along SMT-2, two (2) cross sections along SMT 3, and five (5) cross sections along SMT-4.



PROPOSED CONDITIONS MODEL INFORMATION

Under proposed conditions, the cross-section data was adjusted based on the proposed box culvert. To accurately model the proposed culvert in HEC-RAS an additional, 3 cross sections were added before and after the culvert. It is proposed to install a 6.0m span x 1.5m rise closed bottom box culvert that is counter sunk 15% (0.225m) as per Conservation Halton's requirements. The roadway system will cross SMT-1 over the culvert structure. The culvert will have a total length of approximately 10.0 m.

Boundary Conditions – The boundary conditions of the original model were maintained in the proposed conditions model.

Cross-Section Flows – The flow rates applied to the cross-sections for the 5-yr, 10-yr, 25-yr, 50-yr, 100-yr, and Regional storm events in the AMEC HEC-RAS model were maintained in the proposed condition. The hydrology in the original HEC-RAS model was derived from the SWMHYMO file for the future conditions with stormwater management controls which were included in the “Stormwater Management Report for the proposed Cemetery Developments At Regional Road No. 25 and Lower Baseline Road In the Town of Milton” completed in February 2012 by AMEC Environmental & Infrastructure. Since this SWMHYMO model stipulates the maximum permissible post-development flow rates from the site the hydrology in the original AMEC HEC-RAS model is conservative.

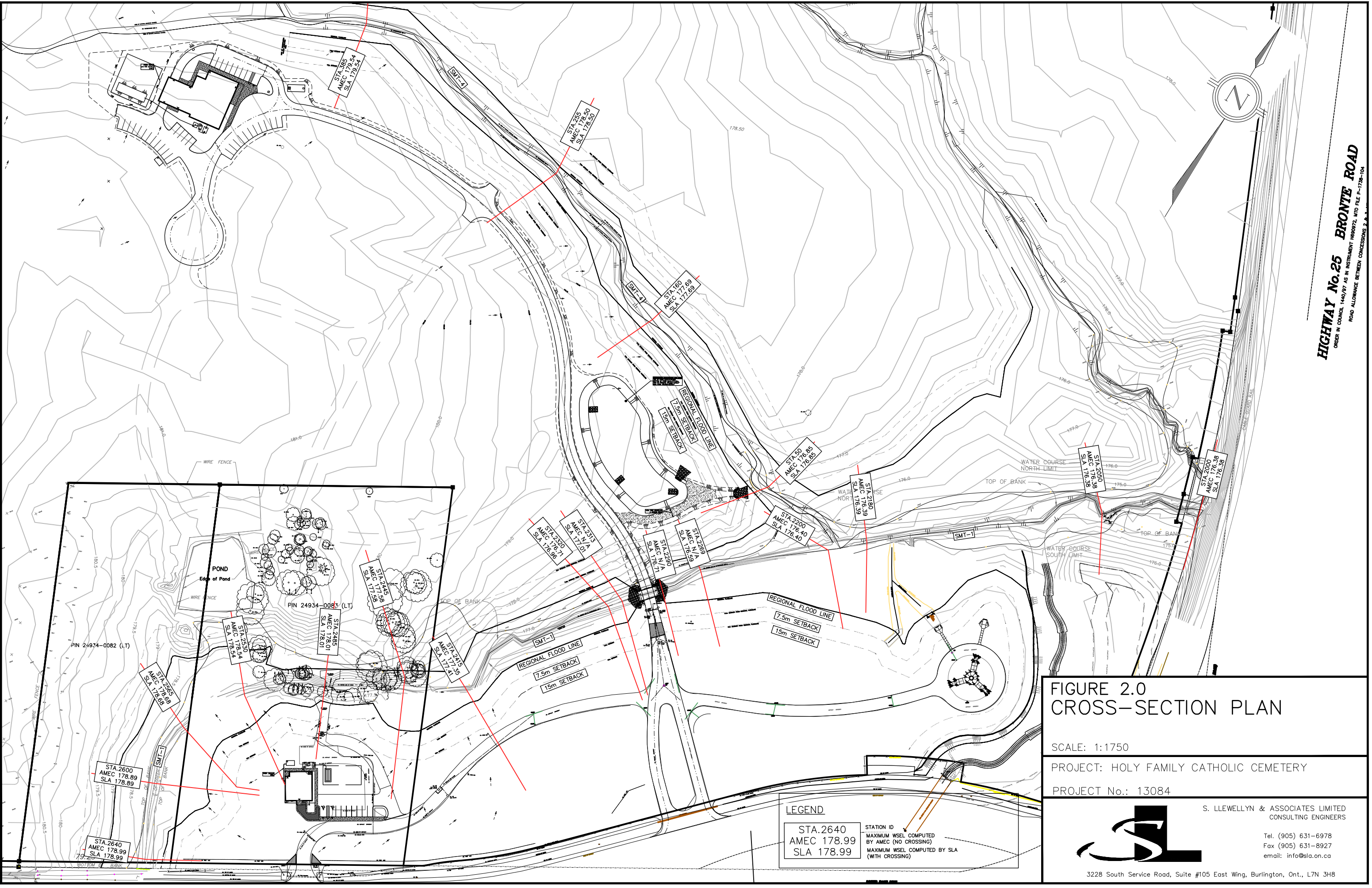
Culvert Cross-Section – The proposed culvert cross-section was entered into HEC-RAS model as depicted in the technical drawings completed by MCON products for the typical 6.0m span closed bottom box culvert. The road deck is conservatively 1.29m above the soffit of the culvert at the crown of the road. This accounts for the thickness of the culvert wall along with the pavement buildup over the culvert. See Appendix B for proposed conditions output information.

ANALYSIS RESULTS AND COMMENTS

Table 1.0 summarizes the calculated water surface elevations for the existing and proposed conditions upstream and downstream of the proposed bridge work. Figure 2.0 shows cross-section locations as well as the existing and proposed Regional Event floodline elevations.

The analysis results indicate the following:

- With the installation of the 6.0m x 1.5m box culvert there is a slight increase in the calculated water surface elevation (WSEL) upstream of the culvert crossing. This increase in water surface elevation extends from the proposed culvert to the upstream cross section 2415.
- Downstream of the proposed culvert crossing there is no change in water surface elevation during any of the storm events.
- All storm events including the regional storm will pass under the structure.



**FIGURE 2.0
CROSS-SECTION PLAN**

SCALE: 1:1750

PROJECT: HOLY FAMILY CATHOLIC CEMETERY

PROJECT No.: 13084

LEGEND

STA.2640	STATION ID
AMEC 178.99	MAXIMUM WSEL COMPUTED BY AMEC (NO CROSSING)
SLA 178.99	MAXIMUM WSEL COMPUTED BY SLA (WITH CROSSING)

S. LLEWELLYN & ASSOCIATES LIMITED
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email: info@sla.on.ca

3228 South Service Road, Suite #105 East Wing, Burlington, Ont., L7N 3H8

HIGHWAY No.25 BRONTE ROAD
ORDER IN COUNCIL 1440/97 AS IN INSTRUMENT H86972, M70 FILE P-173-104
ROAD ALLOWANCE BETWEEN CONCESSIONS 2 & 3

Table 1 - Comparison of Existing & Proposed Water Surface Elevations (see Fig. 2.0 for x-section locations)

Reach	River Sta	Profile	Q Total (m ³ /s)	Existing W.S. Elev (m)	Proposed W.S. Elev (m)	Difference in WSEL (m)
SMT-4	385	2 YR	0.54	179.33	179.33	0.00
SMT-4	385	5 YR	0.94	179.41	179.41	0.00
SMT-4	385	10 YR	1.23	179.45	179.45	0.00
SMT-4	385	25 YR	1.61	179.49	179.49	0.00
SMT-4	385	50 YR	1.89	179.51	179.51	0.00
SMT-4	385	100 YR	2.18	179.54	179.54	0.00
SMT-4	385	REG	1.90	179.51	179.51	0.00
SMT-4	255	2 YR	0.54	178.35	178.35	0.00
SMT-4	255	5 YR	0.94	178.41	178.41	0.00
SMT-4	255	10 YR	1.23	178.44	178.44	0.00
SMT-4	255	25 YR	1.61	178.47	178.47	0.00
SMT-4	255	50 YR	1.89	178.49	178.49	0.00
SMT-4	255	100 YR	2.18	178.50	178.50	0.00
SMT-4	255	REG	1.90	178.49	178.49	0.00
SMT-4	160	2 YR	0.54	177.54	177.54	0.00
SMT-4	160	5 YR	0.94	177.59	177.59	0.00
SMT-4	160	10 YR	1.23	177.62	177.62	0.00
SMT-4	160	25 YR	1.61	177.65	177.65	0.00
SMT-4	160	50 YR	1.89	177.67	177.67	0.00
SMT-4	160	100 YR	2.18	177.69	177.69	0.00
SMT-4	160	REG	1.90	177.67	177.67	0.00
SMT-4	50	2 YR	0.54	176.75	176.75	0.00
SMT-4	50	5 YR	0.94	176.78	176.78	0.00
SMT-4	50	10 YR	1.23	176.80	176.80	0.00
SMT-4	50	25 YR	1.61	176.82	176.82	0.00
SMT-4	50	50 YR	1.89	176.83	176.83	0.00
SMT-4	50	100 YR	2.18	176.85	176.85	0.00
SMT-4	50	REG	1.90	176.83	176.83	0.00
SMT-1	2640	2 YR	2.76	178.69	178.69	0.00
SMT-1	2640	5 YR	4.83	178.77	178.77	0.00
SMT-1	2640	10 YR	6.30	178.82	178.82	0.00
SMT-1	2640	25 YR	8.20	178.88	178.88	0.00
SMT-1	2640	50 YR	10.15	178.93	178.93	0.00
SMT-1	2640	100 YR	11.71	178.97	178.97	0.00
SMT-1	2640	REG	12.67	178.99	178.99	0.00
SMT-1	2600	2 YR	2.76	178.49	178.49	0.00
SMT-1	2600	5 YR	4.83	178.61	178.61	0.00
SMT-1	2600	10 YR	6.30	178.68	178.68	0.00
SMT-1	2600	25 YR	8.20	178.75	178.75	0.00
SMT-1	2600	50 YR	10.15	178.81	178.81	0.00
SMT-1	2600	100 YR	11.71	178.86	178.86	0.00
SMT-1	2600	REG	12.67	178.89	178.89	0.00
SMT-1	2565	2 YR	2.76	178.31	178.31	0.00
SMT-1	2565	5 YR	4.83	178.40	178.40	0.00
SMT-1	2565	10 YR	6.30	178.46	178.46	0.00
SMT-1	2565	25 YR	8.20	178.53	178.53	0.00
SMT-1	2565	50 YR	10.15	178.59	178.59	0.00
SMT-1	2565	100 YR	11.71	178.65	178.65	0.00
SMT-1	2565	REG	12.67	178.68	178.68	0.00
SMT-1	2530	2 YR	2.76	177.98	177.98	0.00
SMT-1	2530	5 YR	4.83	178.15	178.15	0.00
SMT-1	2530	10 YR	6.30	178.24	178.24	0.00
SMT-1	2530	25 YR	8.20	178.33	178.33	0.00
SMT-1	2530	50 YR	10.15	178.43	178.43	0.00
SMT-1	2530	100 YR	11.71	178.50	178.50	0.00
SMT-1	2530	REG	12.67	178.54	178.54	0.00
SMT-1	2485	2 YR	2.76	177.50	177.50	0.00
SMT-1	2485	5 YR	4.83	177.62	177.62	0.00
SMT-1	2485	10 YR	6.30	177.71	177.71	0.00
SMT-1	2485	25 YR	8.20	177.82	177.82	0.00
SMT-1	2485	50 YR	10.15	177.92	177.92	0.00
SMT-1	2485	100 YR	11.71	177.98	177.98	0.00
SMT-1	2485	REG	12.67	178.01	178.01	0.00
SMT-1	2445	2 YR	2.76	177.18	177.18	0.00
SMT-1	2445	5 YR	4.83	177.29	177.29	0.00
SMT-1	2445	10 YR	6.30	177.36	177.36	0.00
SMT-1	2445	25 YR	8.20	177.44	177.44	0.00
SMT-1	2445	50 YR	10.15	177.50	177.50	0.00
SMT-1	2445	100 YR	11.71	177.56	177.56	0.00
SMT-1	2445	REG	12.67	177.58	177.58	0.00
SMT-1	2415	2 YR	2.76	176.92	176.93	0.01
SMT-1	2415	5 YR	4.83	177.05	177.05	0.00
SMT-1	2415	10 YR	6.30	177.12	177.13	0.01
SMT-1	2415	25 YR	8.20	177.20	177.22	0.02
SMT-1	2415	50 YR	10.15	177.27	177.30	0.03
SMT-1	2415	100 YR	11.71	177.32	177.37	0.05
SMT-1	2415	REG	12.67	177.35	177.41	0.06
SMT-1	2320	2 YR	2.76	176.19	176.26	0.07
SMT-1	2320	5 YR	4.83	176.34	176.45	0.11
SMT-1	2320	10 YR	6.30	176.43	176.56	0.13
SMT-1	2320	25 YR	8.20	176.53	176.70	0.17
SMT-1	2320	50 YR	10.15	176.61	176.81	0.20
SMT-1	2320	100 YR	11.71	176.67	176.90	0.23
SMT-1	2320	REG	12.67	176.71	176.96	0.25

Reach	River Sta	Profile	Q Total (m ³ /s)	Existing W.S. Elev (m)	Proposed W.S. Elev (m)	Difference in WSEL (m)
<i>(Note: Cross-Section 2313 only in Proposed Model)</i>						
SMT-1	2313	2 YR	2.76		176.34	N/A
SMT-1	2313	5 YR	4.83		176.54	N/A
SMT-1	2313	10 YR	6.30		176.64	N/A
SMT-1	2313	25 YR	8.20		176.77	N/A
SMT-1	2313	50 YR	10.15		176.88	N/A
SMT-1	2313	100 YR	11.71		176.96	N/A
SMT-1	2313	REG	12.67		177.01	N/A
<i>6.0mx1.5m Box Culvert @ River Station 2308</i>						
<i>(Note: Cross-Section 2290 only in Proposed Model)</i>						
SMT-1	2290	2 YR	2.76		176.30	N/A
SMT-1	2290	5 YR	4.83		176.45	N/A
SMT-1	2290	10 YR	6.30		176.53	N/A
SMT-1	2290	25 YR	8.20		176.61	N/A
SMT-1	2290	50 YR	10.15		176.66	N/A
SMT-1	2290	100 YR	11.71		176.69	N/A
SMT-1	2290	REG	12.67		176.71	N/A
<i>(Note: Cross-Section 2269 only in Proposed Model)</i>						
SMT-1	2269	2 YR	2.76		176.11	N/A
SMT-1	2269	5 YR	4.83		176.24	N/A
SMT-1	2269	10 YR	6.30		176.32	N/A
SMT-1	2269	25 YR	8.20		176.41	N/A
SMT-1	2269	50 YR	10.15		176.50	N/A
SMT-1	2269	100 YR	11.71		176.56	N/A
SMT-1	2269	REG	12.67		176.59	N/A
SMT-1	2200	2 YR	3.63	175.39	175.39	0.00
SMT-1	2200	5 YR	6.34	175.56	175.56	0.00
SMT-1	2200	10 YR	8.24	175.64	175.64	0.00
SMT-1	2200	25 YR	10.67	175.73	175.73	0.00
SMT-1	2200	50 YR	12.82	175.79	175.79	0.00
SMT-1	2200	100 YR	14.98	175.95	175.95	0.00
SMT-1	2200	REG	17.26	176.40	176.40	0.00
SMT-1	2180	2 YR	3.63	175.17	175.17	0.00
SMT-1	2180	5 YR	6.34	175.32	175.32	0.00
SMT-1	2180	10 YR	8.24	175.40	175.40	0.00
SMT-1	2180	25 YR	10.67	175.49	175.49	0.00
SMT-1	2180	50 YR	12.82	175.55	175.55	0.00
SMT-1	2180	100 YR	14.98	175.90	175.90	0.00
SMT-1	2180	REG	17.26	176.39	176.39	0.00
SMT-1	2050	2 YR	4.61	174.56	174.56	0.00
SMT-1	2050	5 YR	8.07	174.77	174.77	0.00
SMT-1	2050	10 YR	10.50	174.97	174.97	0.00
SMT-1	2050	25 YR	13.66	175.27	175.27	0.00
SMT-1	2050	50 YR	16.37	175.50	175.50	0.00
SMT-1	2050	100 YR	19.10	175.90	175.90	0.00
SMT-1	2050	REG	21.52	176.38	176.38	0.00
SMT-1	2040	2 YR	4.61	174.46	174.46	0.00
SMT-1	2040	5 YR	8.07	174.70	174.70	0.00
SMT-1	2040	10 YR	10.50	174.94	174.94	0.00
SMT-1	2040	25 YR	13.66	175.26	175.26	0.00
SMT-1	2040	50 YR	16.37	175.49	175.49	0.00
SMT-1	2040	100 YR	19.10	175.89	175.89	0.00
SMT-1	2040	REG	21.52	176.38	176.38	0.00
SMT-1	2000	2 YR	6.82	174.18	174.18	0.00
SMT-1	2000	5 YR	11.98	174.60	174.60	0.00
SMT-1	2000	10 YR	15.56	174.88	174.88	0.00
SMT-1	2000	25 YR	20.16	175.23	175.23	0.00
SMT-1	2000	50 YR	23.25	175.47	175.47	0.00
SMT-1	2000	100 YR	27.73	175.89	175.89	0.00
SMT-1	2000	REG	32.10	176.38	176.38	0.00



S. LLEWELLYN & ASSOCIATES LIMITED
CONSULTING ENGINEERS

Page 4

Therefore, the proposed crossing does not present an increased flooding risk to life or property.

S. Llewellyn & Associates Limited.

S. DeGrow, Dipl.T



Steven Frankovich, P.Eng.



S. LLEWELLYN & ASSOCIATES LIMITED
CONSULTING ENGINEERS

APPENDIX A

HEC-RAS-ORIGINAL AMEC OUTPUT

HEC-RAS Plan: PROP_RVA_2.1 Locations: User Defined

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
SMT-1	UPPER	2600	2 YR	2.76	178.00	178.49	178.44	178.54	0.005158	1.15	4.36	31.13	0.64
SMT-1	UPPER	2600	5 YR	4.83	178.00	178.61		178.66	0.003718	1.21	8.68	37.20	0.57
SMT-1	UPPER	2600	10 YR	6.30	178.00	178.68		178.73	0.003416	1.27	11.26	39.75	0.56
SMT-1	UPPER	2600	25 YR	8.20	178.00	178.75		178.81	0.003268	1.35	14.22	42.49	0.56
SMT-1	UPPER	2600	50 YR	10.15	178.00	178.81		178.87	0.003222	1.43	16.96	44.88	0.56
SMT-1	UPPER	2600	100 YR	11.71	178.00	178.86		178.92	0.003193	1.49	19.08	46.64	0.57
SMT-1	UPPER	2600	REG	12.67	178.00	178.89		178.95	0.003181	1.53	20.33	47.64	0.57
SMT-1	UPPER	2565	2 YR	2.76	177.80	178.31		178.37	0.004890	1.28	4.23	20.74	0.64
SMT-1	UPPER	2565	5 YR	4.83	177.80	178.40	178.36	178.50	0.006644	1.70	6.21	25.37	0.77
SMT-1	UPPER	2565	10 YR	6.30	177.80	178.46	178.42	178.57	0.006864	1.86	7.83	28.61	0.80
SMT-1	UPPER	2565	25 YR	8.20	177.80	178.53	178.49	178.66	0.006777	2.00	9.99	32.18	0.81
SMT-1	UPPER	2565	50 YR	10.15	177.80	178.59		178.73	0.006456	2.09	12.29	35.18	0.80
SMT-1	UPPER	2565	100 YR	11.71	177.80	178.65		178.78	0.006117	2.14	14.23	37.53	0.79
SMT-1	UPPER	2565	REG	12.67	177.80	178.68		178.81	0.005922	2.17	15.43	38.91	0.78
SMT-1	UPPER	2530	2 YR	2.76	177.50	177.98	177.97	178.09	0.013476	1.49	1.85	7.70	0.97
SMT-1	UPPER	2530	5 YR	4.83	177.50	178.15	178.09	178.25	0.006677	1.46	4.07	18.22	0.74
SMT-1	UPPER	2530	10 YR	6.30	177.50	178.24	178.16	178.34	0.005329	1.50	5.92	23.21	0.69
SMT-1	UPPER	2530	25 YR	8.20	177.50	178.33	178.23	178.44	0.004456	1.54	8.42	28.62	0.65
SMT-1	UPPER	2530	50 YR	10.15	177.50	178.43		178.53	0.003743	1.56	11.33	33.85	0.61
SMT-1	UPPER	2530	100 YR	11.71	177.50	178.50		178.60	0.003274	1.56	13.93	37.91	0.58
SMT-1	UPPER	2530	REG	12.67	177.50	178.54		178.64	0.002984	1.55	15.65	39.36	0.56
SMT-1	UPPER	2485	2 YR	2.76	176.82	177.50	177.43	177.62	0.005856	1.78	2.93	9.00	0.74
SMT-1	UPPER	2485	5 YR	4.83	176.82	177.62	177.61	177.83	0.008310	2.40	4.14	10.71	0.91
SMT-1	UPPER	2485	10 YR	6.30	176.82	177.71	177.71	177.96	0.008736	2.66	5.13	11.94	0.95
SMT-1	UPPER	2485	25 YR	8.20	176.82	177.82	177.82	178.09	0.008457	2.85	6.56	13.52	0.95
SMT-1	UPPER	2485	50 YR	10.15	176.82	177.92	177.92	178.21	0.008396	3.04	7.93	14.87	0.97
SMT-1	UPPER	2485	100 YR	11.71	176.82	177.98	177.98	178.30	0.008667	3.21	8.87	15.72	0.99
SMT-1	UPPER	2485	REG	12.67	176.82	178.01	178.01	178.35	0.008930	3.33	9.38	16.22	1.01
SMT-1	UPPER	2445	2 YR	2.76	176.80	177.18	177.18	177.30	0.012237	1.57	2.20	12.05	0.95
SMT-1	UPPER	2445	5 YR	4.83	176.80	177.29	177.29	177.45	0.010592	1.83	3.80	15.97	0.93
SMT-1	UPPER	2445	10 YR	6.30	176.80	177.36	177.36	177.53	0.009884	1.97	4.96	18.29	0.93
SMT-1	UPPER	2445	25 YR	8.20	176.80	177.44	177.44	177.63	0.009499	2.13	6.39	20.79	0.93
SMT-1	UPPER	2445	50 YR	10.15	176.80	177.50	177.50	177.71	0.009083	2.25	7.88	23.15	0.93
SMT-1	UPPER	2445	100 YR	11.71	176.80	177.56	177.56	177.77	0.008708	2.33	9.13	25.21	0.92
SMT-1	UPPER	2445	REG	12.67	176.80	177.58	177.58	177.81	0.008606	2.38	9.85	26.32	0.92
SMT-1	UPPER	2415	2 YR	2.76	176.50	176.92		176.98	0.004343	1.10	3.03	13.89	0.59
SMT-1	UPPER	2415	5 YR	4.83	176.50	177.05		177.13	0.004351	1.34	5.09	18.88	0.62
SMT-1	UPPER	2415	10 YR	6.30	176.50	177.12		177.22	0.004420	1.48	6.49	21.52	0.64
SMT-1	UPPER	2415	25 YR	8.20	176.50	177.20		177.31	0.004398	1.62	8.33	24.56	0.65
SMT-1	UPPER	2415	50 YR	10.15	176.50	177.27		177.39	0.004404	1.74	10.16	27.18	0.66
SMT-1	UPPER	2415	100 YR	11.71	176.50	177.32		177.45	0.004441	1.83	11.56	28.89	0.67
SMT-1	UPPER	2415	REG	12.67	176.50	177.35		177.49	0.004448	1.88	12.41	29.89	0.68
SMT-1	UPPER	2320	2 YR	2.76	175.75	176.19	176.19	176.34	0.011851	1.74	1.85	7.84	0.96
SMT-1	UPPER	2320	5 YR	4.83	175.75	176.34	176.34	176.53	0.009785	2.02	3.27	11.99	0.93
SMT-1	UPPER	2320	10 YR	6.30	175.75	176.43	176.43	176.64	0.008713	2.13	4.50	15.15	0.90
SMT-1	UPPER	2320	25 YR	8.20	175.75	176.53	176.53	176.75	0.008097	2.28	6.08	18.56	0.89
SMT-1	UPPER	2320	50 YR	10.15	175.75	176.61	176.61	176.85	0.007611	2.39	7.80	21.88	0.88
SMT-1	UPPER	2320	100 YR	11.71	175.75	176.67	176.67	176.92	0.007325	2.47	9.20	24.26	0.88
SMT-1	UPPER	2320	REG	12.67	175.75	176.71	176.71	176.96	0.007168	2.51	10.06	25.62	0.87
SMT-1	MID	2200	2 YR	3.63	174.75	175.39		175.43	0.001690	0.92	6.62	27.38	0.40
SMT-1	MID	2200	5 YR	6.34	174.75	175.56		175.60	0.001653	1.09	12.38	40.84	0.41
SMT-1	MID	2200	10 YR	8.24	174.75	175.64		175.69	0.001675	1.18	16.03	46.26	0.42
SMT-1	MID	2200	25 YR	10.67	174.75	175.73	175.49	175.78	0.001739	1.28	20.28	51.86	0.43
SMT-1	MID	2200	50 YR	12.82	174.75	175.79	175.55	175.85	0.001802	1.37	23.76	56.21	0.45
SMT-1	MID	2200	100 YR	14.98	174.75	175.95		175.99	0.001182	1.23	33.47	67.13	0.37
SMT-1	MID	2200	REG	17.26	174.75	176.40		176.41	0.000284	0.76	69.84	92.15	0.19
SMT-1	MID	2180	2 YR	3.63	174.75	175.17	175.17	175.31	0.011158	1.70	2.57	12.16	0.93
SMT-1	MID	2180	5 YR	6.34	174.75	175.32	175.32	175.49	0.009071	1.95	4.85	20.86	0.89
SMT-1	MID	2180	10 YR	8.24	174.75	175.40	175.40	175.58	0.007844	2.02	7.02	28.66	0.86
SMT-1	MID	2180	25 YR	10.67	174.75	175.49	175.49	175.68	0.006950	2.10	10.03	36.83	0.83
SMT-1	MID	2180	50 YR	12.82	174.75	175.55	175.55	175.74	0.006848	2.21	12.29	40.70	0.83
SMT-1	MID	2180	100 YR	14.98	174.75	175.90		175.95	0.001476	1.33	30.21	63.67	0.41
SMT-1	MID	2180	REG	17.26	174.75	176.39		176.40	0.000293	0.76	69.02	91.73	0.20
SMT-1	MID2	2050	2 YR	4.61	173.75	174.56		174.63	0.003115	1.44	6.55	19.76	0.55
SMT-1	MID2	2050	5 YR	8.07	173.75	174.77		174.86	0.002838	1.64	11.73	27.43	0.55
SMT-1	MID2	2050	10 YR	10.50	173.75	174.97		175.04	0.001923	1.54	17.36	31.22	0.47
SMT-1	MID2	2050	25 YR	13.66	173.75	175.27		175.31	0.001045	1.33	27.72	37.27	0.36
SMT-1	MID2	2050	50 YR	16.37	173.75	175.50		175.53	0.000748	1.25	36.75	41.84	0.31
SMT-1	MID2	2050	100 YR	19.10	173.75	175.90		175.92	0.000369	1.01	55.23	49.91	0.23
SMT-1	MID2	2050	REG	21.52	173.75	176.38		176.40	0.000177	0.81	81.82	60.21	0.16
SMT-1	MID2	2040	2 YR	4.61	173.75	174.46	174.40	174.59	0.005954	1.79	4.76	16.28	0.74
SMT-1	MID2	2040	5 YR	8.07	173.75	174.70		174.83	0.004093	1.87	9.88	25.26	0.65
SMT-1	MID2	2040	10 YR	10.50	173.75	174.94		175.01	0.002186	1.61	16.45	30.64	0.50

HEC-RAS Plan: PROP_RVA_2,1 Locations: User Defined (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
SMT-1	MID2	2040	25 YR	13.66	173.75	175.26		175.30	0.001088	1.35	27.26	37.02	0.37
SMT-1	MID2	2040	50 YR	16.37	173.75	175.49		175.53	0.000765	1.26	36.41	41.68	0.31
SMT-1	MID2	2040	100 YR	19.10	173.75	175.89		175.92	0.000372	1.02	55.03	49.83	0.23
SMT-1	MID2	2040	REG	21.52	173.75	176.38		176.39	0.000177	0.81	81.71	60.16	0.16
SMT-1	Lower	2000	2 YR	6.82	173.50	174.18	174.07	174.31	0.007470	1.66	4.42	11.15	0.71
SMT-1	Lower	2000	5 YR	11.98	173.50	174.60	174.28	174.69	0.002678	1.44	13.67	33.70	0.46
SMT-1	Lower	2000	10 YR	15.56	173.50	174.88	174.44	174.94	0.001415	1.24	24.96	45.43	0.35
SMT-1	Lower	2000	25 YR	20.16	173.50	175.23	174.58	175.27	0.000742	1.06	42.67	56.39	0.27
SMT-1	Lower	2000	50 YR	23.25	173.50	175.47	174.65	175.50	0.000503	0.96	57.26	63.85	0.22
SMT-1	Lower	2000	100 YR	27.73	173.50	175.89	174.75	175.90	0.000270	0.80	86.45	75.85	0.17
SMT-1	Lower	2000	REG	32.10	173.50	176.38	174.82	176.39	0.000144	0.67	127.35	93.65	0.13
SMT-1	Lower	800		Culvert									
SMT-4	SMT-4	385	2 YR	0.54	178.98	179.33		179.35	0.003283	0.51	1.04	5.89	0.39
SMT-4	SMT-4	385	5 YR	0.94	178.98	179.41		179.43	0.003446	0.62	1.57	8.73	0.42
SMT-4	SMT-4	385	10 YR	1.23	178.98	179.45		179.47	0.003561	0.68	1.94	10.92	0.43
SMT-4	SMT-4	385	25 YR	1.61	178.98	179.49		179.52	0.003611	0.76	2.45	14.34	0.45
SMT-4	SMT-4	385	50 YR	1.89	178.98	179.51		179.55	0.003686	0.81	2.84	16.52	0.46
SMT-4	SMT-4	385	100 YR	2.18	178.98	179.54		179.57	0.003718	0.85	3.27	18.58	0.46
SMT-4	SMT-4	385	REG	1.90	178.98	179.51		179.55	0.003691	0.81	2.85	16.56	0.46
SMT-4	SMT-4	255	2 YR	0.54	178.15	178.35	178.35	178.41	0.026649	1.02	0.53	5.18	1.02
SMT-4	SMT-4	255	5 YR	0.94	178.15	178.41	178.41	178.47	0.025173	1.10	0.86	7.20	1.01
SMT-4	SMT-4	255	10 YR	1.23	178.15	178.44	178.44	178.50	0.023765	1.13	1.09	8.36	1.00
SMT-4	SMT-4	255	25 YR	1.61	178.15	178.47	178.47	178.54	0.023633	1.19	1.35	9.49	1.01
SMT-4	SMT-4	255	50 YR	1.89	178.15	178.49	178.49	178.56	0.022911	1.22	1.54	10.27	1.01
SMT-4	SMT-4	255	100 YR	2.18	178.15	178.50	178.50	178.59	0.022912	1.29	1.69	10.83	1.02
SMT-4	SMT-4	255	REG	1.90	178.15	178.49	178.49	178.56	0.022802	1.22	1.55	10.29	1.00
SMT-4	SMT-4	160	2 YR	0.54	177.37	177.54		177.55	0.003022	0.43	1.46	12.95	0.36
SMT-4	SMT-4	160	5 YR	0.94	177.37	177.59		177.60	0.003189	0.55	2.18	15.06	0.39
SMT-4	SMT-4	160	10 YR	1.23	177.37	177.62		177.64	0.003302	0.61	2.64	16.27	0.41
SMT-4	SMT-4	160	25 YR	1.61	177.37	177.65		177.67	0.003467	0.68	3.19	17.60	0.43
SMT-4	SMT-4	160	50 YR	1.89	177.37	177.67		177.70	0.003546	0.73	3.59	18.52	0.44
SMT-4	SMT-4	160	100 YR	2.18	177.37	177.69	177.58	177.72	0.003639	0.77	3.97	19.35	0.45
SMT-4	SMT-4	160	REG	1.90	177.37	177.67		177.70	0.003549	0.73	3.60	18.54	0.44
SMT-4	SMT-4	50	2 YR	0.54	176.62	176.75	176.75	176.78	0.029702	0.80	0.67	10.35	1.00
SMT-4	SMT-4	50	5 YR	0.94	176.62	176.78	176.78	176.83	0.027142	0.93	1.02	12.59	1.00
SMT-4	SMT-4	50	10 YR	1.23	176.62	176.80	176.80	176.85	0.025754	1.00	1.27	13.96	1.00
SMT-4	SMT-4	50	25 YR	1.61	176.62	176.82	176.82	176.88	0.023421	1.08	1.57	15.26	0.98
SMT-4	SMT-4	50	50 YR	1.89	176.62	176.83	176.83	176.90	0.022688	1.14	1.78	16.10	0.99
SMT-4	SMT-4	50	100 YR	2.18	176.62	176.85	176.85	176.92	0.021769	1.19	2.01	16.94	0.98
SMT-4	SMT-4	50	REG	1.90	176.62	176.83	176.83	176.90	0.022640	1.14	1.79	16.12	0.98



S. LLEWELLYN & ASSOCIATES LIMITED
CONSULTING ENGINEERS

APPENDIX B

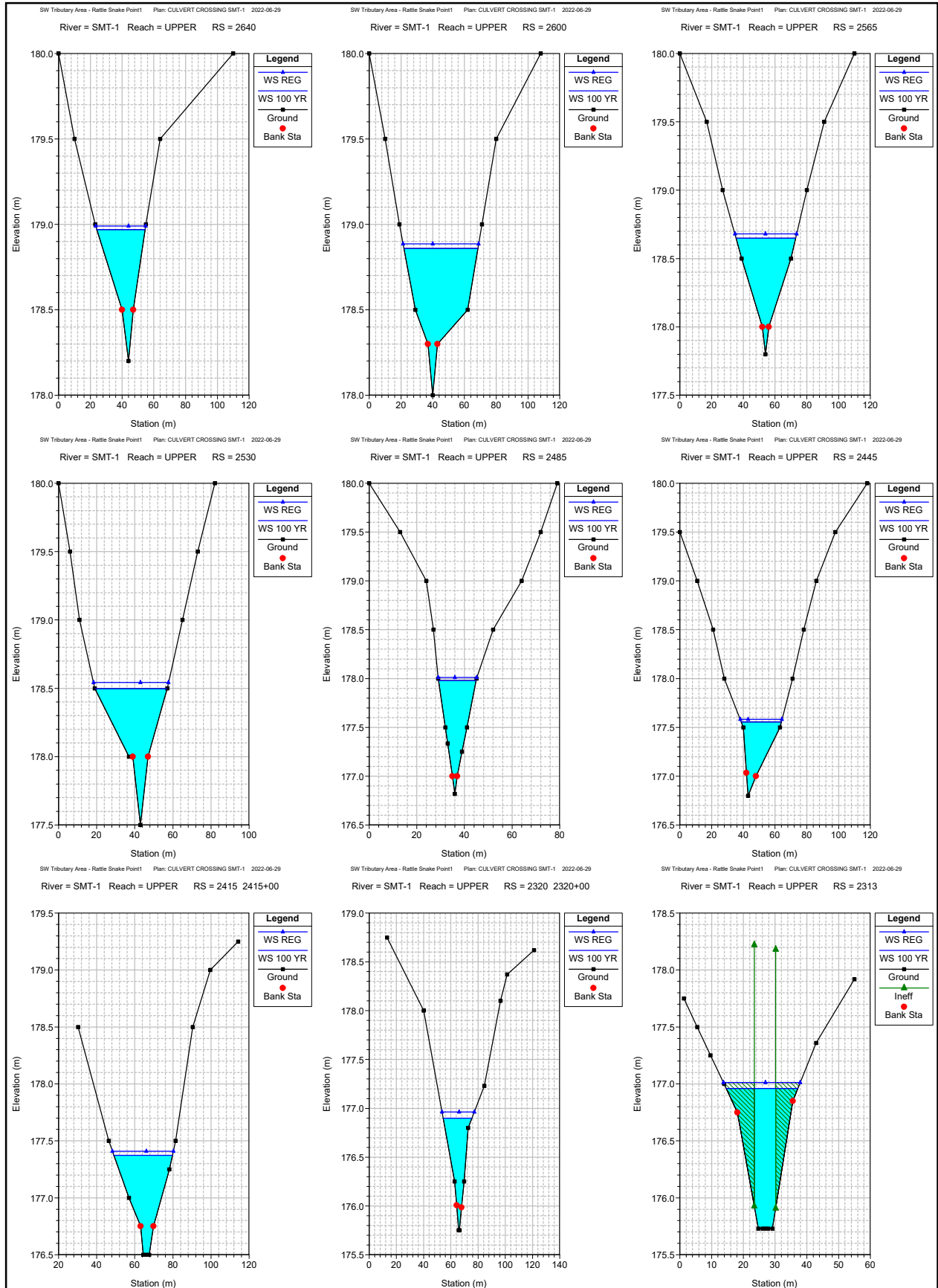
HEC-RAS PROPOSED CONDITIONS OUTPUT

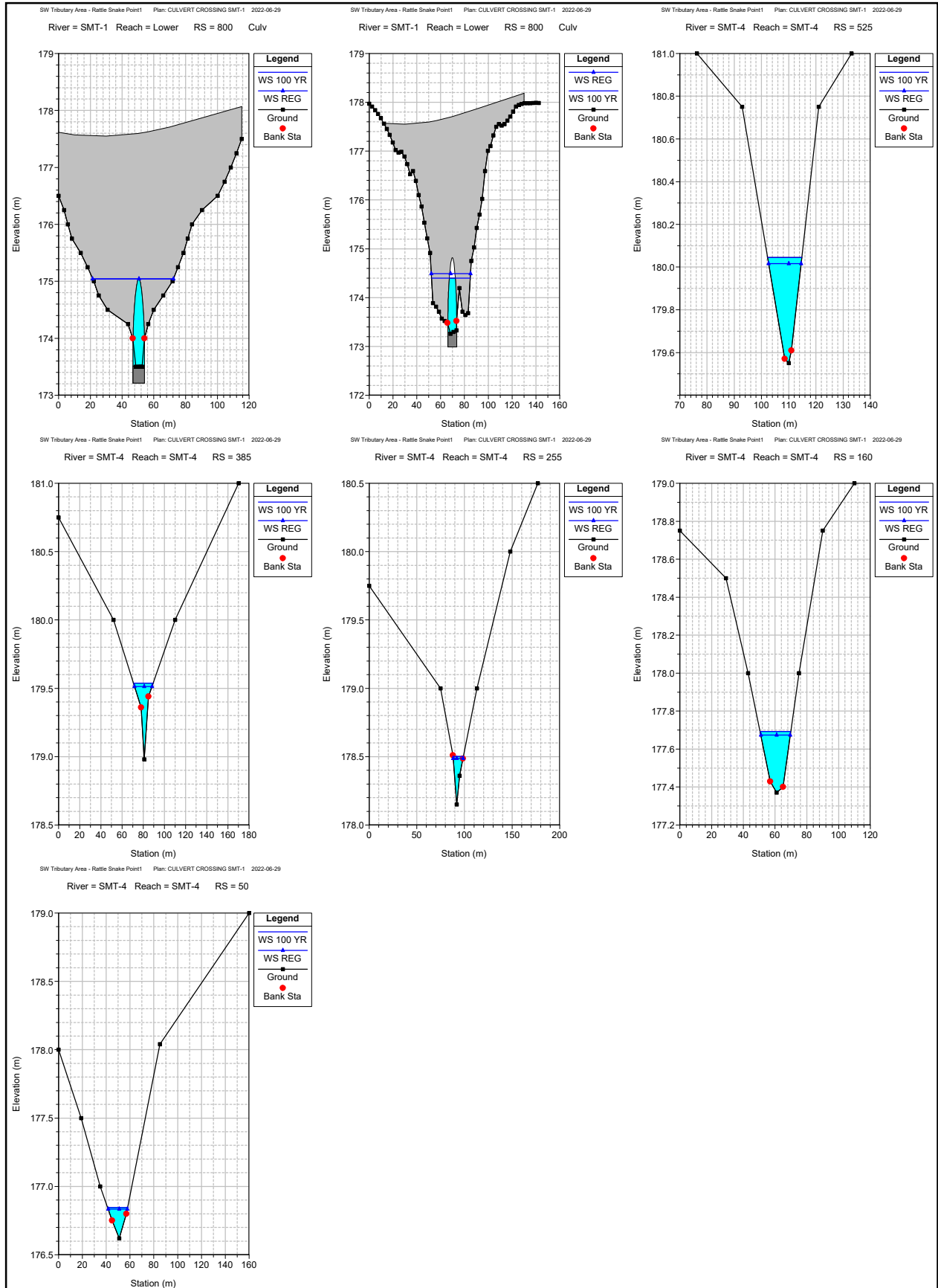
HEC-RAS Plan: CULVERT CROSSING SMT-1 Locations: User Defined

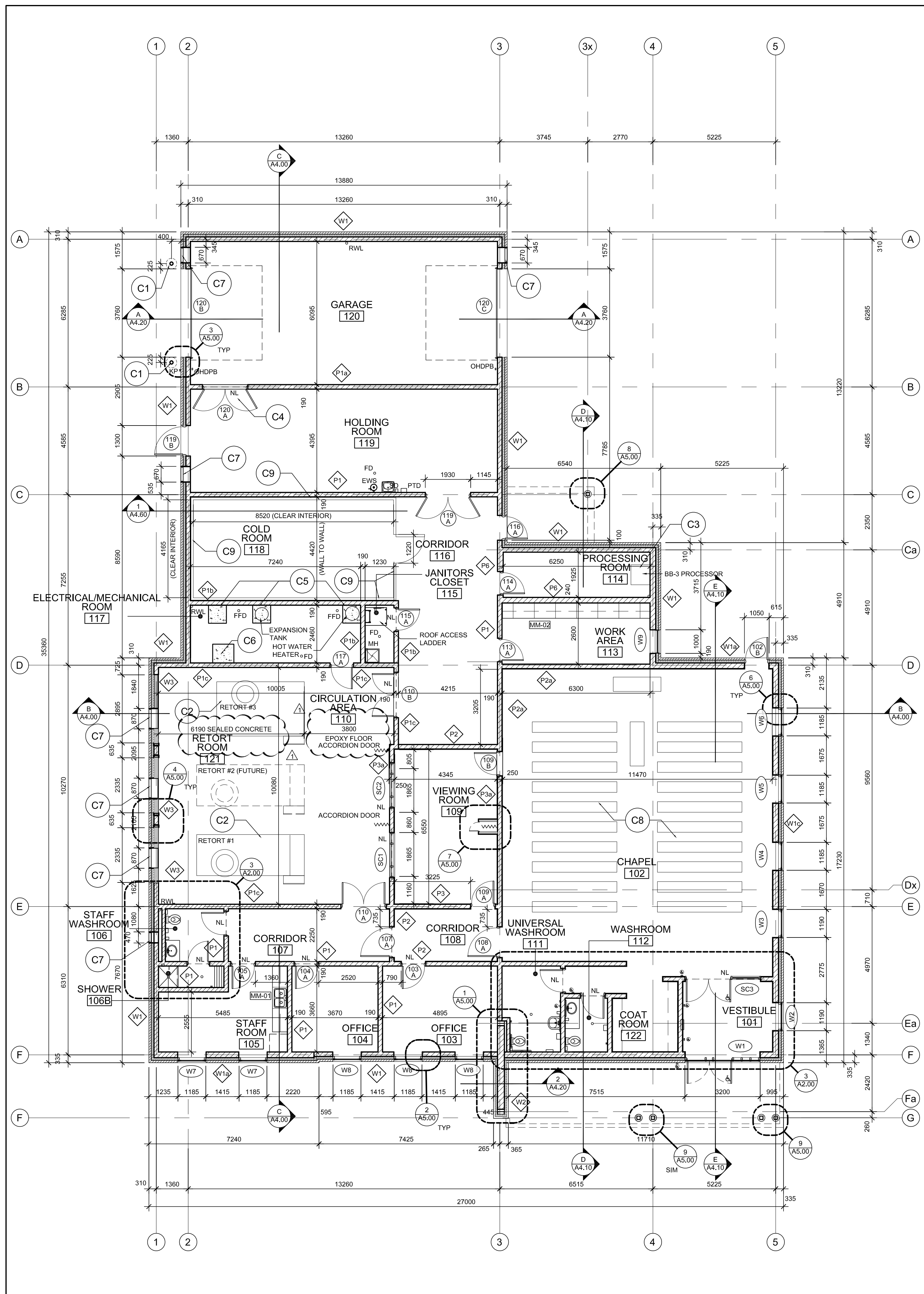
River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
SMT-1	UPPER	2640	2 YR	2.76	178.20	178.69		178.75	0.004525	1.09	3.29	16.52	0.60
SMT-1	UPPER	2640	5 YR	4.83	178.20	178.77	178.72	178.87	0.006085	1.46	4.84	20.69	0.72
SMT-1	UPPER	2640	10 YR	6.30	178.20	178.82	178.78	178.95	0.006758	1.66	5.93	23.18	0.77
SMT-1	UPPER	2640	25 YR	8.20	178.20	178.88	178.85	179.03	0.007348	1.87	7.32	26.01	0.82
SMT-1	UPPER	2640	50 YR	10.15	178.20	178.93	178.91	179.11	0.007761	2.04	8.72	28.58	0.85
SMT-1	UPPER	2640	100 YR	11.71	178.20	178.97	178.96	179.16	0.008006	2.16	9.84	30.47	0.88
SMT-1	UPPER	2640	REG	12.66	178.20	178.99	178.99	179.19	0.008155	2.23	10.50	31.53	0.89
SMT-1	UPPER	2600	2 YR	2.76	178.00	178.49	178.44	178.54	0.005165	1.15	4.35	31.12	0.64
SMT-1	UPPER	2600	5 YR	4.83	178.00	178.61		178.66	0.003717	1.21	8.68	37.20	0.57
SMT-1	UPPER	2600	10 YR	6.30	178.00	178.68		178.73	0.003416	1.27	11.26	39.75	0.56
SMT-1	UPPER	2600	25 YR	8.20	178.00	178.75		178.81	0.003268	1.35	14.22	42.49	0.56
SMT-1	UPPER	2600	50 YR	10.15	178.00	178.81		178.87	0.003222	1.43	16.96	44.88	0.56
SMT-1	UPPER	2600	100 YR	11.71	178.00	178.86		178.92	0.003193	1.49	19.08	46.64	0.57
SMT-1	UPPER	2600	REG	12.66	178.00	178.89		178.95	0.003181	1.53	20.32	47.64	0.57
SMT-1	UPPER	2565	2 YR	2.76	177.80	178.31	178.24	178.38	0.004872	1.28	4.24	20.76	0.64
SMT-1	UPPER	2565	5 YR	4.83	177.80	178.40	178.36	178.50	0.006646	1.70	6.21	25.37	0.77
SMT-1	UPPER	2565	10 YR	6.30	177.80	178.46	178.42	178.57	0.006864	1.86	7.83	28.61	0.80
SMT-1	UPPER	2565	25 YR	8.20	177.80	178.53	178.49	178.66	0.006777	2.00	9.99	32.18	0.81
SMT-1	UPPER	2565	50 YR	10.15	177.80	178.59		178.73	0.006456	2.09	12.29	35.18	0.80
SMT-1	UPPER	2565	100 YR	11.71	177.80	178.65		178.78	0.006117	2.14	14.23	37.53	0.79
SMT-1	UPPER	2565	REG	12.66	177.80	178.68		178.81	0.005922	2.17	15.42	38.90	0.78
SMT-1	UPPER	2530	2 YR	2.76	177.50	177.98	177.97	178.09	0.013605	1.49	1.84	7.68	0.97
SMT-1	UPPER	2530	5 YR	4.83	177.50	178.15	178.09	178.25	0.006676	1.46	4.07	18.22	0.74
SMT-1	UPPER	2530	10 YR	6.30	177.50	178.24	178.16	178.34	0.005329	1.50	5.92	23.21	0.69
SMT-1	UPPER	2530	25 YR	8.20	177.50	178.33	178.23	178.44	0.004456	1.54	8.42	28.62	0.65
SMT-1	UPPER	2530	50 YR	10.15	177.50	178.43		178.53	0.003743	1.56	11.33	33.85	0.61
SMT-1	UPPER	2530	100 YR	11.71	177.50	178.50		178.60	0.003274	1.56	13.93	37.91	0.58
SMT-1	UPPER	2530	REG	12.66	177.50	178.54		178.64	0.002984	1.55	15.64	39.36	0.56
SMT-1	UPPER	2485	2 YR	2.76	176.82	177.50	177.43	177.62	0.005823	1.77	2.94	9.01	0.74
SMT-1	UPPER	2485	5 YR	4.83	176.82	177.62	177.61	177.83	0.008310	2.40	4.14	10.71	0.91
SMT-1	UPPER	2485	10 YR	6.30	176.82	177.71	177.71	177.96	0.008736	2.66	5.13	11.94	0.95
SMT-1	UPPER	2485	25 YR	8.20	176.82	177.82	177.82	178.09	0.008457	2.85	6.56	13.52	0.95
SMT-1	UPPER	2485	50 YR	10.15	176.82	177.92	177.92	178.21	0.008396	3.04	7.93	14.87	0.97
SMT-1	UPPER	2485	100 YR	11.71	176.82	177.98	177.98	178.30	0.008667	3.21	8.87	15.72	0.99
SMT-1	UPPER	2485	REG	12.66	176.82	178.01	178.01	178.35	0.008937	3.33	9.37	16.21	1.01
SMT-1	UPPER	2445	2 YR	2.76	176.80	177.18	177.18	177.30	0.012237	1.57	2.20	12.05	0.95
SMT-1	UPPER	2445	5 YR	4.83	176.80	177.29	177.29	177.45	0.010592	1.83	3.80	15.97	0.93
SMT-1	UPPER	2445	10 YR	6.30	176.80	177.36	177.36	177.53	0.009884	1.97	4.96	18.29	0.93
SMT-1	UPPER	2445	25 YR	8.20	176.80	177.44	177.44	177.63	0.009499	2.13	6.39	20.79	0.93
SMT-1	UPPER	2445	50 YR	10.15	176.80	177.50	177.50	177.71	0.009083	2.25	7.88	23.15	0.93
SMT-1	UPPER	2445	100 YR	11.71	176.80	177.56	177.56	177.77	0.008708	2.33	9.13	25.21	0.92
SMT-1	UPPER	2445	REG	12.66	176.80	177.58	177.58	177.81	0.008607	2.38	9.84	26.31	0.92
SMT-1	UPPER	2415	2 YR	2.76	176.50	176.93		176.98	0.004162	1.08	3.09	14.06	0.58
SMT-1	UPPER	2415	5 YR	4.83	176.50	177.05		177.14	0.004102	1.32	5.23	19.17	0.60
SMT-1	UPPER	2415	10 YR	6.30	176.50	177.13		177.22	0.003946	1.43	6.84	22.13	0.61
SMT-1	UPPER	2415	25 YR	8.20	176.50	177.22		177.32	0.003894	1.55	8.82	25.31	0.62
SMT-1	UPPER	2415	50 YR	10.15	176.50	177.30		177.41	0.003628	1.63	11.11	28.36	0.61
SMT-1	UPPER	2415	100 YR	11.71	176.50	177.37		177.48	0.003320	1.66	13.21	30.79	0.59
SMT-1	UPPER	2415	REG	12.66	176.50	177.41		177.52	0.003249	1.69	14.32	32.01	0.59
SMT-1	UPPER	2320	2 YR	2.76	175.75	176.26	176.24	176.41	0.009341	1.76	1.97	7.35	0.88
SMT-1	UPPER	2320	5 YR	4.83	175.75	176.45	176.41	176.63	0.007202	1.99	3.65	10.75	0.82
SMT-1	UPPER	2320	10 YR	6.30	175.75	176.56	176.51	176.75	0.006471	2.10	4.91	12.72	0.80
SMT-1	UPPER	2320	25 YR	8.20	175.75	176.70	176.61	176.89	0.005348	2.16	6.86	15.27	0.75
SMT-1	UPPER	2320	50 YR	10.15	175.75	176.81	176.71	177.01	0.004882	2.25	8.75	17.67	0.73
SMT-1	UPPER	2320	100 YR	11.71	175.75	176.90	176.77	177.11	0.004649	2.32	10.45	21.22	0.73
SMT-1	UPPER	2320	REG	12.66	175.75	176.96	176.78	177.16	0.004286	2.32	11.83	23.71	0.70
SMT-1	UPPER	2313	2 YR	2.76	175.73	176.34	176.02	176.37	0.000929	0.71	3.91	11.90	0.30
SMT-1	UPPER	2313	5 YR	4.83	175.73	176.54	176.14	176.58	0.001100	0.93	5.19	14.23	0.34
SMT-1	UPPER	2313	10 YR	6.30	175.73	176.64	176.21	176.70	0.001219	1.07	5.91	15.53	0.36
SMT-1	UPPER	2313	25 YR	8.20	175.73	176.77	176.30	176.84	0.001319	1.21	6.76	17.28	0.39
SMT-1	UPPER	2313	50 YR	10.15	175.73	176.88	176.38	176.97	0.001441	1.36	7.48	19.92	0.41
SMT-1	UPPER	2313	100 YR	11.71	175.73	176.96	176.44	177.07	0.001511	1.46	8.04	22.52	0.43
SMT-1	UPPER	2313	REG	12.66	175.73	177.01	176.47	177.13	0.001530	1.51	8.39	24.16	0.43
SMT-1	UPPER	2308		Culvert									
SMT-1	UPPER	2290	2 YR	2.76	175.63	176.30	176.03	176.34	0.001974	0.97	2.87	7.60	0.42
SMT-1	UPPER	2290	5 YR	4.83	175.63	176.45	176.19	176.54	0.002577	1.30	3.86	12.65	0.50
SMT-1	UPPER	2290	10 YR	6.30	175.63	176.53	176.28	176.65	0.003053	1.52	4.39	15.08	0.55
SMT-1	UPPER	2290	25 YR	8.20	175.63	176.61	176.39	176.77	0.003662	1.78	4.94	17.88	0.61
SMT-1	UPPER	2290	50 YR	10.15	175.63	176.66	176.49	176.88	0.004617	2.08	5.28	19.61	0.70
SMT-1	UPPER	2290	100 YR	11.71	175.63	176.69	176.56	176.96	0.005503	2.32	5.48	20.65	0.77
SMT-1	UPPER	2290	REG	12.66	175.63	176.71	176.60	177.01	0.005963	2.45	5.62	21.37	0.80
SMT-1	UPPER	2269	2 YR	2.76	175.54	176.11	176.11	176.25	0.013954	1.67	1.65	5.82	1.01

HEC-RAS Plan: CULVERT CROSSING SMT-1 Locations: User Defined (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
SMT-1	UPPER	2269	5 YR	4.83	175.54	176.24	176.24	176.43	0.013317	1.89	2.55	7.25	1.02
SMT-1	UPPER	2269	10 YR	6.30	175.54	176.32	176.32	176.53	0.011591	2.01	3.21	9.55	0.98
SMT-1	UPPER	2269	25 YR	8.20	175.54	176.41	176.41	176.64	0.010700	2.17	4.10	12.09	0.97
SMT-1	UPPER	2269	50 YR	10.15	175.54	176.50	176.50	176.75	0.009033	2.23	5.45	16.71	0.92
SMT-1	UPPER	2269	100 YR	11.71	175.54	176.56	176.56	176.82	0.008468	2.31	6.55	19.81	0.90
SMT-1	UPPER	2269	REG	12.66	175.54	176.59	176.59	176.86	0.008170	2.34	7.26	21.59	0.89
SMT-1	MID	2200	2 YR	3.63	174.75	175.39		175.43	0.001690	0.92	6.62	27.38	0.40
SMT-1	MID	2200	5 YR	6.34	174.75	175.56		175.60	0.001653	1.09	12.38	40.84	0.41
SMT-1	MID	2200	10 YR	8.24	174.75	175.64		175.69	0.001675	1.18	16.03	46.26	0.42
SMT-1	MID	2200	25 YR	10.67	174.75	175.73	175.49	175.78	0.001739	1.28	20.28	51.86	0.43
SMT-1	MID	2200	50 YR	12.82	174.75	175.79	175.55	175.85	0.001802	1.37	23.76	56.21	0.45
SMT-1	MID	2200	100 YR	14.98	174.75	175.95		175.99	0.001182	1.23	33.47	67.13	0.47
SMT-1	MID	2200	REG	17.26	174.75	176.40		176.41	0.000284	0.76	69.84	92.15	0.19
SMT-1	MID	2180	2 YR	3.63	174.75	175.17	175.17	175.31	0.011158	1.70	2.57	12.16	0.93
SMT-1	MID	2180	5 YR	6.34	174.75	175.32	175.32	175.49	0.009071	1.95	4.85	20.86	0.89
SMT-1	MID	2180	10 YR	8.24	174.75	175.40	175.40	175.58	0.007844	2.02	7.02	28.66	0.86
SMT-1	MID	2180	25 YR	10.67	174.75	175.49	175.49	175.68	0.006950	2.10	10.03	36.83	0.83
SMT-1	MID	2180	50 YR	12.82	174.75	175.55	175.55	175.74	0.006848	2.21	12.29	40.70	0.83
SMT-1	MID	2180	100 YR	14.98	174.75	175.90		175.95	0.001476	1.33	30.21	63.67	0.41
SMT-1	MID	2180	REG	17.26	174.75	176.39		176.40	0.000293	0.76	69.02	91.73	0.20
SMT-1	MID2	2050	2 YR	4.61	173.75	174.56		174.63	0.003115	1.44	6.55	19.76	0.55
SMT-1	MID2	2050	5 YR	8.07	173.75	174.77		174.86	0.002838	1.64	11.73	27.43	0.55
SMT-1	MID2	2050	10 YR	10.50	173.75	174.97		175.04	0.001923	1.54	17.36	31.22	0.47
SMT-1	MID2	2050	25 YR	13.66	173.75	175.27		175.31	0.001045	1.33	27.72	37.27	0.36
SMT-1	MID2	2050	50 YR	16.37	173.75	175.50		175.53	0.000748	1.25	36.75	41.84	0.31
SMT-1	MID2	2050	100 YR	19.10	173.75	175.90		175.92	0.000369	1.01	55.23	49.91	0.23
SMT-1	MID2	2050	REG	21.52	173.75	176.38		176.40	0.000177	0.81	81.82	60.21	0.16
SMT-1	MID2	2040	2 YR	4.61	173.75	174.46	174.40	174.59	0.005954	1.79	4.76	16.28	0.74
SMT-1	MID2	2040	5 YR	8.07	173.75	174.70		174.83	0.004093	1.87	9.88	25.26	0.65
SMT-1	MID2	2040	10 YR	10.50	173.75	174.94		175.01	0.002186	1.61	16.45	30.64	0.50
SMT-1	MID2	2040	25 YR	13.66	173.75	175.26		175.30	0.001088	1.35	27.26	37.02	0.37
SMT-1	MID2	2040	50 YR	16.37	173.75	175.49		175.53	0.000765	1.26	36.41	41.68	0.31
SMT-1	MID2	2040	100 YR	19.10	173.75	175.89		175.92	0.000372	1.02	55.03	49.83	0.23
SMT-1	MID2	2040	REG	21.52	173.75	176.38		176.39	0.000177	0.81	81.71	60.16	0.16
SMT-1	Lower	2000	2 YR	6.82	173.50	174.18	174.07	174.31	0.007470	1.66	4.42	11.15	0.71
SMT-1	Lower	2000	5 YR	11.98	173.50	174.60	174.28	174.69	0.002678	1.44	13.67	33.70	0.46
SMT-1	Lower	2000	10 YR	15.56	173.50	174.88	174.44	174.94	0.001415	1.24	24.96	45.43	0.35
SMT-1	Lower	2000	25 YR	20.16	173.50	175.23	174.58	175.27	0.000742	1.06	42.67	56.39	0.27
SMT-1	Lower	2000	50 YR	23.25	173.50	175.47	174.65	175.50	0.000503	0.96	57.26	63.85	0.22
SMT-1	Lower	2000	100 YR	27.73	173.50	175.89	174.75	175.90	0.000270	0.80	86.45	75.85	0.17
SMT-1	Lower	2000	REG	32.10	173.50	176.38	174.82	176.39	0.000144	0.67	127.35	93.65	0.13
SMT-1	Lower	800		Culvert									
SMT-4	SMT-4	385	2 YR	0.54	178.98	179.33		179.35	0.003283	0.51	1.04	5.89	0.39
SMT-4	SMT-4	385	5 YR	0.94	178.98	179.41		179.43	0.003446	0.62	1.57	8.73	0.42
SMT-4	SMT-4	385	10 YR	1.23	178.98	179.45		179.47	0.003561	0.68	1.94	10.92	0.43
SMT-4	SMT-4	385	25 YR	1.61	178.98	179.49		179.52	0.003611	0.76	2.45	14.34	0.45
SMT-4	SMT-4	385	50 YR	1.89	178.98	179.51		179.55	0.003686	0.81	2.84	16.52	0.46
SMT-4	SMT-4	385	100 YR	2.18	178.98	179.54		179.57	0.003718	0.85	3.27	18.58	0.46
SMT-4	SMT-4	385	REG	1.90	178.98	179.51		179.55	0.003691	0.81	2.85	16.56	0.46
SMT-4	SMT-4	255	2 YR	0.54	178.15	178.35	178.35	178.41	0.026649	1.02	0.53	5.18	1.02
SMT-4	SMT-4	255	5 YR	0.94	178.15	178.41	178.41	178.47	0.025173	1.10	0.86	7.20	1.01
SMT-4	SMT-4	255	10 YR	1.23	178.15	178.44	178.44	178.50	0.023765	1.13	1.09	8.36	1.00
SMT-4	SMT-4	255	25 YR	1.61	178.15	178.47	178.47	178.54	0.023633	1.19	1.35	9.49	1.01
SMT-4	SMT-4	255	50 YR	1.89	178.15	178.49	178.49	178.56	0.022911	1.22	1.54	10.27	1.01
SMT-4	SMT-4	255	100 YR	2.18	178.15	178.50	178.50	178.59	0.022912	1.29	1.69	10.83	1.02
SMT-4	SMT-4	255	REG	1.90	178.15	178.49	178.49	178.56	0.022802	1.22	1.55	10.29	1.00
SMT-4	SMT-4	160	2 YR	0.54	177.37	177.54		177.55	0.003022	0.43	1.46	12.95	0.36
SMT-4	SMT-4	160	5 YR	0.94	177.37	177.59		177.60	0.003189	0.55	2.18	15.06	0.39
SMT-4	SMT-4	160	10 YR	1.23	177.37	177.62		177.64	0.003302	0.61	2.64	16.27	0.41
SMT-4	SMT-4	160	25 YR	1.61	177.37	177.65		177.67	0.003467	0.68	3.19	17.60	0.43
SMT-4	SMT-4	160	50 YR	1.89	177.37	177.67		177.70	0.003546	0.73	3.59	18.52	0.44
SMT-4	SMT-4	160	100 YR	2.18	177.37	177.69	177.58	177.72	0.003639	0.77	3.97	19.35	0.45
SMT-4	SMT-4	160	REG	1.90	177.37	177.67		177.70	0.003549	0.73	3.60	18.54	0.44
SMT-4	SMT-4	50	2 YR	0.54	176.62	176.75	176.75	176.78	0.029702	0.80	0.67	10.35	1.00
SMT-4	SMT-4	50	5 YR	0.94	176.62	176.78	176.78	176.83	0.027142	0.93	1.02	12.59	1.00
SMT-4	SMT-4	50	10 YR	1.23	176.62	176.80	176.80	176.85	0.025754	1.00	1.27	13.96	1.00
SMT-4	SMT-4	50	25 YR	1.61	176.62	176.82	176.82	176.88	0.023421	1.08	1.57	15.26	0.98
SMT-4	SMT-4	50	50 YR	1.89	176.62	176.83	176.83	176.90	0.022688	1.14	1.78	16.10	0.99
SMT-4	SMT-4	50	100 YR	2.18	176.62	176.85	176.85	176.92	0.021769	1.19	2.01	16.94	0.98
SMT-4	SMT-4	50	REG	1.90	176.62	176.83	176.83	176.90	0.022640	1.14	1.79	16.12	0.98







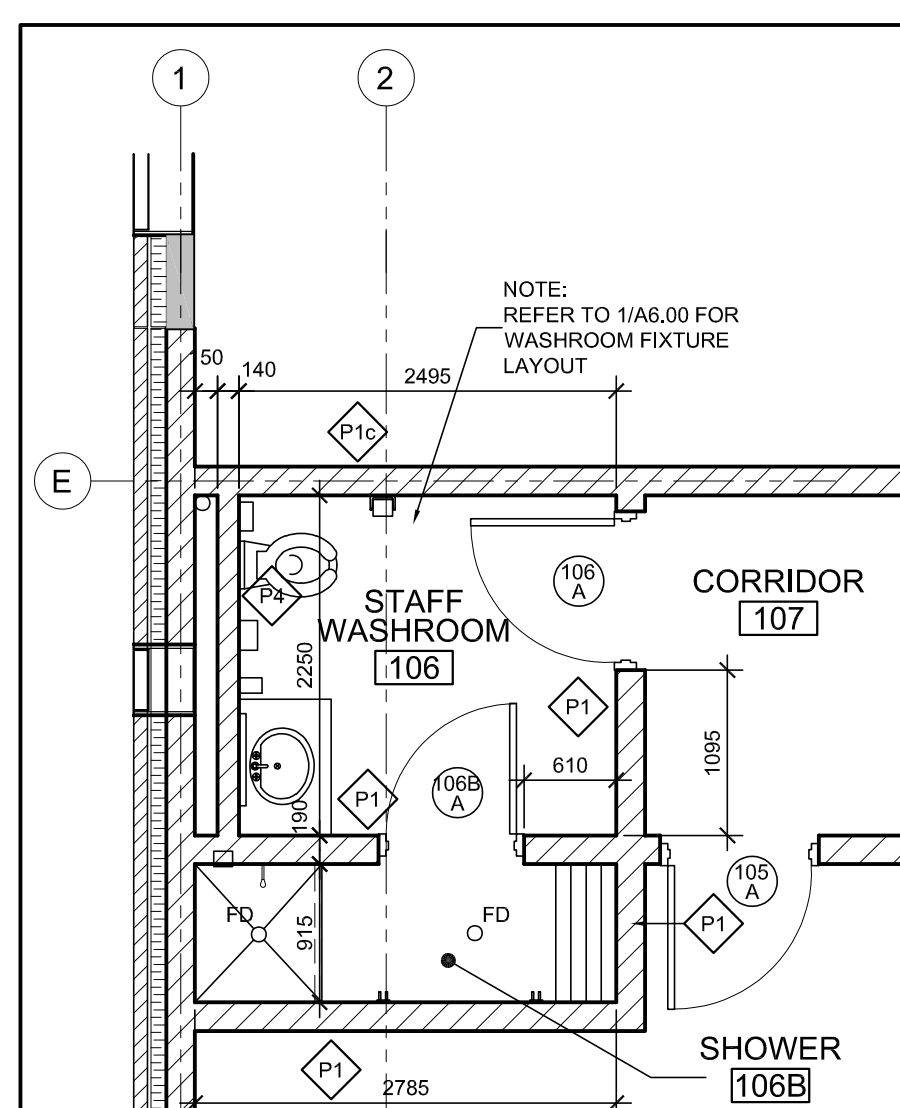
1 FLOOR PLAN
A2.00 SCALE 1:100

GENERAL NOTES

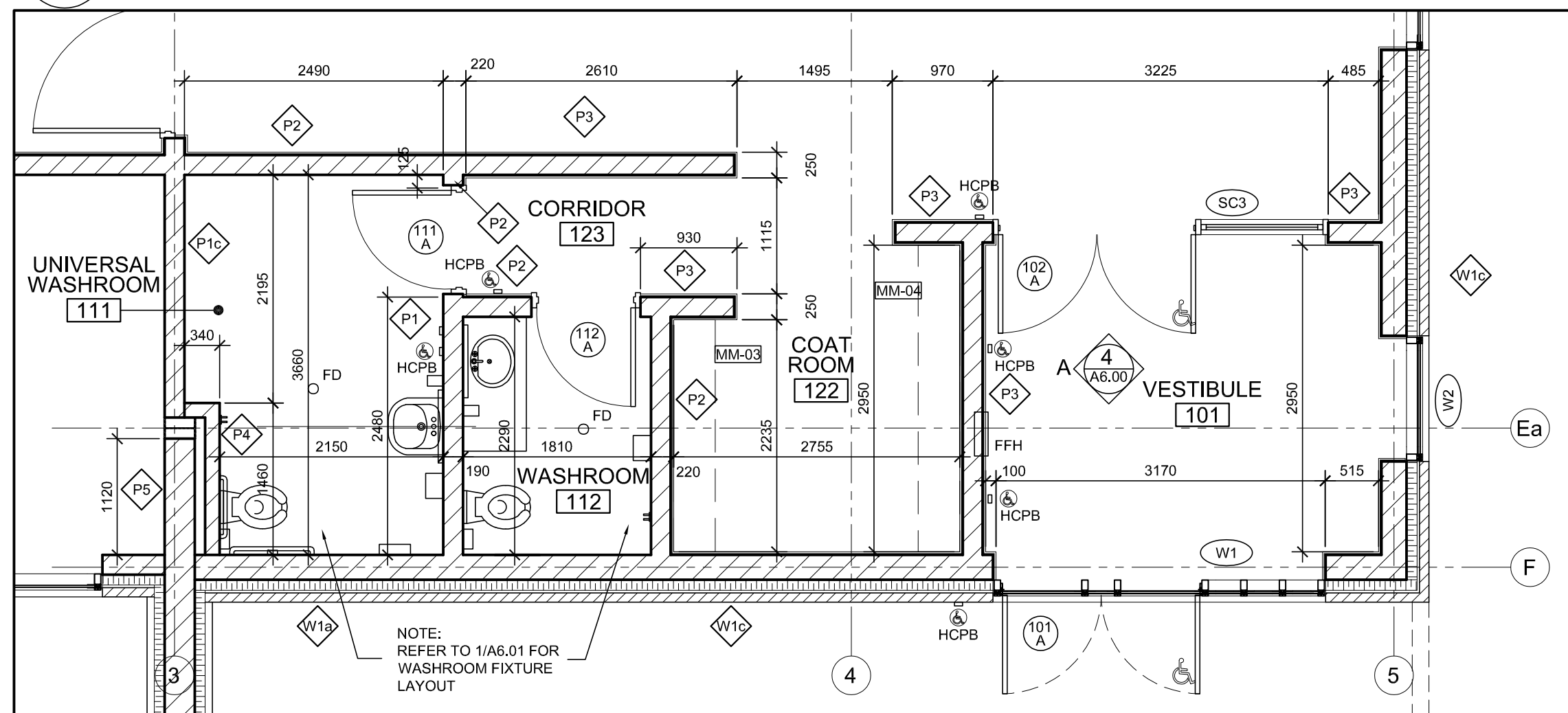
- MECHANICAL AND ELECTRICAL ITEMS SHOWN, I.E. DUCTWORK, PIPING, LIGHT FIXTURES, ETC. ARE FOR REFERENCE ONLY AND ARE NOT INCLUSIVE. REFER TO MECHANICAL AND ELECTRICAL DRAWING FOR ALL RELATED.
- CONNECTIONS OF ALL NON STRUCTURAL ELEMENTS AND EQUIPMENT TO SUPPORTING STRUCTURE TO BE DESIGNED TO COMPLY WITH ARTICLE 4.1.3.18 OF THE 2012 ONTARIO BUILDING CODE FOR SEISMIC LOADS. CONTRACTOR TO SUBMIT SHOP DRAWINGS SHOWING THESE CONNECTIONS STAMPED AND SIGNED BY A PROFESSIONAL ENGINEER IF APPLICABLE.
- TRANSITIONS BETWEEN FLOOR FINISHES TO BE MADE SMOOTH, CONTINUOUS & FLUSH. GRIND DOWN FLOOR SLAB ACROSS DOOR THRESHOLDS WHERE APPLICABLE TO SUIT THICKNESS OF MATERIALS AND ENSURE FLOOR FINISH MATERIALS ARE INSTALLED FLUSH THROUGHOUT
- APPLIANCES SHOWN IN KITCHENS, KITCHENETTES AND LAUNDRY ROOMS ARE SHOWN FOR REFERENCE. SUPPLY & INSTALL BY OTHERS, NOT IN CONTRACT, INCLUDES BUT IS NOT LIMITED TO; WASHERS, DRYERS, FRIDGES, STOVES, MICROWAVES, ETC.
- CONCRETE FLOOR SLAB TO BE SLOPED TOWARDS FLOOR DRAIN (FD) LOCATIONS. REFER TO AND COORDINATE WITH MECHANICAL DRAWINGS FOR ALL FLOOR DRAIN LOCATIONS.
- NL - DENOTES A NON-LOAD BEARING LINTEL. REFER TO STRUCTURAL DRAWINGS FOR LINTEL CONSTRUCTION.

CONSTRUCTION NOTES

- C1** 150mm DIA CONCRETE FILLED STEEL BOLLARD. REFER TO DETAIL 6A1.20
- C2** OWNER SUPPLIED RETORTS. CONTRACTOR RESPONSIBLE FOR UNLOADING OF RETORTS, MOVING THEM INTO THE BUILDING AND FINAL HOOK UPS. REFER TO AND COORDINATE W/ MECHANICAL AND ELECTRICAL DRAWINGS
- C3** OWNER SUPPLIED EQUIPMENT. CONTRACTOR RESPONSIBLE MOVING THEM INTO THE BUILDING AND FINAL HOOK UPS. REFER TO AND COORDINATE W/ MECHANICAL AND ELECTRICAL DRAWINGS
- C4** NL - DENOTES NON-LOAD BEARING LINTEL. REFER TO STRUCTURAL DRAWINGS FOR LINTEL CONSTRUCTION
- C5** 760mm X 760mm X 100MM HOUSE KEEPING PAD. REFER TO AND COORDINATE LOCATION OF PAD W/ MECHANICAL DRAWINGS.
- C6** 900mm X 800mm X 100MM HOUSE KEEPING PAD FOR FLOOR MOUNTED ELECTRICAL TRANSFORMER. REFER TO AND COORDINATE LOCATION AND SIZE OF PAD W/ ELECTRICAL DRAWINGS.
- C7** MECHANICAL LOUVRE. REFER TO AND COORDINATE LOCATION AND SIZE OF OPENING W/ MECHANICAL DRAWINGS.
- C8** CHAPEL FURNISHING SHOWN FOR INFORMATION PURPOSES ONLY. FURNISHING TO BE SUPPLIED BY OWNER
- C9** 100mm THK X 2440mm HIGH INSULATED METAL PANELS (IMP) CW/ 100mm THK IMP CEILING SUSPENDED FROM STRUCTURE ABOVE BY 10mm GALVANIZED THREADED RODS AT 1800mm O/C (MAX). PROVIDE A 1220mm X 2135mm INSULATED COLD STORAGE (ICS) DOOR CW LATCH. PROVIDE A CONTINUOUS SELF ADHERING AIR/VAPOUR BARRIER TO THE INTERIOR FACE OF THE SURROUNDING CONCRETE BLOCK WALL. PROVIDE 25mm VERTICAL METAL HAT CHANNELS AT EACH WALL PANEL JOINT.



2 ENLARGED STAFF WASHROOM FLOOR PLAN
A2.00 SCALE 1:50



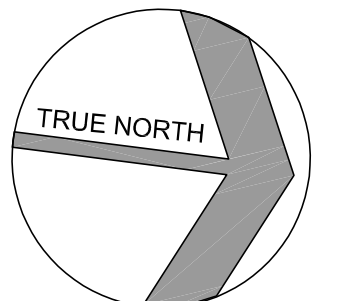
3 ENLARGED FLOOR PLAN
A2.00 SCALE 1:50

EXTERIOR WALL TYPES

NO.	DESCRIPTION	REMARKS
W1	-90mm BRICK VENEER OR -90mm ARCHITECTURAL MASONRY (AS PER ELEVATIONS & SECTIONS)	W1 190mm CONCRETE BLOCK
W1a	-25mm AIR SPACE -100mm RIGID INSULATION -AIR / VAPOUR BARRIER ON -CONC. BLOCK	W1a 240mm CONCRETE BLOCK
W1b		W1b SAME AS W1 W/ 16mm GYPSUM BOARD ON 13mm RESILIENT CHANNELS ON INTERIOR SIDE
W1c		W1c SAME AS W1a W/ 16mm GYPSUM BOARD ON 13mm RESILIENT CHANNELS ON INTERIOR SIDE
	* REFER TO ELEVATIONS FOR EXTENT OF BRICK TYPES, MASONRY & PATTERN LOCATIONS * SEE REMARKS FOR VARIATIONS OF SIMILAR TYPES	
W2	-57mm ALUMINUM COMPOSITE PANEL (CW EXTRUSION SYSTEM AND THERMAL SEPARATORS) -100mm GALV. METAL Z' SUB-GIRTS -100mm SEMI-RIGID INSULATION FILLED CAV. -AIR / VAPOUR BARRIER ON EA FACE OF -290mm CONC. BLOCK	
W3	-90mm ARCHITECTURAL MASONRY (AS PER ELEVATIONS & SECTIONS) -25mm AIR SPACE -100mm RIGID INSULATION -AIR / VAPOUR BARRIER ON -13mm EXTERIOR GRADE SHEATHING -150mm METAL STUDS @ 400mm O/C -16mm GYPSUM BOARD	W1 190mm CONCRETE BLOCK

INTERIOR WALL PARTITION TYPES

NO.	DESCRIPTION	REMARKS
P1	- 190mm CONC. BLOCK	P1a 1 1/2 hr FIRE RESISTANCE RATING (OBC SB-2 TABLE 2.1.1)
P1a		P1b 1hr FIRE RESISTANCE RATING (OBC SB-2 TABLE 2.1.1)
P1b		P1c 75% SOLID UNITS 2hr FIRE RESISTANCE RATING (OBC SB-2 TABLE 2.1.1)
P1c		• EXTEND TO U/S OF STRUCTURE ABOVE • BULL-NOSE BLOCKS AT ALL EXPOSED CORNERS
P2	- 190mm CONC. BLOCK - 13mm RESILIENT CHANNEL (HORIZONTAL) - 16mm GYPSUM BOARD	P2a 75% SOLID UNITS 2hr FIRE RESISTANCE RATING (OBC SB-2 TABLE 2.1.1)
P2a		• EXTEND TO U/S OF STRUCTURE ABOVE • BULL-NOSE BLOCKS AT ALL EXPOSED CORNERS
P3	- 16mm GYPSUM BOARD - 13mm RESILIENT CHANNEL AT 400mm O/C (HORIZONTAL) ON EA SIDE OF - 190mm CONC. BLOCK	P3a 75% SOLID UNITS 2hr FIRE RESISTANCE RATING (OBC SB-2 TABLE 2.1.1)
P3a		• EXTEND TO U/S OF STRUCTURE ABOVE • BULL-NOSE BLOCKS AT ALL EXPOSED CORNERS
P4	PLUMBING WALL -140mm CONC. BLOCK	• EXTEND TO 150mm ABOVE ADJACENT CEILING • BULL-NOSE BLOCKS AT ALL EXPOSED CORNERS
P5	-290mm CONC. BLOCK	• 2 hr FIRE RESISTANCE RATING (OBC SB-2 TABLE 2.1.1) • EXTEND TO U/S OF STRUCTURE ABOVE • BULL-NOSE BLOCKS AT ALL EXPOSED CORNERS
P6	-240mm CONC. BLOCK (GROUT FILL BLOCK CELLS)	• EXTEND TO U/S OF STRUCTURE ABOVE • BULL-NOSE BLOCKS AT ALL EXPOSED CORNERS
P7	- 16mm GYPSUM BOARD - 92mm METAL STUDS AT 400mm O/C - 16mm GYPSUM BOARD	• EXTEND TO U/S OF CEILING



ABBREVIATIONS LEGEND

CONC	CONCRETE
CW	COMPLETE WITH
DA	DIAMETER
EA	EACH
EQ	EQUAL
EWS	EYE WASH STATION
FD	FLOOR DRAIN
FFD	FUNNEL FLOOR DRAIN
FFH	FORCE FLOW HEATER
HCPB	HANDICAPPED PUSH BUTTON
HR	HOUR
HP	KEY PAD
MH	MOP HOLDER
MIN	MINUTE
MM	MINUTE
MM-01	OVERHEAD DOOR PUSH BUTTON
PTD	PAPER TOWEL DISPENSER
RWL	RAIN WATER LEADER
SD	SOAP DISPENSER
TYP	TYPICAL
U/S	UNDERSIDE
W	WITH

NO.	REVISIONS	DATE
4	ISSUED FOR ADDENDUM 4	2023-10-24
5	ISSUED FOR TENDER	2023-09-21
4	ISSUED FOR BUILDING PERMIT	2023-05-26
3	RE-ISSUED FOR SPA REVIEW #2	2022-07-15
2	ISSUED FOR SITE PLAN APPROVAL	2021-06-03
1	ISSUED FOR PRE-CONSULTATION	2020-05-27

DRAWINGS ARE NOT TO BE SCALED. CONTRACTOR MUST CHECK AND VERIFY ALL DIMENSIONS AND CONDITIONS ON THE PROJECT, AND MUST REPORT ANY DISCREPANCIES TO THE ARCHITECTS BEFORE PROCEEDING WITH THE WORK. THE USE OF THIS DRAWING OR PART THEREOF IS FORBIDDEN WITHOUT THE WRITTEN APPROVAL OF THE ARCHITECTS.

HOLY FAMILY CEMETERY CREMATORIUM
2543 LOWER BASE LINE ROAD
MILTON, ONTARIO

FLOOR PLAN

GRGURIC ARCHITECTS INCORPORATED



28 KING STREET EAST, UNIT B
STONEY CREEK, ONTARIO, L8G 1J8
Tel. 905-664-8735 Fax. 905-664-8737
Web: www.2gai.com

SCALE:	PROJECT:
AS NOTED	2019-08
START DATE:	OCT. 2019
DRAWN:	DRAWING:
D.W.	A2.00
CHECKED:	J.G.
PRINT DATE	10/24/23

ROOM FINISH SCHEDULE

RM. NO.	ROOM NAME	FLOOR FINISH		WALLS		CEILING		FINISH	HEIGHT	REMARKS
		FINISH	BASE	MATL		FINISH	MATL			
GROUND FLOOR										
101	VESTIBULE	PT	PT	GYP. BOARD	PAINT	GYP. BOARD	PAINT	3655		
102	CHAPEL	CPT	CPT	GYP. BOARD	PAINT	ACT-1 GYP. BOARD	-- PAINT	4095 3500		
103	OFFICE	CPT	CPT	CONC. BLOCK	PAINT	ACT-2	--	2745		
104	OFFICE	CPT	CPT	CONC. BLOCK	PAINT	ACT-2	--	2745		
105	STAFF ROOM	LVT	RB	CONC. BLOCK	PAINT	ACT-2	--	2745		
106	STAFF WASHROOM	PT	--	CONC. BLOCK	PAINT / CWT	GYP. BOARD	PAINT	2745		
106B	SHOWER	PT	--	CONC. BLOCK	CWT	GYP. BOARD	PAINT	2400		MOISTURE RESISTANT GYP. BOARD
107	CORRIDOR	LVT	RB	CONC. BLOCK	PAINT	ACT-2	--	2745		
108	CORRIDOR	LVT	RB	GYP. BOARD	PAINT	ACT-2	--	2745		
109	VIEWING ROOM	CPT	CPT	GYP. BOARD	PAINT	GYP. BOARD	PAINT	2745		
110	CIRCULATION AREA	EPOXY	RB	CONC. BLOCK	PAINT	ACT-2	--	3050		
111	UNIVERSAL WASHROOM	PT		GYP. BOARD	PAINT / CWT	GYP. BOARD	PAINT	2745		
112	WASHROOM	PT		GYP. BOARD	PAINT / CWT	GYP. BOARD	PAINT	2745		
113	WORK AREA	SC	RB	CONC. BLOCK	PAINT	GYP. BOARD	PAINT	3050		
114	PROCESSING ROOM	SC	RB	CONC. BLOCK	PAINT	GYP. BOARD	PAINT	3050		
115	JANITORS CLOSET	SC		CONC. BLOCK	PAINT	--	--	--		
116	CORRIDOR	SC		CONC. BLOCK	PAINT	ACT-2	--	3050		
117	ELECTRICAL/MECHANICAL ROOM	SC	RB	CONC. BLOCK	PAINT	--	--	2745		
118	COLD ROOM	SC		INTERIOR FINISH OF INSULATED METAL PANELS						
119	HOLDING ROOM	SC		CONC. BLOCK	PAINT	ACT-3	--	3050		
120	GARAGE	SC	RB	CONC. BLOCK	PAINT	GYP. BOARD	PAINT	4385		
121	RETORT ROOM	SC	RB	CONC. BLOCK	PAINT	--	--	--		
122	COAT ROOM	CPT	CPT	GYP. BOARD	PAINT	GYP. BOARD	PAINT	2745		
123	CORRIDOR	CPT	CPT	GYP. BOARD	PAINT	GYP. BOARD	PAINT	2745		

ROOM FINISH SCHEDULE NOTES

- SCHEDULES ARE TO BE READ IN CONJUNCTION WITH ALL DRAWINGS AND SPECIFICATIONS.
- PAINT ALL EXPOSED MISCELLANEOUS METALS AND SERVICES (E.G. DUCTS, CONDUITS, PIPING, ETC.) WHERE CEILINGS AND WALLS ARE SCHEDULED TO BE PAINTED.
- EXISTING WALLS SHALL BE CHASED AND OPENINGS CREATED AS REQUIRED TO EXECUTE THE WORK.
- MAKE GOOD ALL MATERIALS AND FINISHED WHERE DISTURBED AND ALTERATIONS OCCUR. REFER TO MECHANICAL AND ELECTRICAL DOCUMENTS FOR FULL EXTENT OF WORK REQUIRED. NOTE THAT MAKING GOOD INCLUDES WORK ASSOCIATED WITH THE INSTALLATION OF SERVICES SHOWN ON DRAWINGS.

DOOR / SCREEN SCHEDULE

ROOM NO	ROOM NAME	DOOR NO.	DOOR / SCREEN			FRAME					REMARKS				
			WIDTH	HEIGHT	THK	FIRE	TYPE	MATL	FIN.	GLASS		TYPE	MATL	FIN.	GLASS
GROUND FLOOR															
101	VESTIBULE	101A	(2) 950	2440	44		3	ALUM	ANOD	DGS	W1	ALUM	ANOD	DGS	HDO, HPB, WS, TH, CH, INS, PH, CL
102	CHAPEL	102A	(2) 950	2440	44		3	ALUM	ANOD	TG	SC3	ALUM	ANOD	TG	HDO, HPB, PH, CH
102	CHAPEL	102B	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	WS, TH, INS, CL, PH. NOTE: NO EXTERIOR HARDWARE REQUIRED.
103	OFFICE	103A	950	2150	44		1	SCWD	PLAM	-	A	HM	PAINT	-	
104	OFFICE	104A	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	
105	STAFF ROOM	105A	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	
106	STAFF WASHROOM	106A	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	
106A	SHOWER	106A A	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	
107	CORRIDOR	107A	1220	2150	44		1	SCWD	PLAM	-	A	HM	PAINT	-	
108	CORRIDOR	108A	1220	2150	44	90 MIN	1	SCWD	PLAM	-	A	HM	PAINT	-	CL
109	VIEWING ROOM	109A	950	2150	44		2	SCWD	PLAM	-	A	HM	PAINT	-	
109	VIEWING ROOM	109B	950	2150	44	90 MIN	2	SCWD	PLAM	-	A	HM	PAINT	-	CL
110	CIRCULATION AREA	110A	(2) 950	2150	44	90 MIN	1	HM	PAINT	-	B	HM	PAINT	-	CL
110	CIRCULATION AREA	110B	(2) 950	2150	44	90 MIN	1	HM	PAINT	-	B	HM	PAINT	-	CL
111	UNIVERSAL WASHROOM	111A	950	2150	44		1	SCWD	PLAM	-	A	HM	PAINT	-	HDO, HPB, ES
112	WASHROOM	112A	950	2150	44		1	SCWD	PLAM	-	A	HM	PAINT	-	
113	WORK AREA	113A	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	
114	PROCESSING ROOM	114A	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	
115	JANITORS CLOSET	128A	950	2150	44	45 MIN	1	HM	PAINT	-	A	HM	PAINT	-	CL
116	CORRIDOR	116A	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	WS, TH, INS, CL, PH
117	ELECTRICAL/MECHANICAL	117A	950	2150	44	90 MIN	1	HM	PAINT	-	A	HM	PAINT	-	CL
119	HOLDING ROOM	119A	(2) 950	2150	44		1	HM	PAINT	-	B	HM	PAINT	-	
119	HOLDING ROOM	119A	950	2150	44		1	HM	PAINT	-	A	HM	PAINT	-	WS, TH, INS, CL, PH
120	GARAGE	120A	(2) 950	2150	44	60 MIN	1	HM	PAINT	-	B	HM	PAINT	-	CL, WS, DS, TH
120	GARAGE	120B	3760	2800	-		4	-	-	-	-	-	-	-	OVERHEAD DOOR. REFER TO SPEC., ADO
120	GARAGE	120C	3760	2800	-		4	-	-	-	-	-	-	-	OVERHEAD DOOR. REFER TO SPEC., ADO
SCREENS															
101	VESTIBULE	SC3	-	-	-	-	-	-	-	-	ST2	ALUM	ANOD	TG	
109	VIEWING ROOM	SC1	-	-	-	90 MIN	-	-	-	-	ST1	HM	PAINT	FG	
109	VIEWING ROOM	SC2	-	-	-	90 MIN	-	-	-	-	ST1	HM	PAINT	FG	

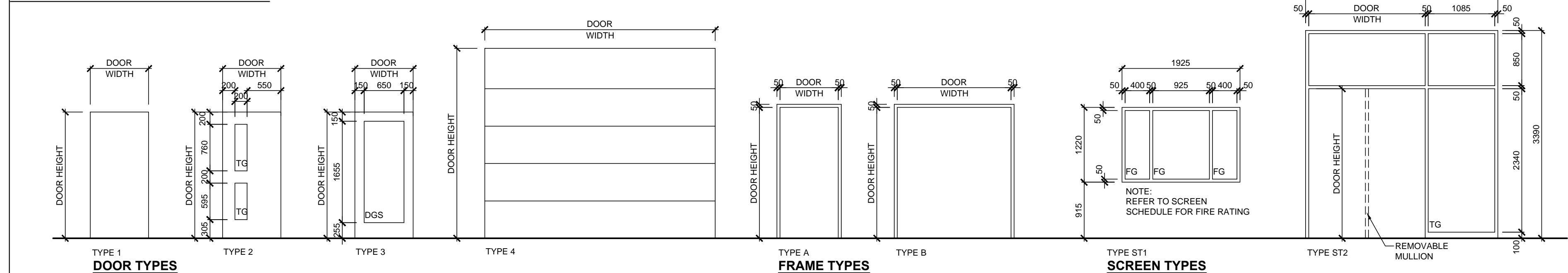
DOOR/SCREEN SCHEDULE NOTES

- GENERAL CONTRACTOR TO FIELD VERIFY ALL DOOR & FRAME ANGLES OR SUPPORTS FOR DOOR / FRAMES (BY DOOR / FRAME INSTALLER)
- GENERAL CONTRACTOR TO CO-ORDINATE LOCATION & INSTALLATION OF PUSH BUTTON / AUTOMATIC DOOR OPERATIONS AND ALL OTHER RELATED TRADES. TO BE SUPPLIED BY GENERAL CONTRACTOR & INSTALLED BY ELECTRICAL.
- REFER TO DOOR SCHEDULE FOR FIRE RESISTANCE RATINGS FOR DOOR, FRAMES & GLAZED FRAMES / SCREENS.
- ALL HM. DOORS & FRAMES TO BE PAINTED.
- REFER TO PLANS / DETAILS & WALL SECTIONS FOR LOCATIONS OF REQUIRED STEEL LINTELS / ANGLES (BY GENERAL CONTRACTOR) AND ANY FORMED ALUMINUM CLOSURE ANGLES OR SUPPORTS FOR DOOR / FRAMES (BY DOOR / FRAME INSTALLER)
- REFER TO DOOR HARDWARE SCHEDULE FOR ALL HOLD OPEN DEVICES, STRIKES, SECURITY, DOOR OPENERS, CLOSERS, PANIC HARDWARE, OVERHEAD STOPS, PUSH & KICK PLATES, ETC. & ANY OTHER DOOR HARDWARE REQUIREMENTS.

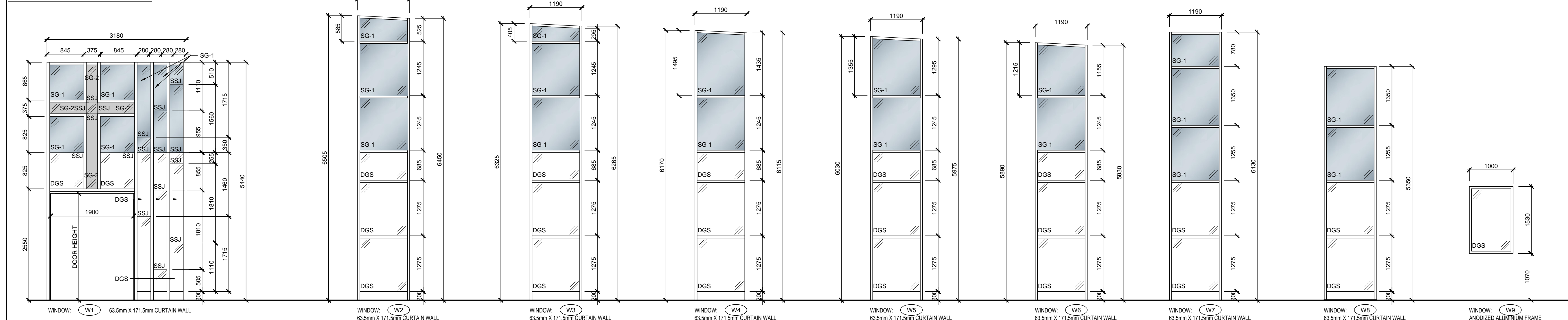
LEGEND

- ACT-X ACOUSTIC CEILING TILE
- ADO AUTOMATIC DOOR OPERATOR
- AFF ABOVE FINISHED FLOOR
- ANOD ANODIZED
- CH CONTINUOUS HINGE
- CL CLOSER
- CG CONCRETE
- CWT CERAMIC WALL TILE
- DGS DOUBLE GLAZED SEALED INSULATING GLASS UNITS
- DS DOOR SWEEP
- ES ELECTRIC STRIKE
- EX EXISTING
- EXP EXPOSED
- FG FIRE RATED GLASS
- HDO HANDICAP DOOR OPERATOR
- HPB HANDICAPPED PUSH BUTTON
- HM HOLLOW METAL
- INS THERMALLY INSULATED DOOR / FRAME
- LVT LUXURY VINYL TILE
- MTL METAL
- PH PANIC HARDWARE
- PLAM PLASTIC LAMINATE
- PT PORCELAIN TILE
- RB RUBBER BASE
- RM REMOVEABLE MULLION
- SG SEALED CONCRETE
- SCWD SOLID CORE WOOD DOOR
- SG-xx SPANDREL GLASS
- STRUCT STRUCTURE
- SSJ STRUCTURAL SILICONE JOINT
- TG TEMPERED GLASS
- TH THRESHOLD
- THK THICKNESS
- UNO UNLESS NOTED OTHERWISE
- VCT VINYL COMPOSITE TILE
- VAR VARIES
- WD WOOD
- WS WEATHER STRIPPING
- W/ WITH

DOOR/FRAME/SCREEN TYPES



WINDOW FRAME TYPES



WINDOW TYPES

HOLY FAMILY CEMETERY
CREMATORIUM
2543 LOWER BASE LINE ROAD
MILTON, ONTARIO

ROOM FINISH AND DOOR SCHEDULES

GRGURIC ARCHITECTS INCORPORATED

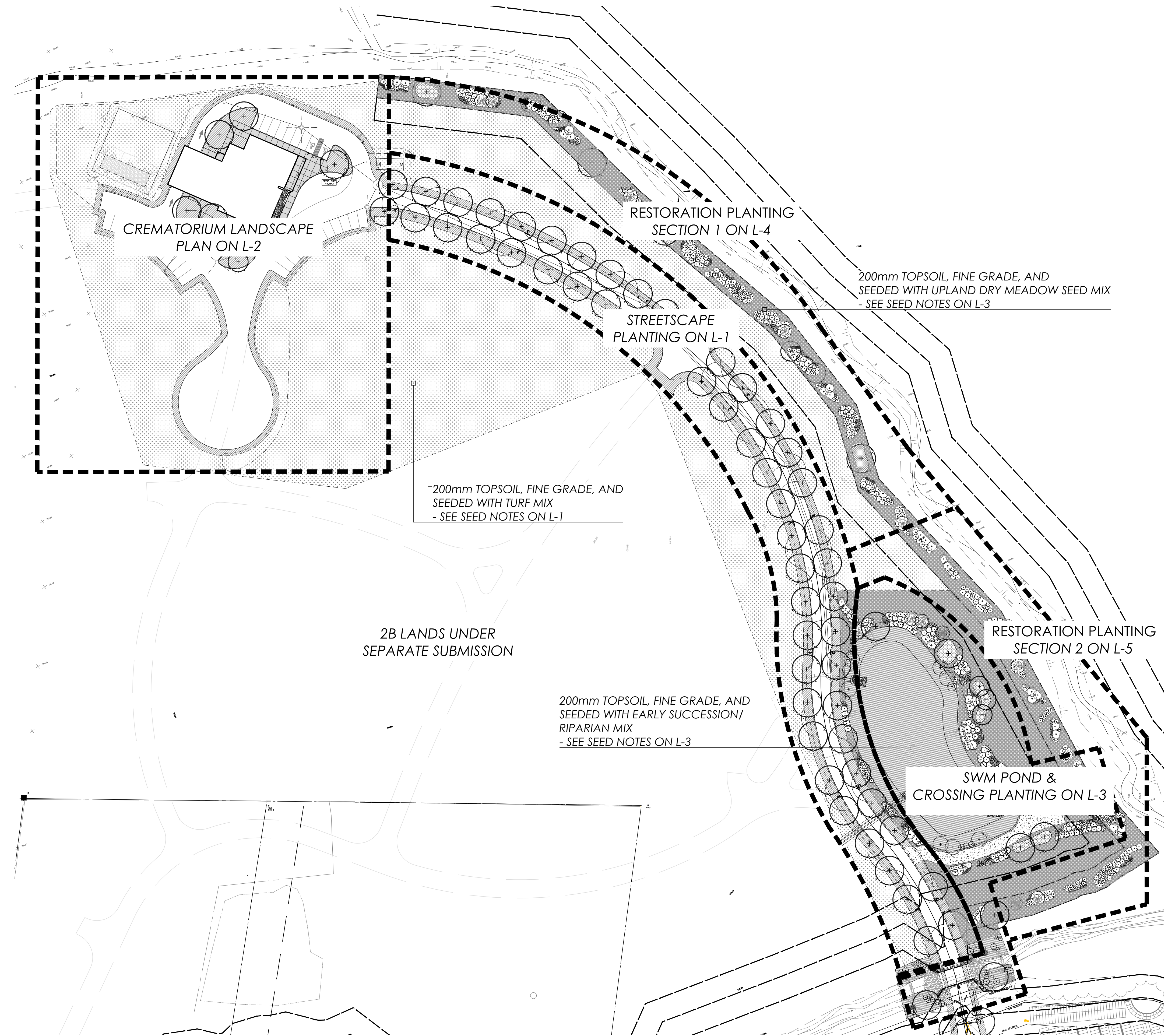
28 KING STREET EAST, UNIT B
STONE CREEK, ONTARIO, L8G 1J8
Tel. 905-664-8735 Fax. 905-664-8737
Web: www.2gai.com

SCALE: AS NOTED	PROJECT: 2019-08
START DATE: OCT. 2019	
DRAWN: D.W.	DRAWING: A8.00
CHECKED: J.G.	
PRINT DATE 10/23/23	

Holy Family Cemetery Crematorium Building

ISSUED FOR SI #1
October 17, 2023

CLIENT:
The Catholic Cemeteries
2523 Lower Base Line
Milton, ON



DRAWING SCHEDULE:

SHEET	DRAWING
L-1	Landscape Plan (Street Planting)
L-2	Landscape Plan (Crematorium Building)
L-3	Storm Water Management Pond
L-4	Landscape Plan (Restoration Planting Section 1)
L-5	Landscape Plan and Details (Restoration Planting Section 2)

PLANT SCHEDULE BUFFER PLANTING

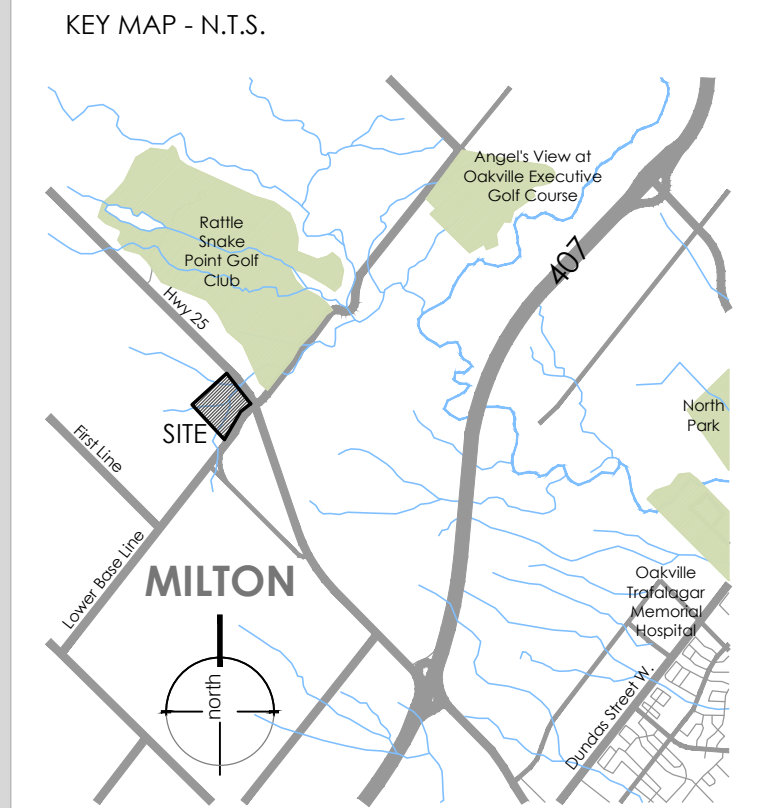
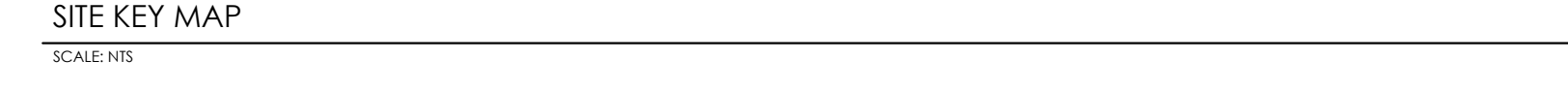
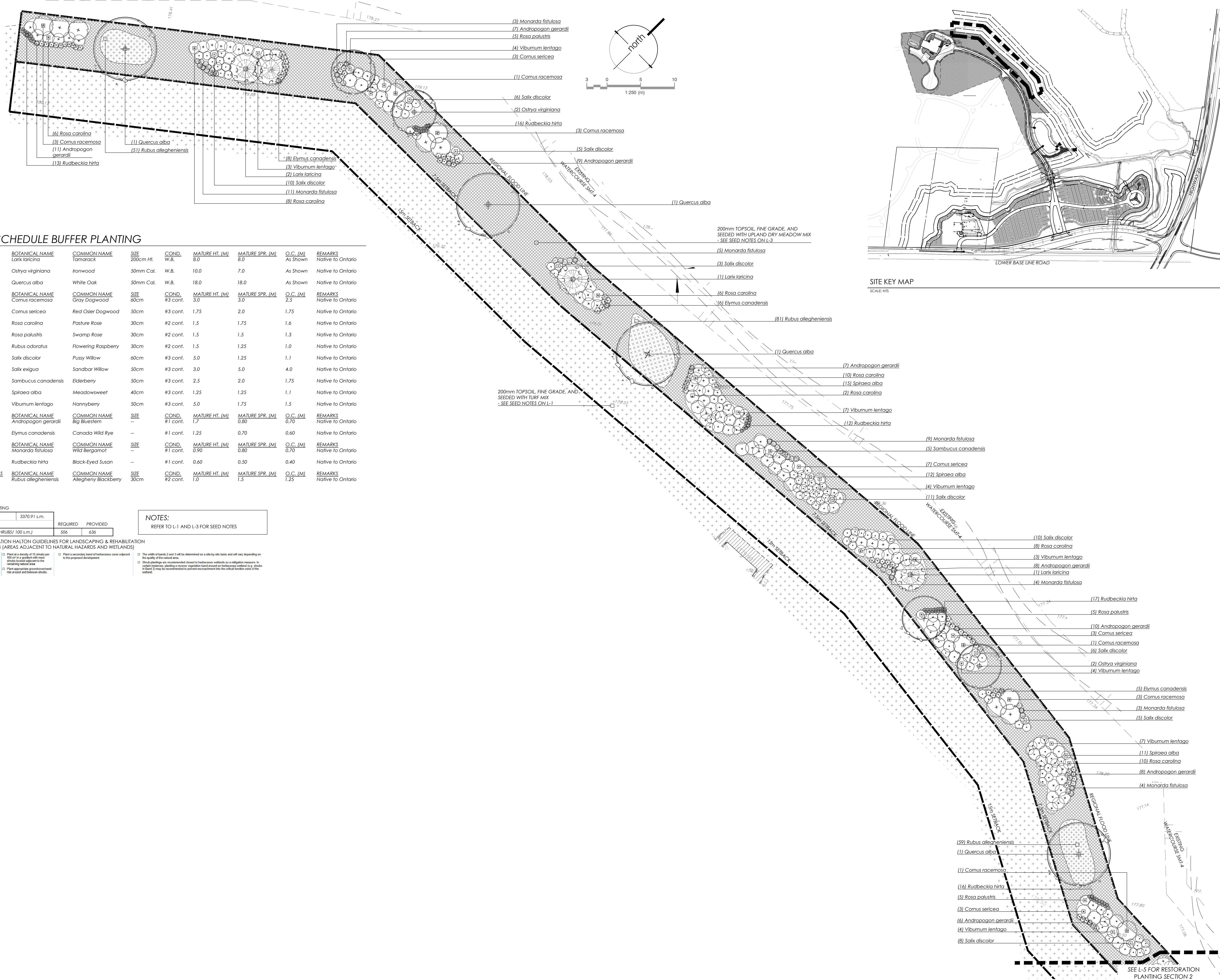
TREES	BOTANICAL NAME	COMMON NAME	SIZE	COND.	MATURE HT. (M)	MATURE SPR. (M)	O.C. (M)	REMARKS
8	Larix laricina	Tamarack	200cm Ht.	W.B.	8.0	8.0	As Shown	Native to Ontario
4	Ostrya virginiana	Ironwood	50mm Cal.	W.B.	10.0	7.0	As Shown	Native to Ontario
5	Quercus alba	White Oak	50mm Cal.	W.B.	18.0	18.0	As Shown	Native to Ontario
SHRUBS	BOTANICAL NAME	COMMON NAME	SIZE	COND.	MATURE HT. (M)	MATURE SPR. (M)	O.C. (M)	REMARKS
31	Cornus racemosa	Gray Dogwood	60cm	#3 cont.	3.0	3.0	2.5	Native to Ontario
35	Cornus sericea	Red Osier Dogwood	50cm	#3 cont.	1.75	2.0	1.75	Native to Ontario
84	Rosa carolina	Pasture Rose	30cm	#2 cont.	1.5	1.75	1.6	Native to Ontario
53	Rosa palustris	Swamp Rose	30cm	#2 cont.	1.5	1.5	1.3	Native to Ontario
4	Rubus odoratus	Flowering Raspberry	30cm	#2 cont.	1.5	1.25	1.0	Native to Ontario
99	Salix discolor	Pussy Willow	60cm	#3 cont.	5.0	1.25	1.1	Native to Ontario
2	Salix exigua	Sandbar Willow	50cm	#3 cont.	3.0	5.0	4.0	Native to Ontario
12	Sambucus canadensis	Elderberry	50cm	#3 cont.	2.5	2.0	1.75	Native to Ontario
69	Spiraea alba	Meadowsweet	40cm	#3 cont.	1.25	1.1	1.25	Native to Ontario
51	Viburnum lentago	Nannyberry	50cm	#3 cont.	5.0	1.75	1.5	Native to Ontario
GRASSES	BOTANICAL NAME	COMMON NAME	SIZE	COND.	MATURE HT. (M)	MATURE SPR. (M)	O.C. (M)	REMARKS
87	Andropogon gerardii	Big Bluestem	#1 cont.	1.7	0.80	0.70	0.70	Native to Ontario
31	Elymus canadensis	Canada Wild Rye	#1 cont.	1.25	0.70	0.60	0.60	Native to Ontario
PERENNIALS	BOTANICAL NAME	COMMON NAME	SIZE	COND.	MATURE HT. (M)	MATURE SPR. (M)	O.C. (M)	REMARKS
49	Monarda fistulosa	Wild Bergamot	#1 cont.	0.90	0.80	0.70	0.70	Native to Ontario
82	Rudbeckia hirta	Black-Eyed Susan	#1 cont.	0.60	0.50	0.40	0.40	Native to Ontario
GROUND COVERS	BOTANICAL NAME	COMMON NAME	SIZE	COND.	MATURE HT. (M)	MATURE SPR. (M)	O.C. (M)	REMARKS
191	Rubus allegheniensis	Allegheny Blackberry	30cm	#2 cont.	1.0	1.5	1.25	Native to Ontario

RESTORATION PLANTING	
BLOCK AREA:	3370.91 s.m.
TOTAL SHRUBS (15 SHRUBS/ 100 s.m.)	505 REQUIRED / 636 PROVIDED

AS PER CONSERVATION HALTON GUIDELINES FOR LANDSCAPING & REHABILITATION PLANS SECTION 3.4 (AREAS ADJACENT TO NATURAL HAZARDS AND WETLANDS)

- 1. This table provides a list of plants that are recommended for use in the proposed development.
- 2. The width of blocks 2 and 3 will be determined on a site-by-site basis and will vary depending on the quality of the natural area.
- 3. Site changes to recommended plants to herbaceous vegetation or a different species, in certain situations, planting a more vigorous plant based on herbaceous material (e.g. shrubs or trees) may be recommended to prevent encroachment into the critical function zone of the wetland.
- 4. These appropriate groundcover/mulch areas and between shrubs.
- 5. There is a secondary band of herbaceous cover adjacent to the proposed development.

NOTES:
REFER TO L-1 AND L-3 FOR SEED NOTES



- LEGEND
- proposed deciduous tree
 - proposed coniferous tree
 - proposed shrub
 - 181.98 existing elevation
 - 179.70 proposed elevation
 - min. 200mm topsoil, fine grade & seed with turf mix
 - min. 200mm topsoil, fine grade & seed with Upland Dry Meadow Mix

FOR LANDSCAPE NOTES REFER TO L-2

ISSUED FOR TENDER

REVISIONS/ SUBMISSIONS

#	DATE	DESCRIPTION
1	2021-04-25	Issued for Submission
2	2022-09-21	Issued for Submission
3	2022-12-15	Issued for Submission
4	2023-05-26	Issued for Permit
5	2023-05-31	Issued for Tender
6	2023-10-17	Issued for SI #1



CLIENT
The Catholic Cemeteries
MUNICIPALITY
Town of Milton

PROJECT
Holy Family Cemetery
Crematorium Building
2523 Lower Base Line Road

MUNICIPAL FILE NUMBER
SP 19/21

SHEET
Landscape Plan
RESTORATION PLANTING
SECTION 1

adesso design inc.
landscape architecture

218 Locke Street South, 2nd Floor
Hamilton, ON L8P 4B4
t. 905.526.8876
www.adessodesigninc.ca

